

H. Eléctricos

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LÁMINAS

B. P.



116

7a

F.A.S.  
218

F.

2

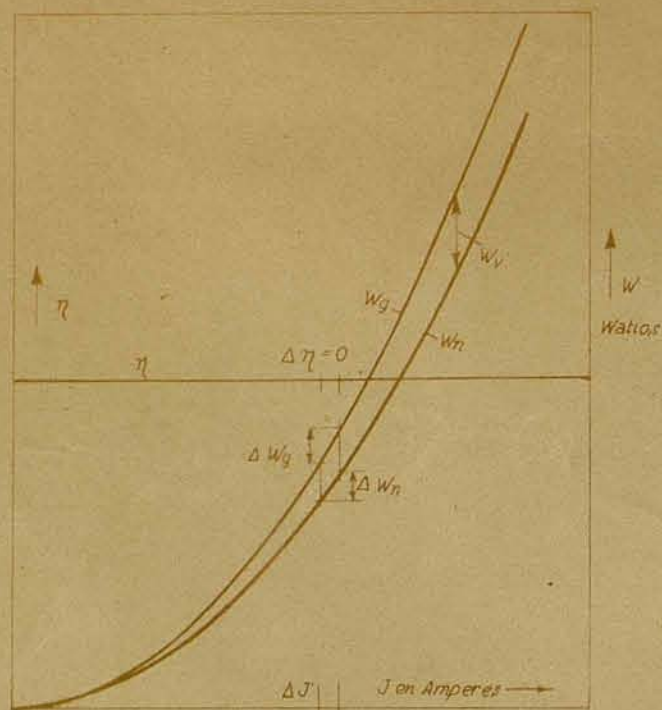


Fig. 1.

$W_g = \text{potencia total}$   
 $W_n = \text{" util.} = J^2 R_n$   
 $W_v = \text{" perdida} = J^2 R_v$   
 $\eta = \frac{W_n}{W_g}$

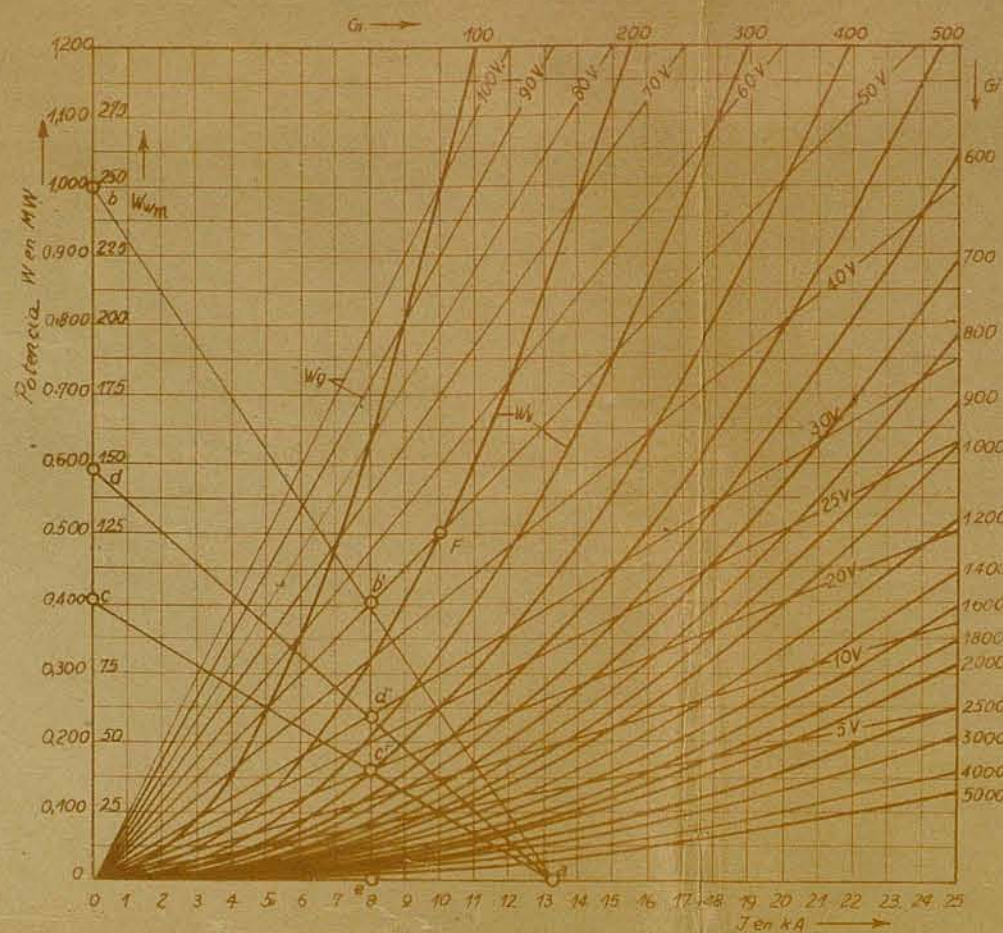


Fig. 3. Gráfico de funcionamiento para hornos de c. continua con diferentes curvas características y tensiones

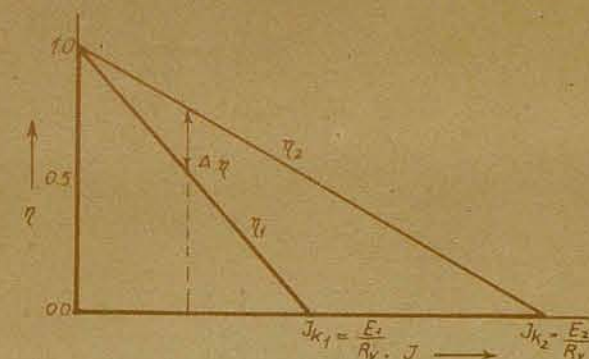


Fig. 5.

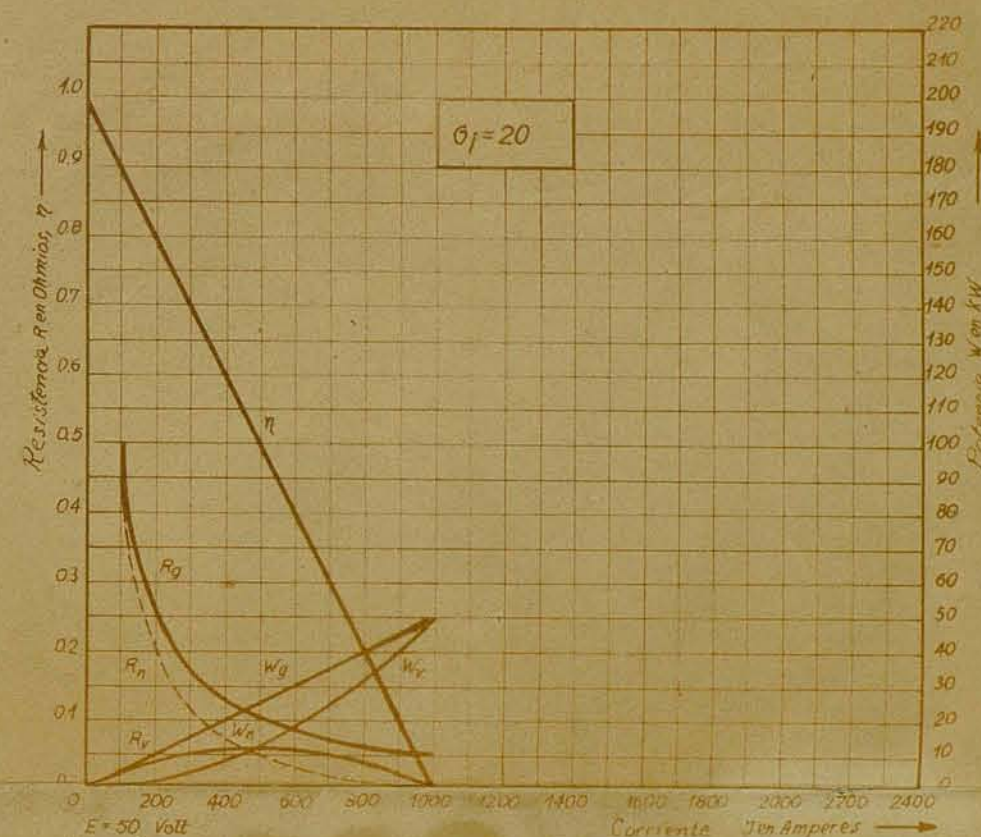


Fig. 6. Características de un horno de c. continua ( $G_1 = 20$ ,  $E = 50$  Volt)

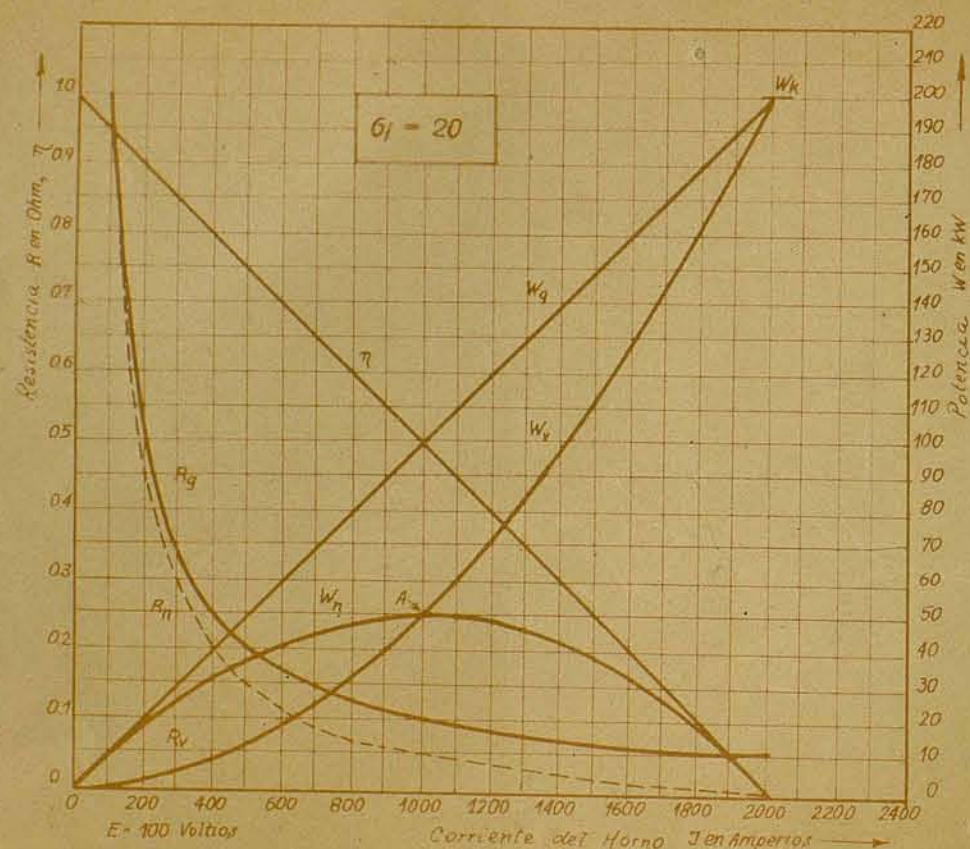


Fig. 2. Líneas características de un horno de arco para c. continua

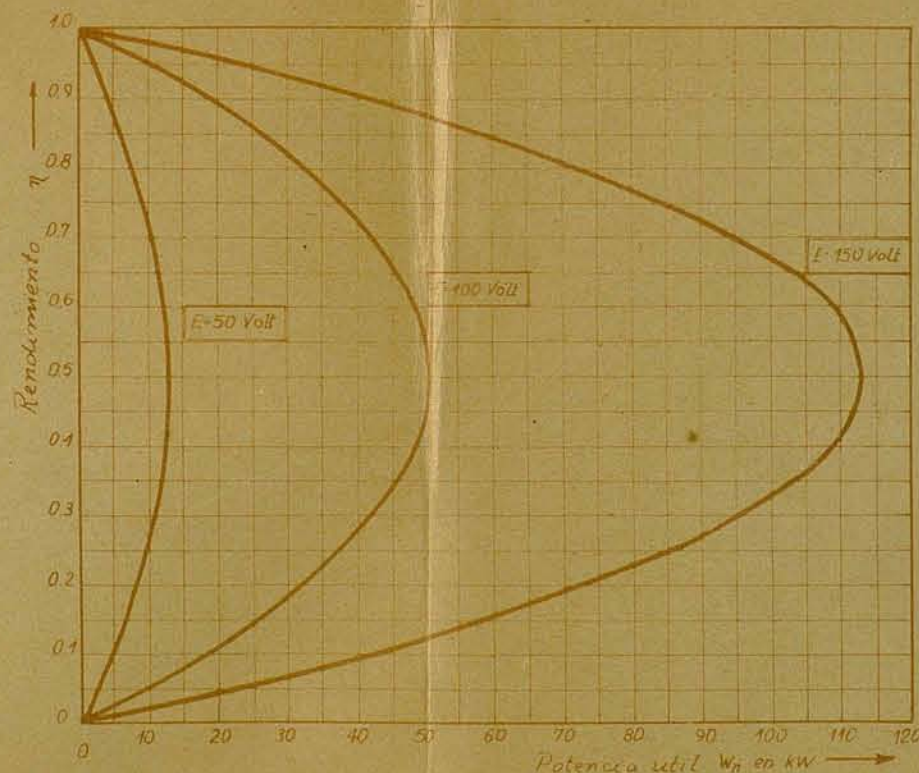


Fig. 4.

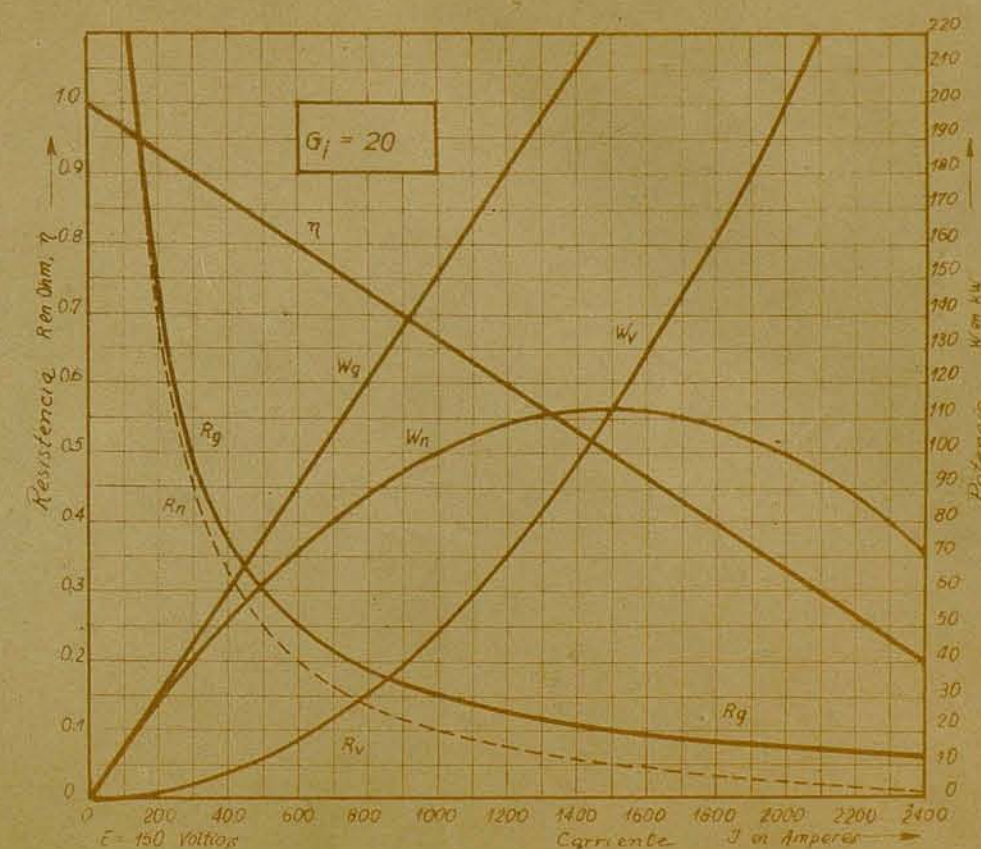


Fig. 1. Características de un horno de c. continua ( $G_1 = 20$ ,  $E = 150$  Volt)

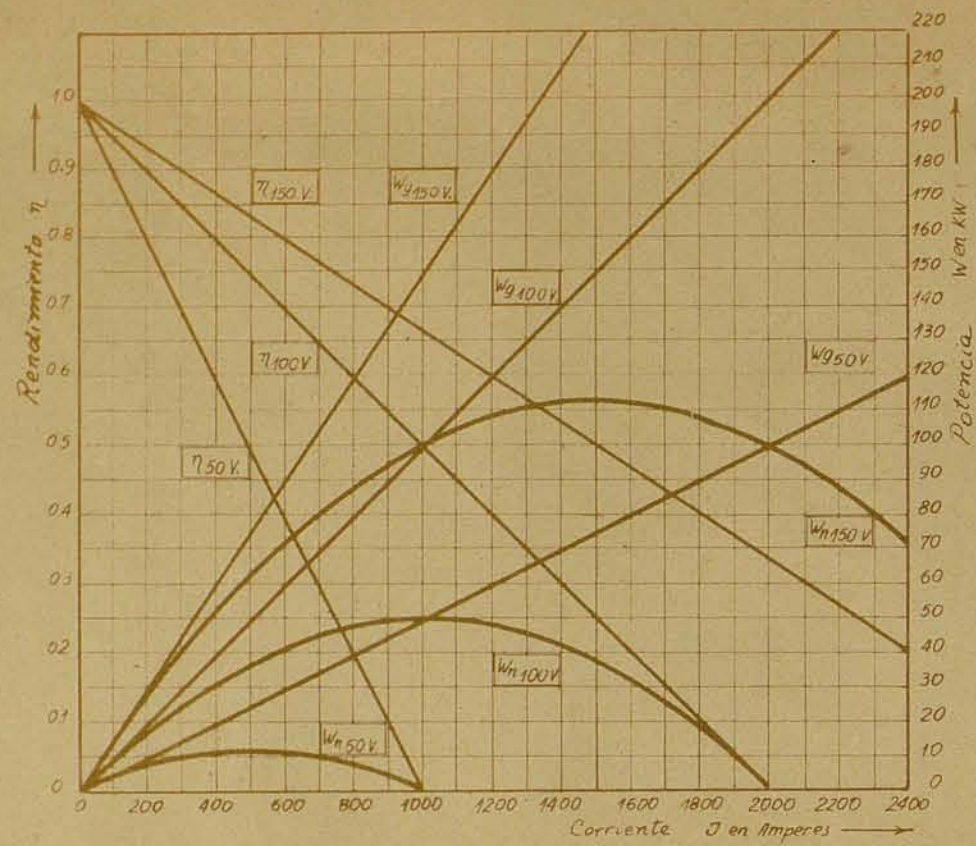


Fig. 8.

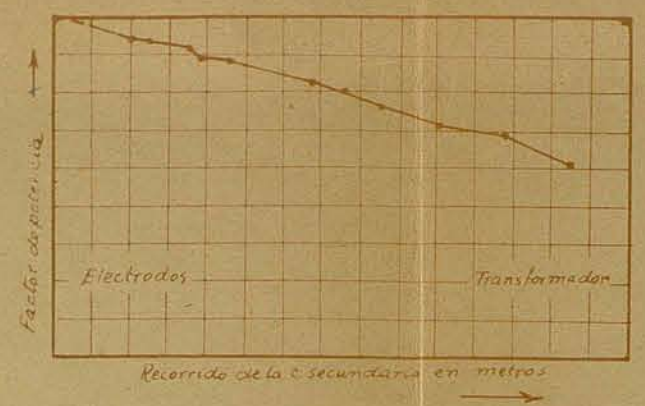


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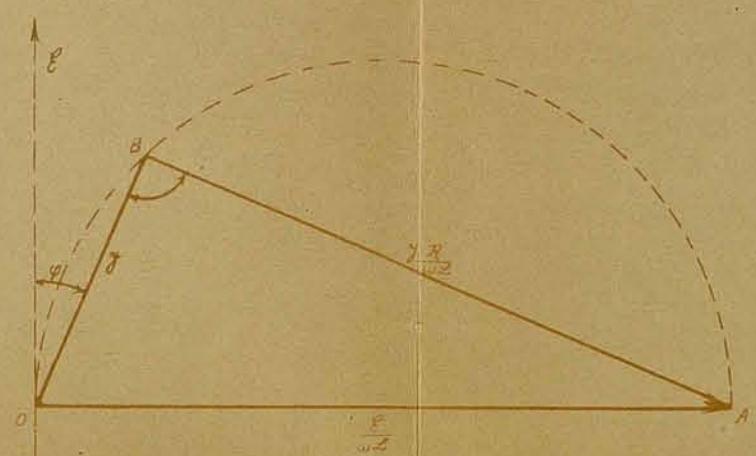


Fig. 11. Diagrama de círculo

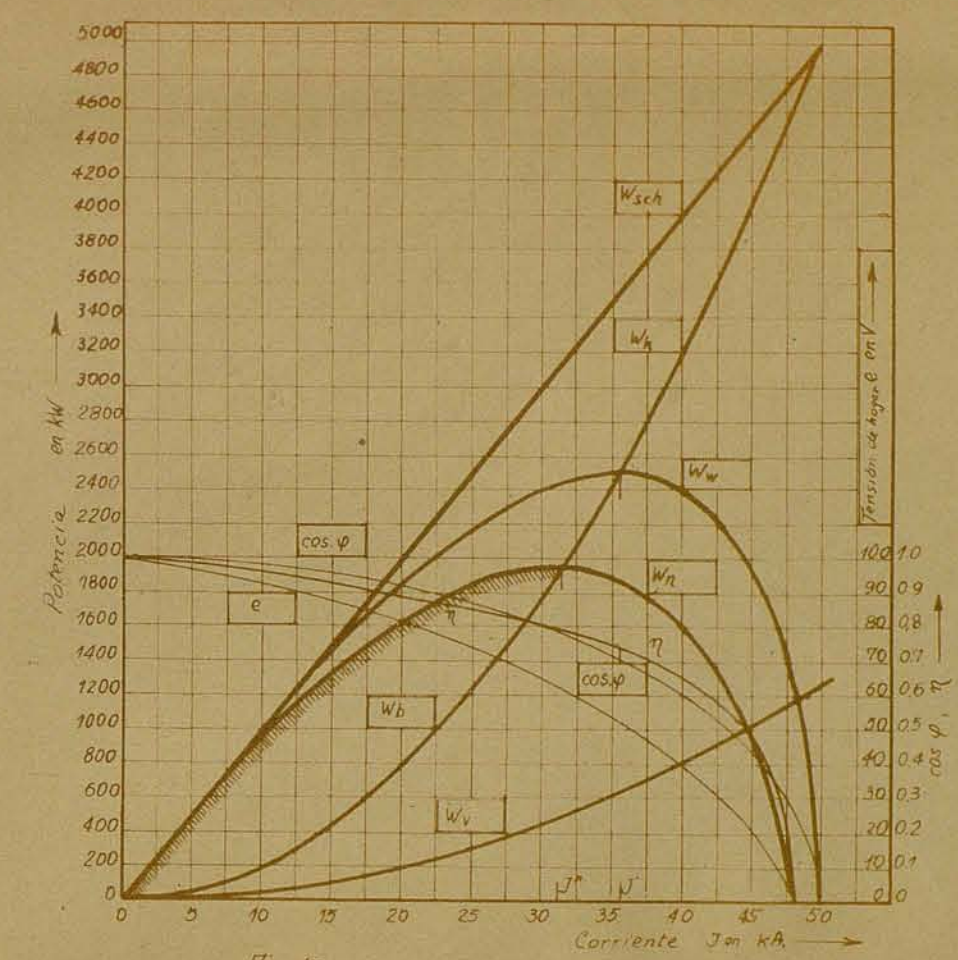


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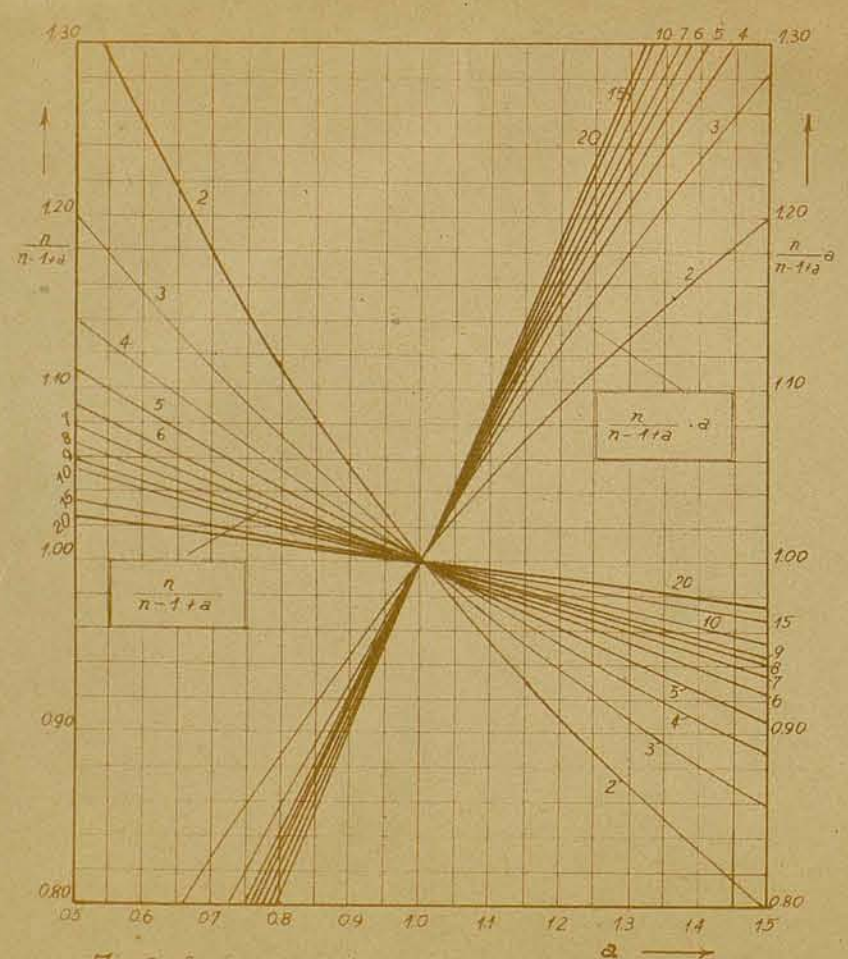


Fig. 9. Gráfico para la conexión en serie de varios hornos de c. continua

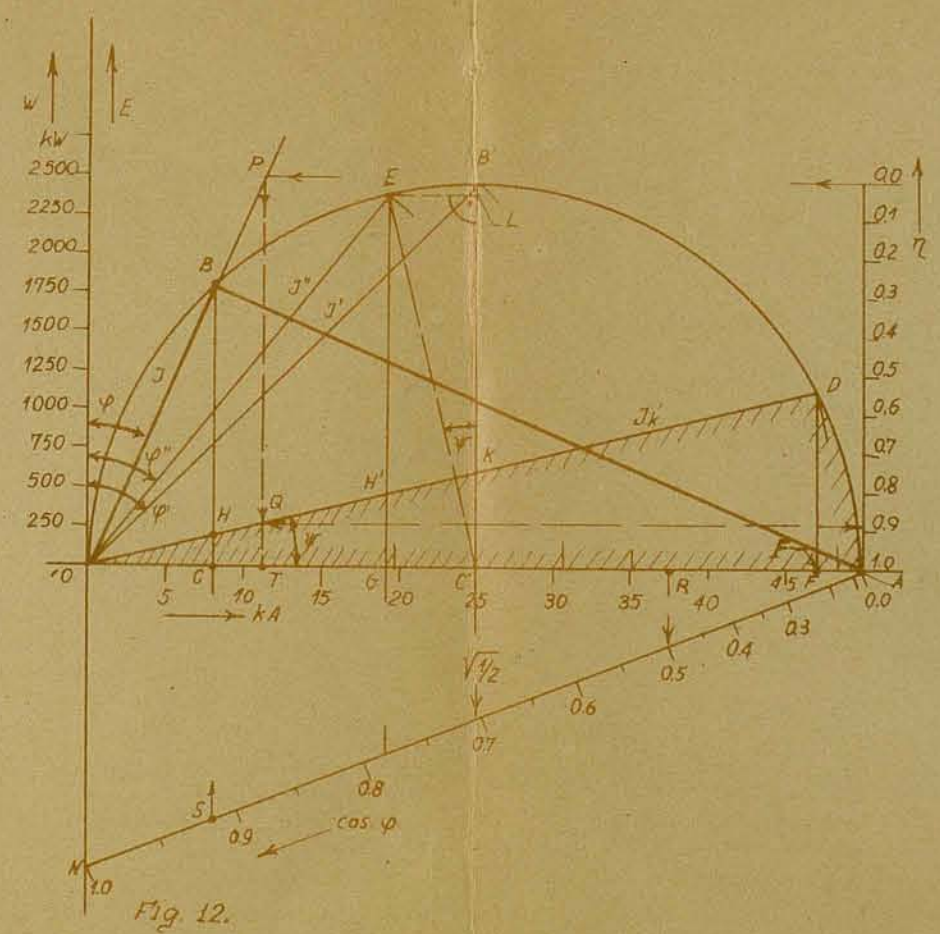


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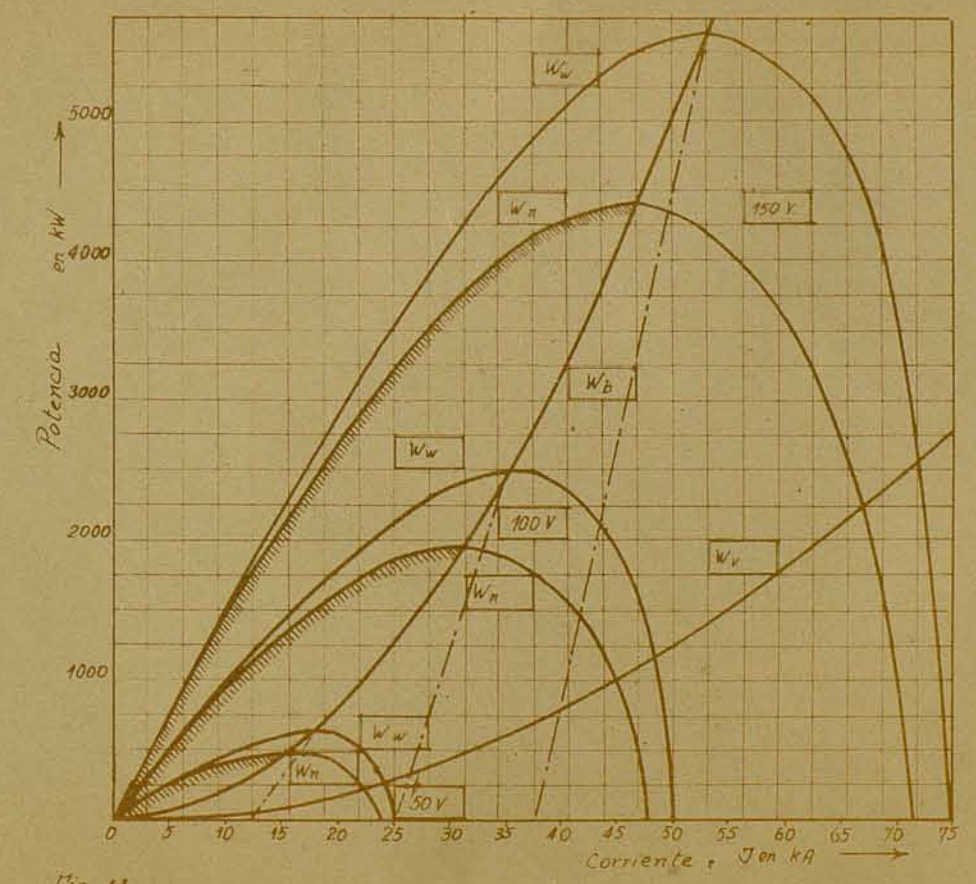


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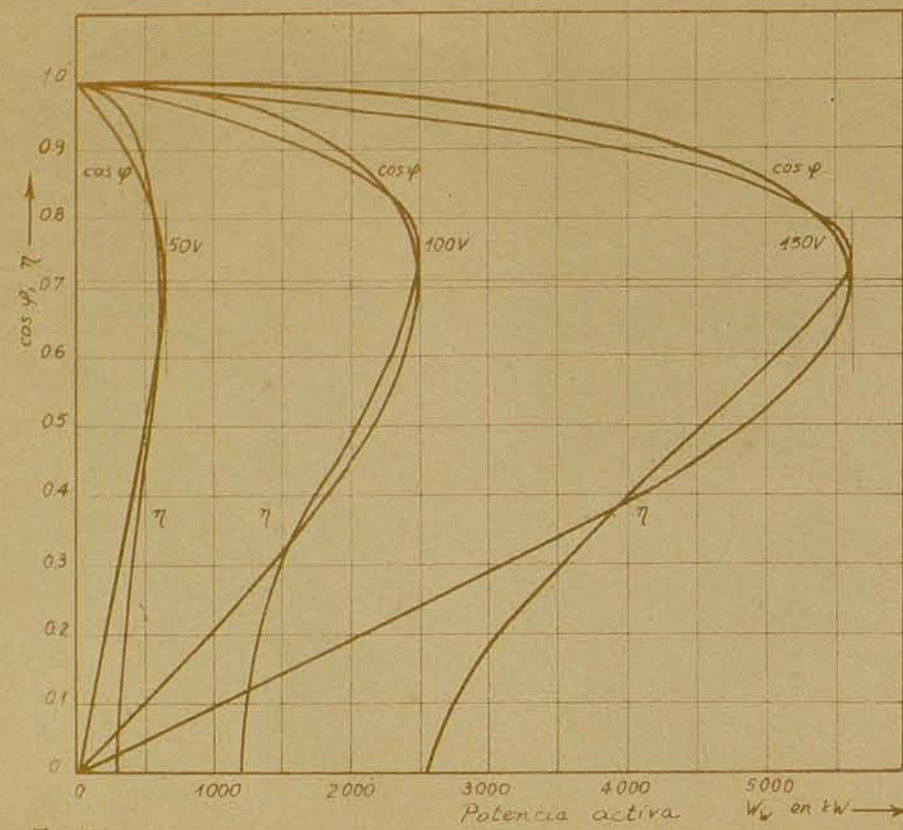


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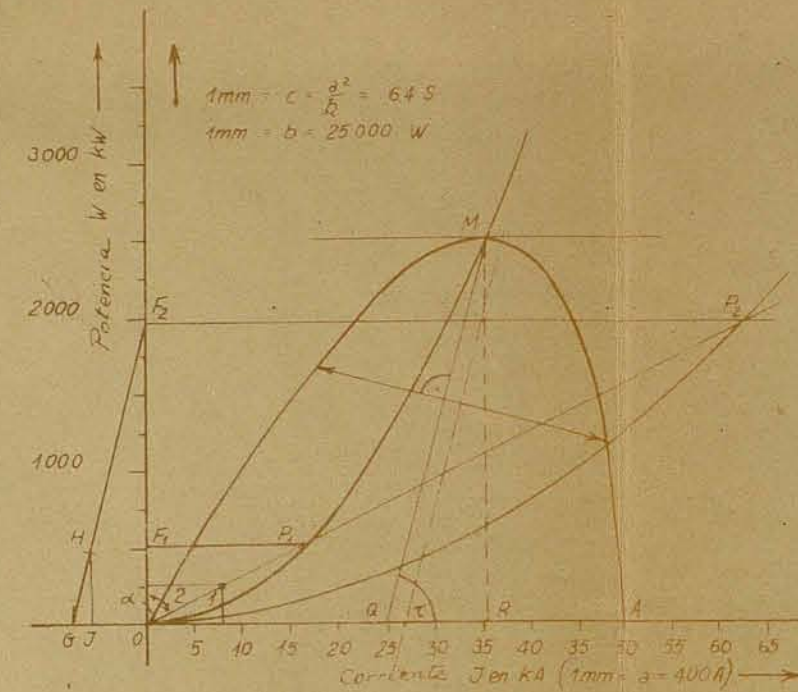


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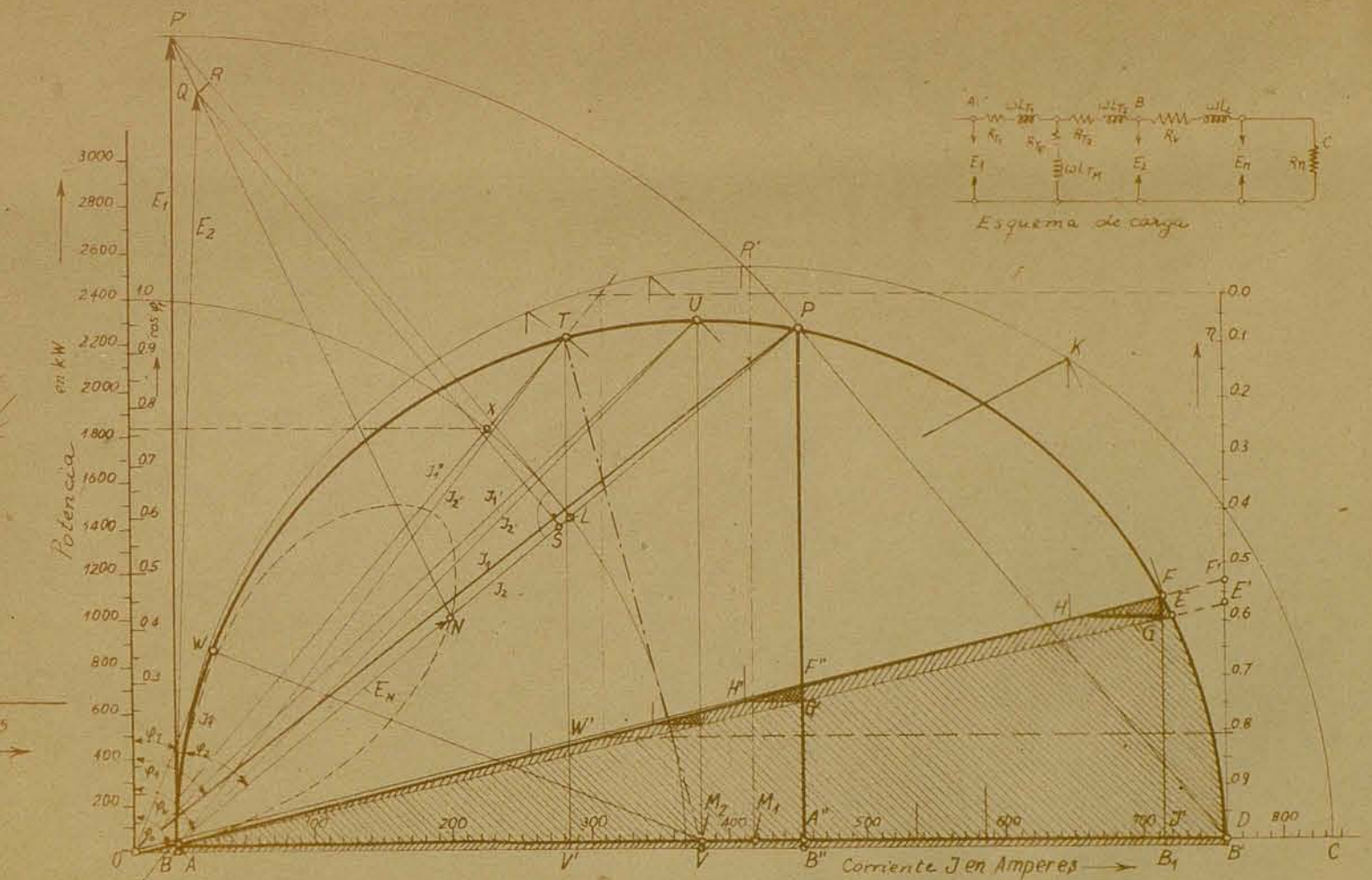


Fig. 20. Diagrama general de circuito del Horno de c alterna teniendo en cuenta la influencia del transformador

(Escala de corrientes)  
 $AC = I_{k1}$ ,  $AB' = I_{kT}$ ,  $AF = I_{kL}$ ,  $OF = I_{kV}$ ,  $OB' = W_{b1}$ ,  $AB' = W_{b1}$ ,  $UV = W_{w,m}$   
 $FG = I_{k2}^2 \cdot R_L$ ,  $GI' = I_{k2}^2 \cdot R_L$ ,  $FI' = I_{k2}^2 \cdot R_{V1}$ ,  $OB' = W_{b1}$ ,  $AB' = W_{b1}$ ,  $UV = W_{w,m}$   
 $= W_{V1}$ ,  $= W_{V2}$ ,  $= W_{V3}$ ,  $= W_{V4}$ ,  $= W_{V5}$ ,  $= W_{V6}$ ,  $= W_{V7}$ ,  $= W_{V8}$ ,  $= W_{V9}$ ,  $= W_{V10}$

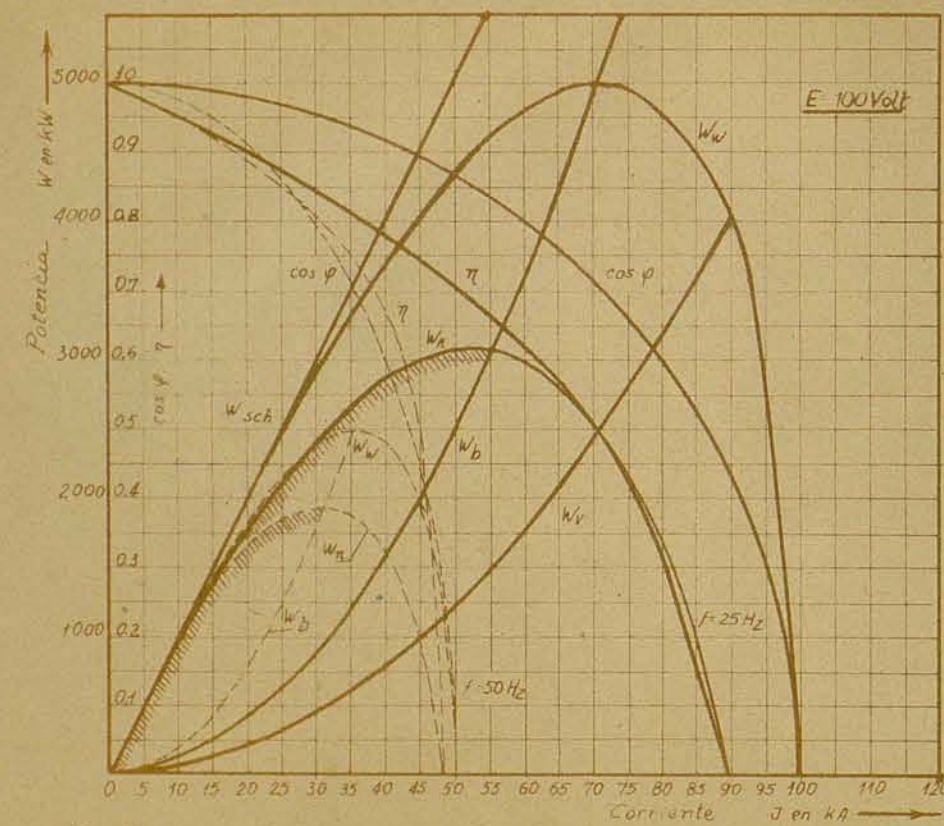


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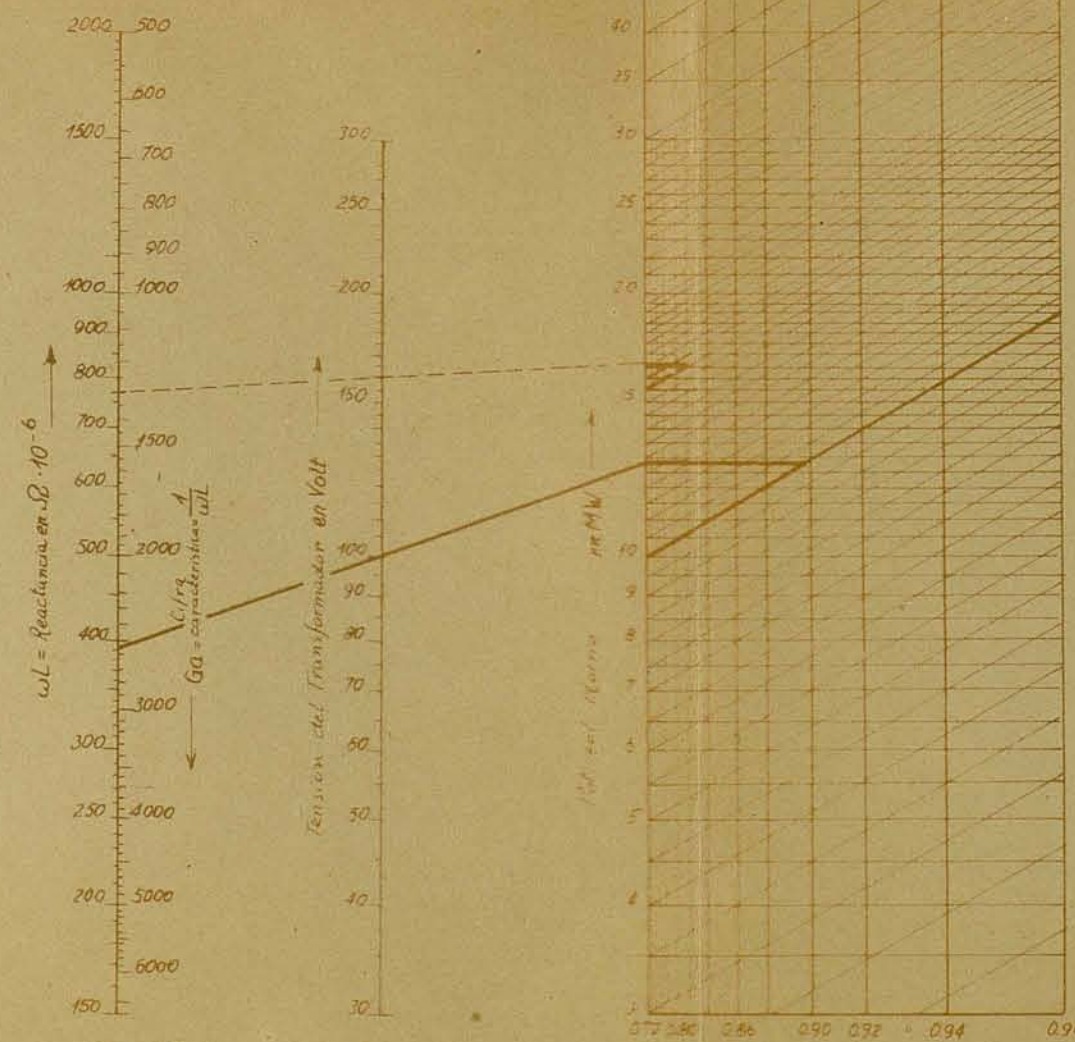


Fig. 19. Abaco para la determinacion de la potencia activa partiendo de la cifra caracteristica, la tension del transformador y el factor de potencia.

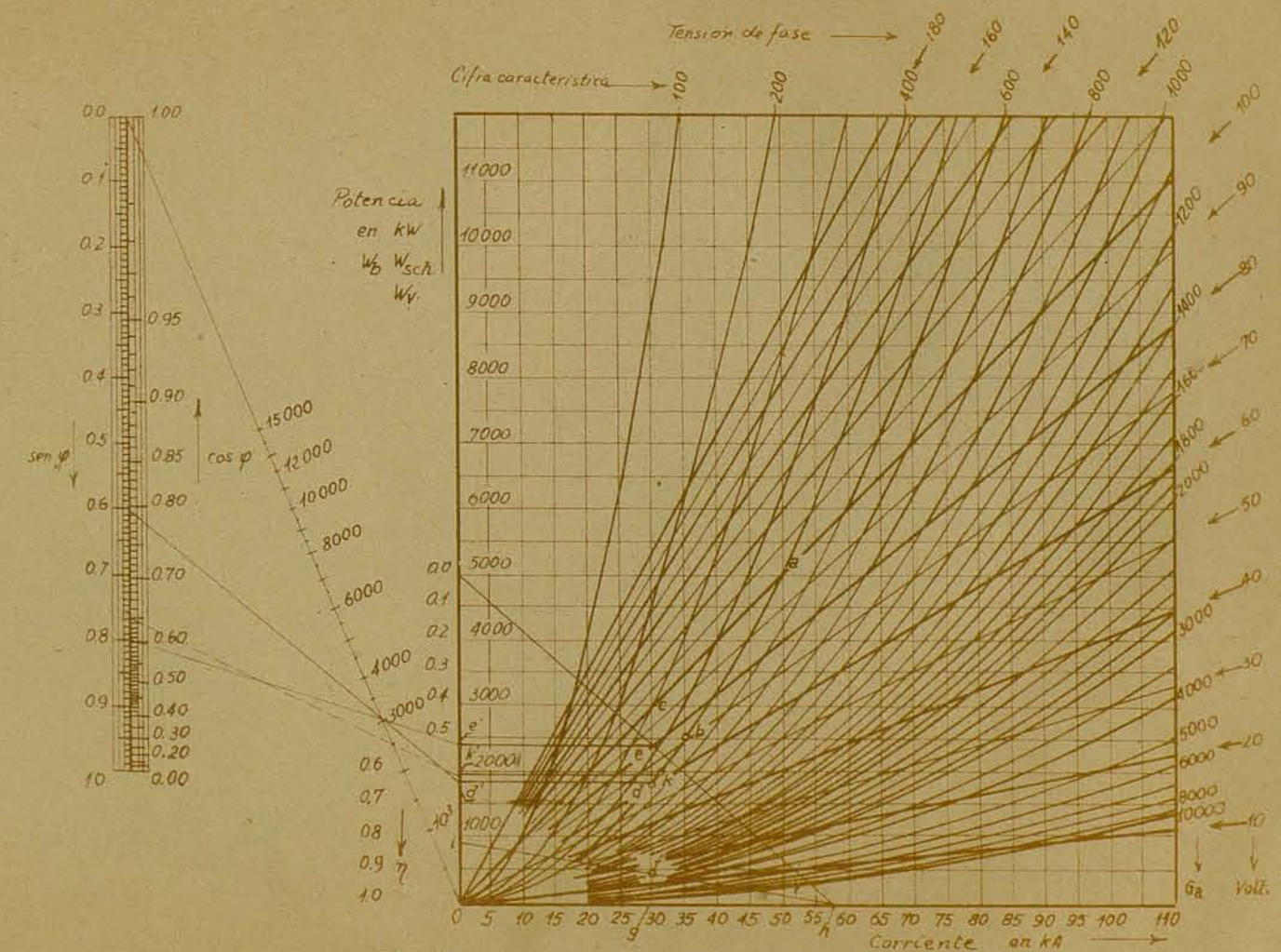


Fig. 18. Abaco para hornos de electrodo de c alterna

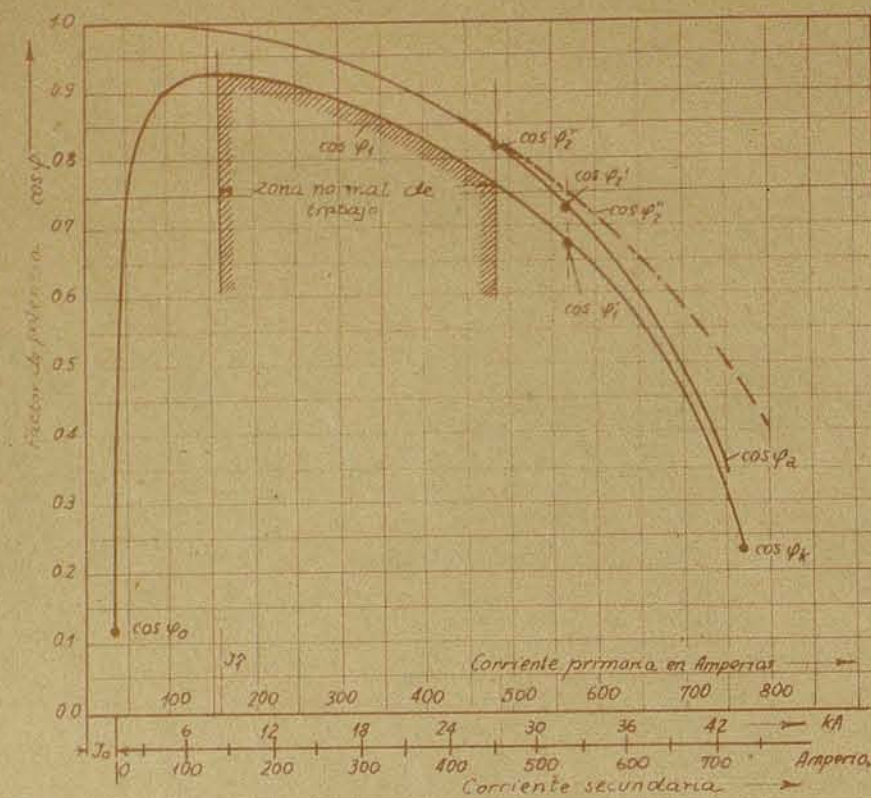


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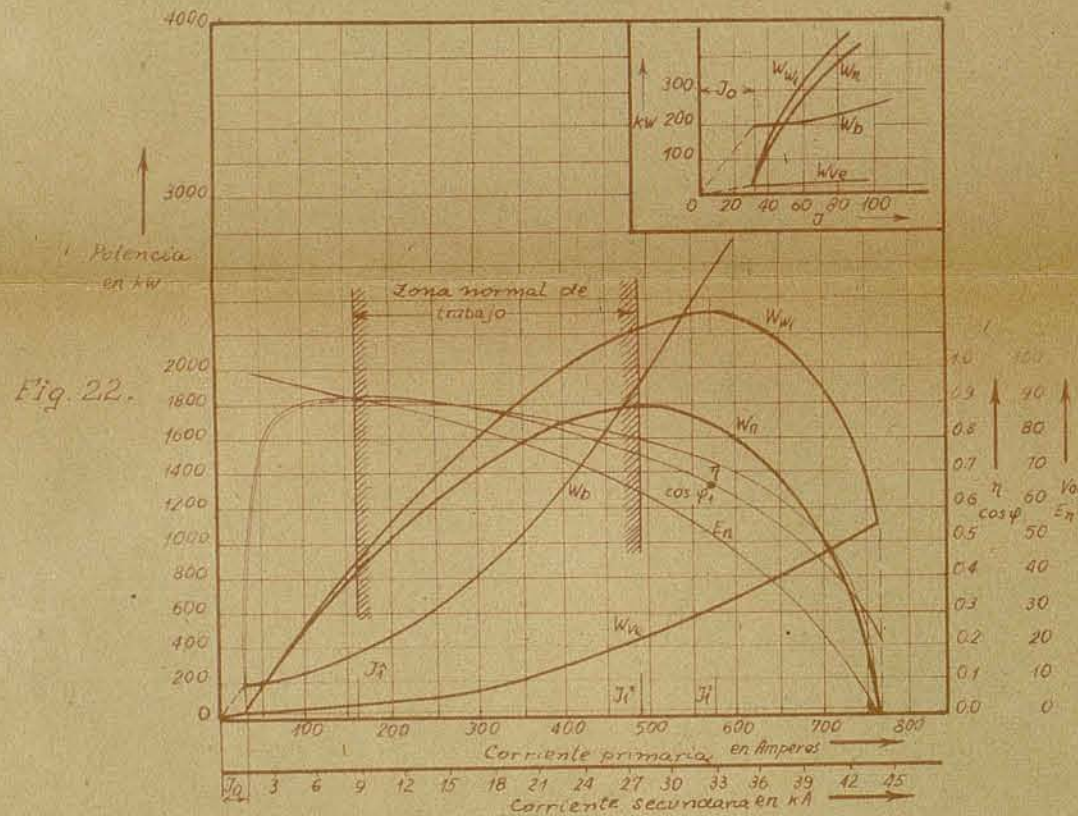


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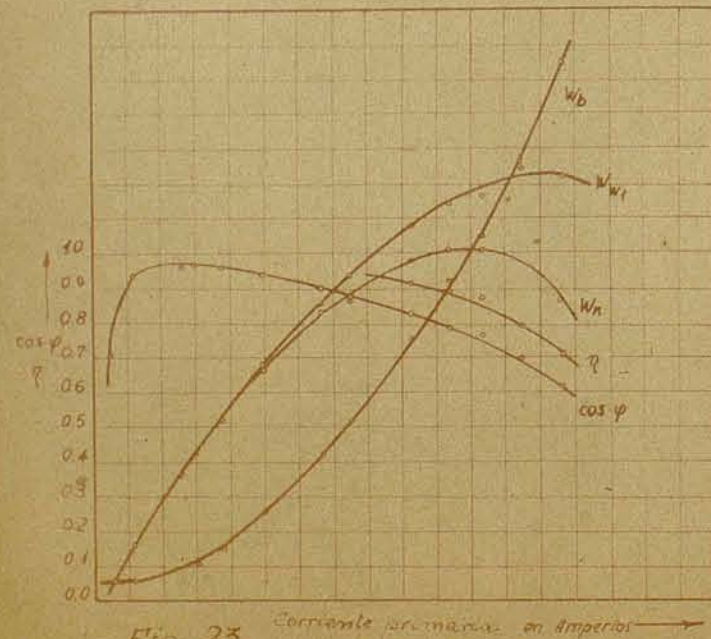


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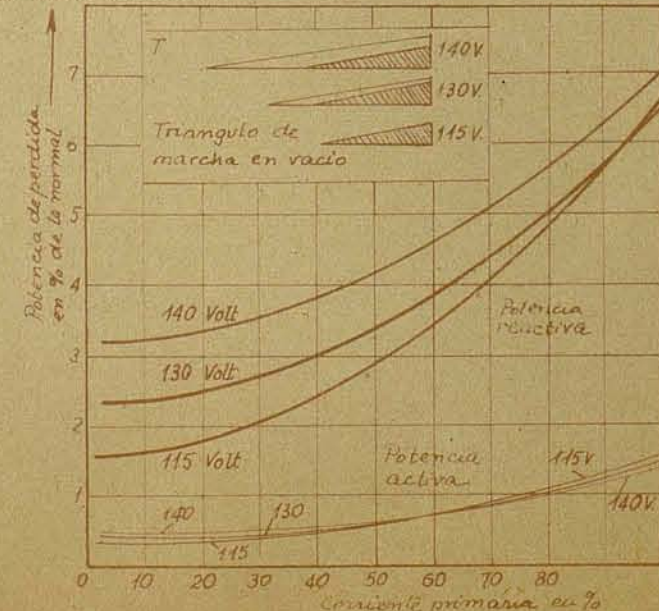


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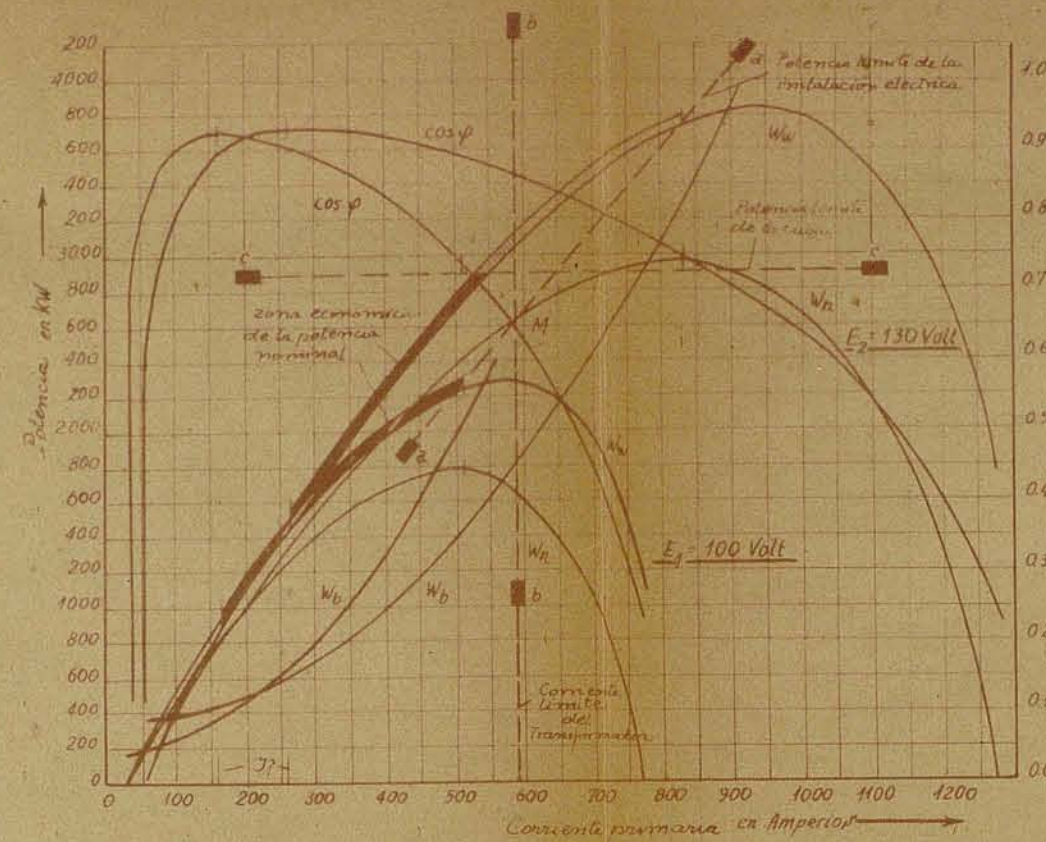


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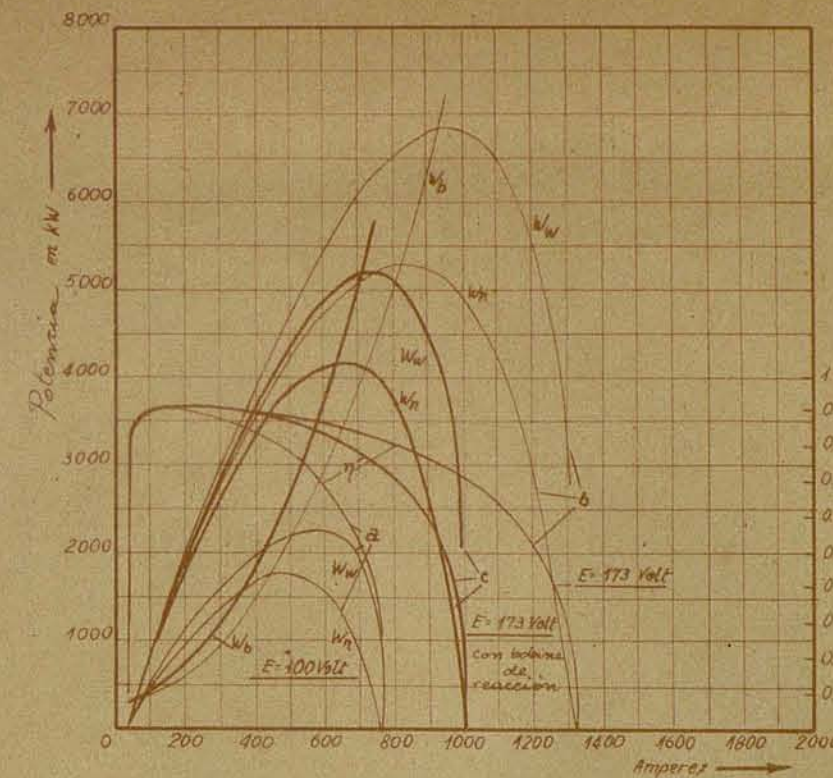


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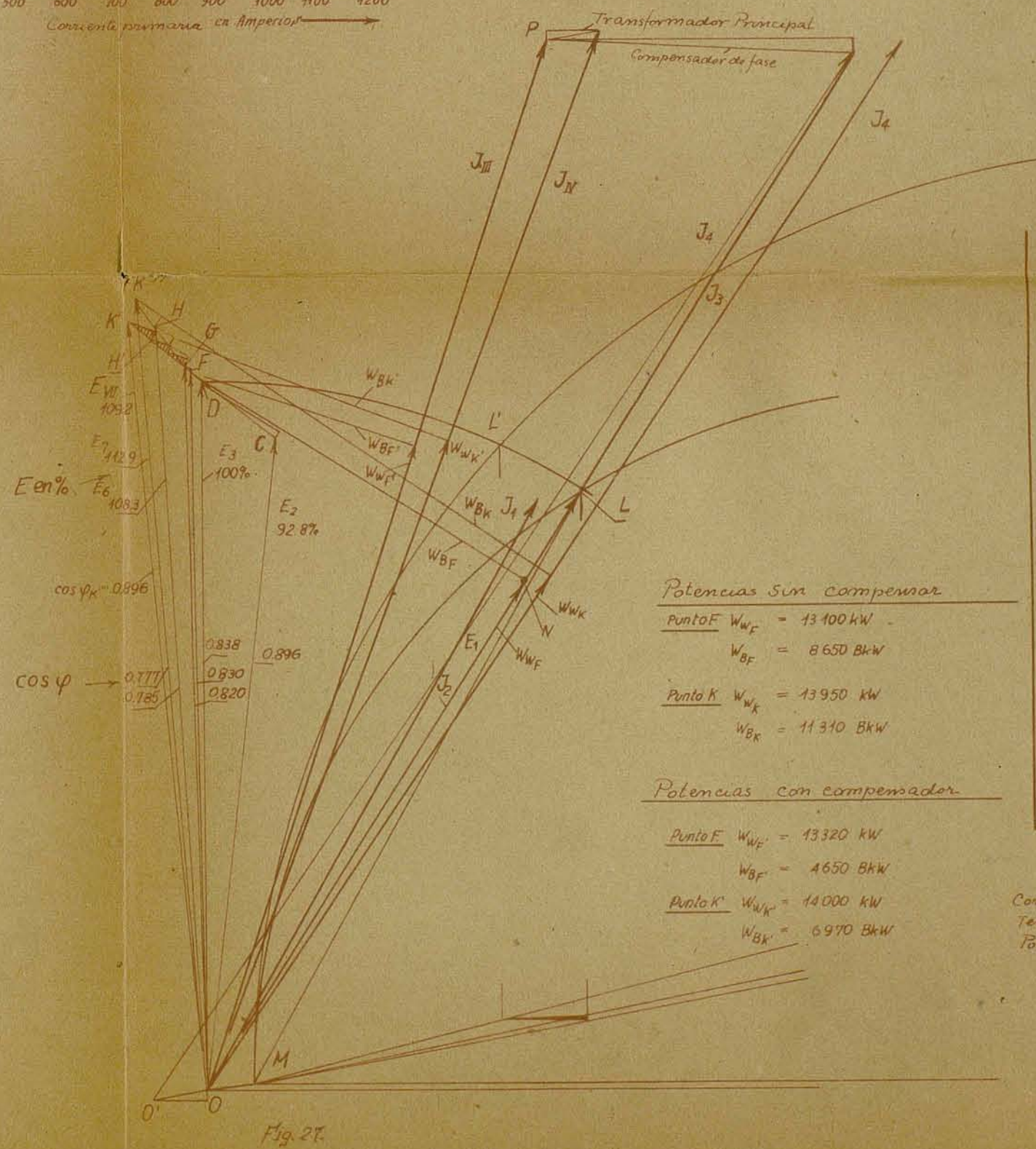
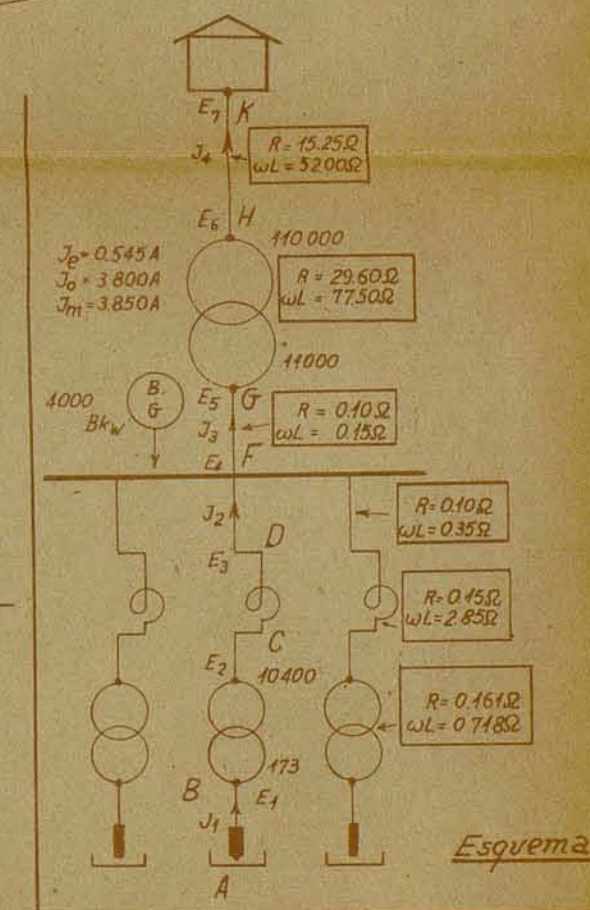


Fig. 27.



Esquema

Potencias sin compensar

Punto F  $W_{WF} = 13400 \text{ kW}$   
 $W_{BF} = 8650 \text{ BkW}$   
 Punto K  $W_{WK} = 13950 \text{ kW}$   
 $W_{BK} = 11310 \text{ BkW}$

Potencias con compensador

Punto F  $W_{WF} = 13320 \text{ kW}$   
 $W_{BF} = 4650 \text{ BkW}$   
 Punto K  $W_{WK} = 14000 \text{ kW}$   
 $W_{BK} = 6970 \text{ BkW}$

Escala

Corriente 1mm = 2 Amperios  
 Tension 1mm = 416 Voltios  
 Potencia 1mm<sup>2</sup> = 2 x 416 = 832 Watios

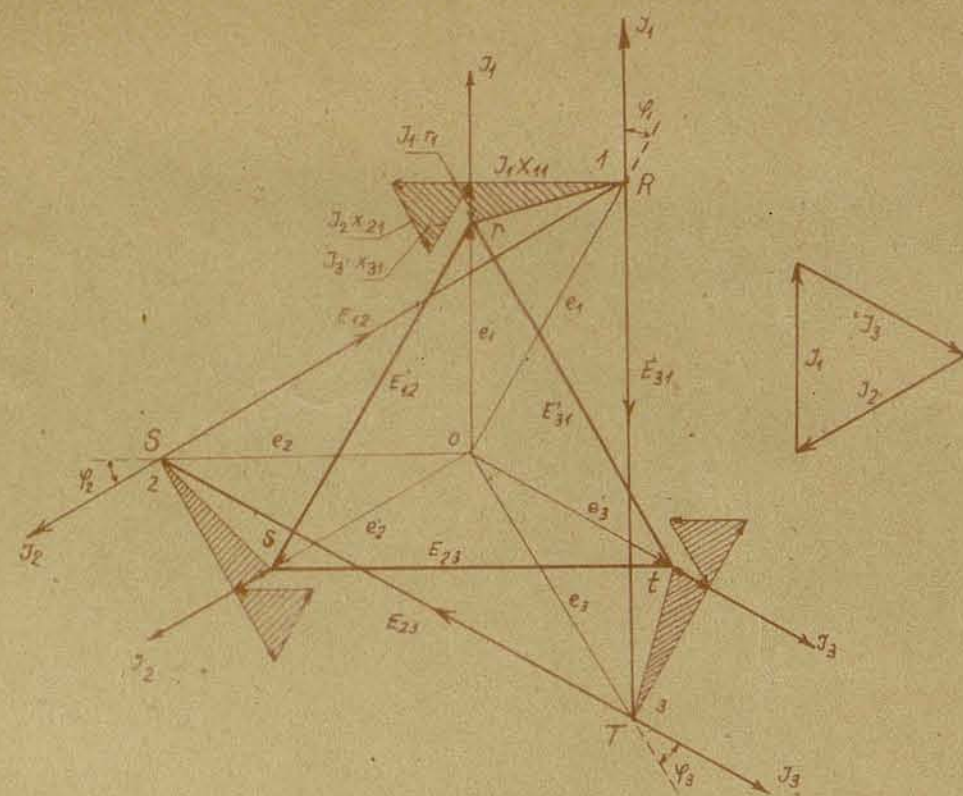


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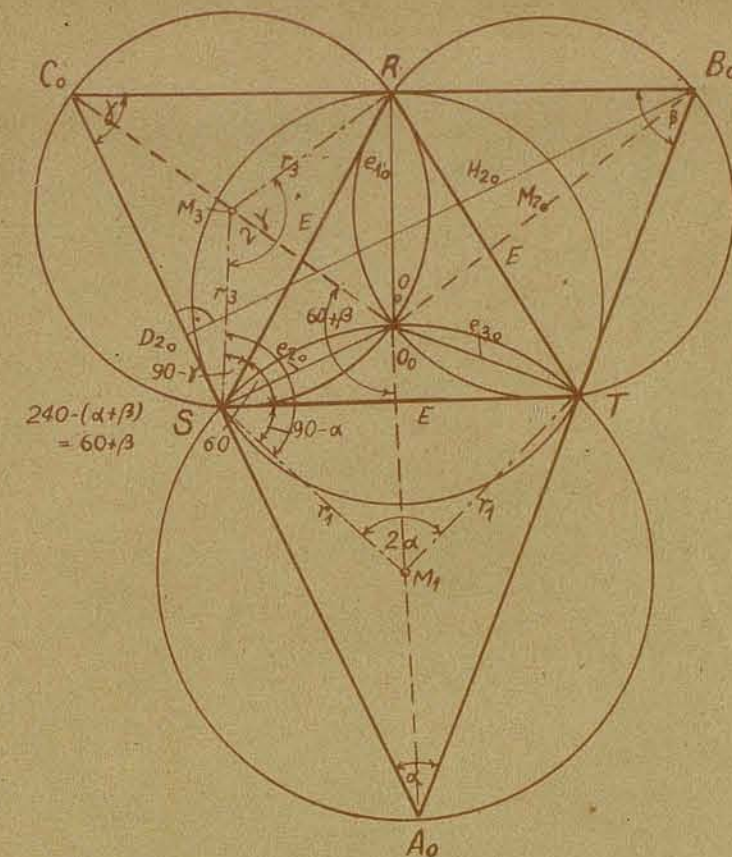
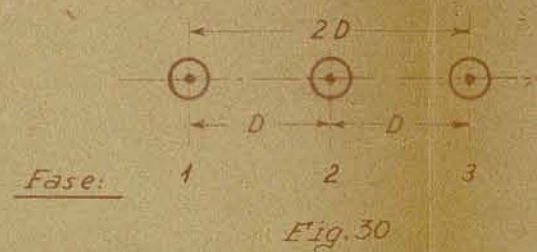
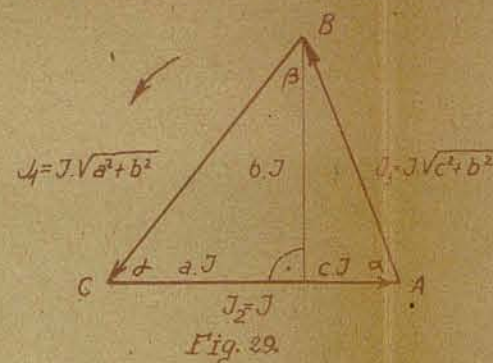


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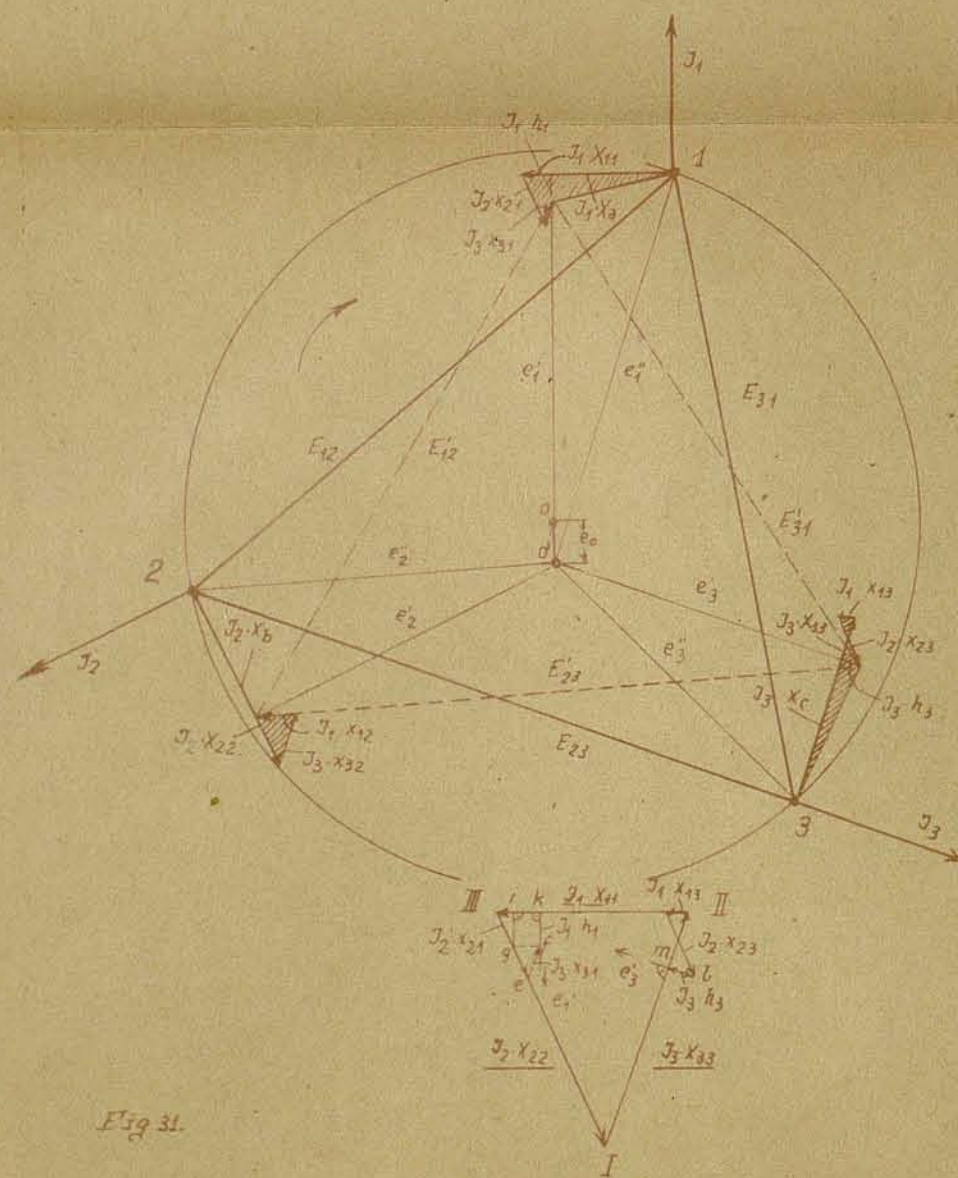


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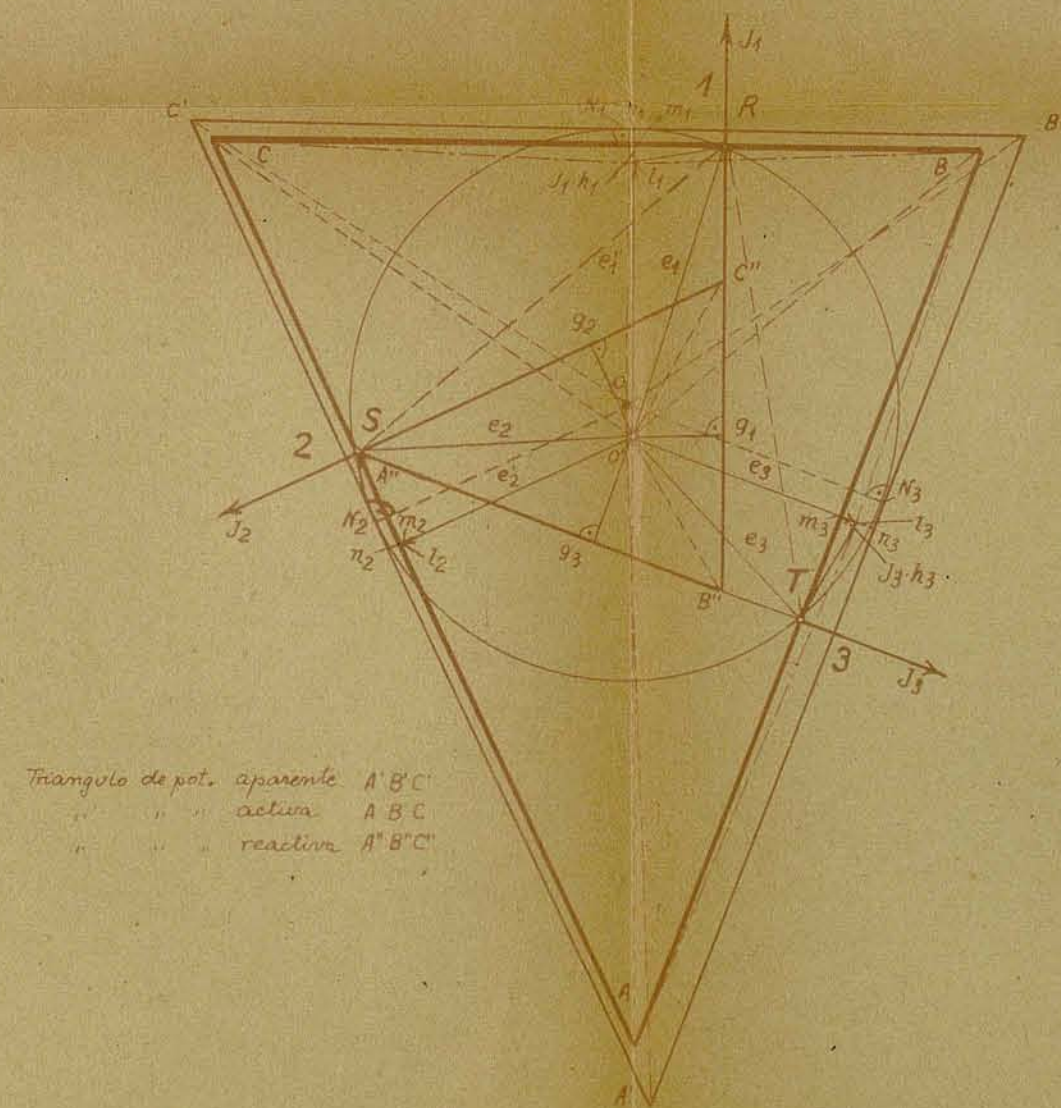
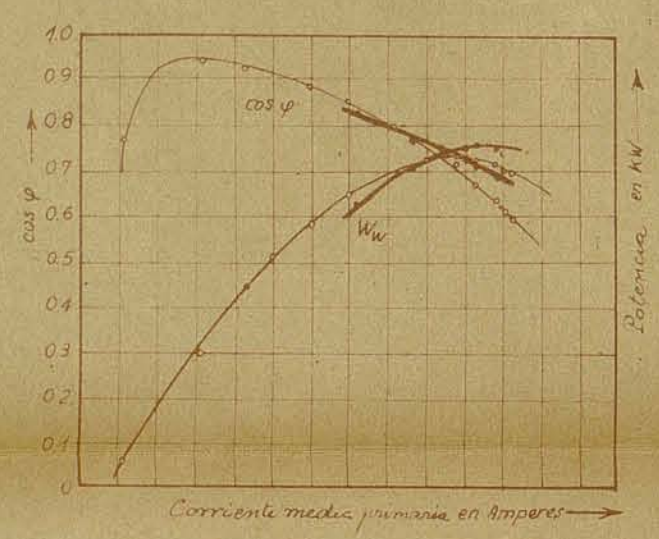
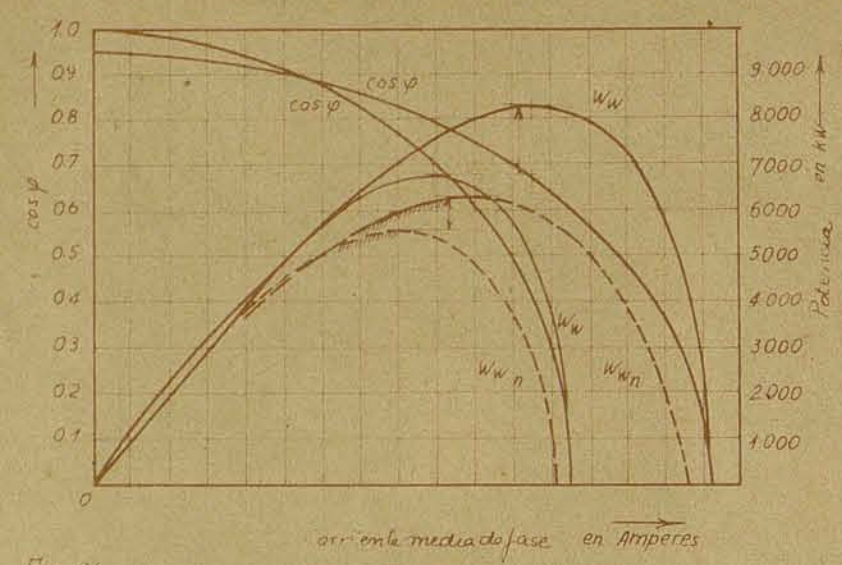
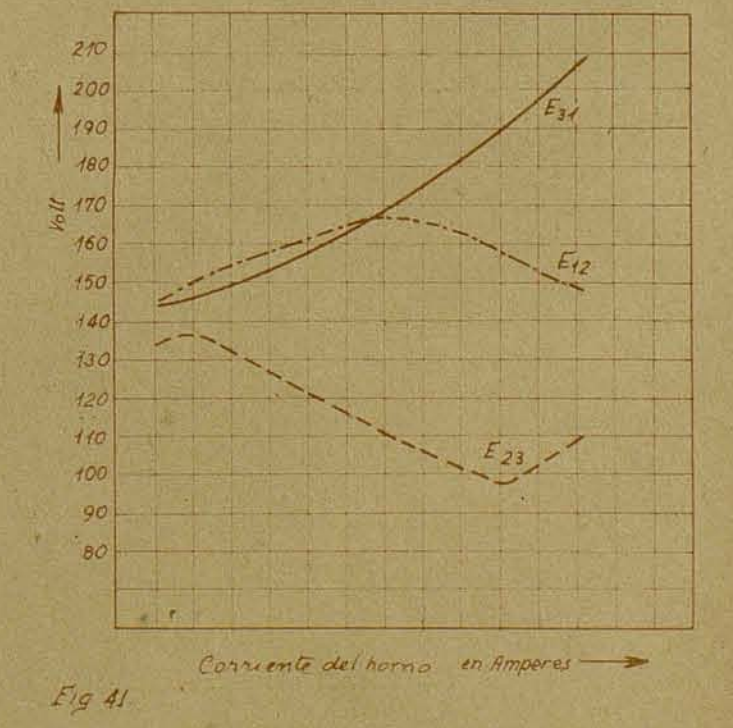
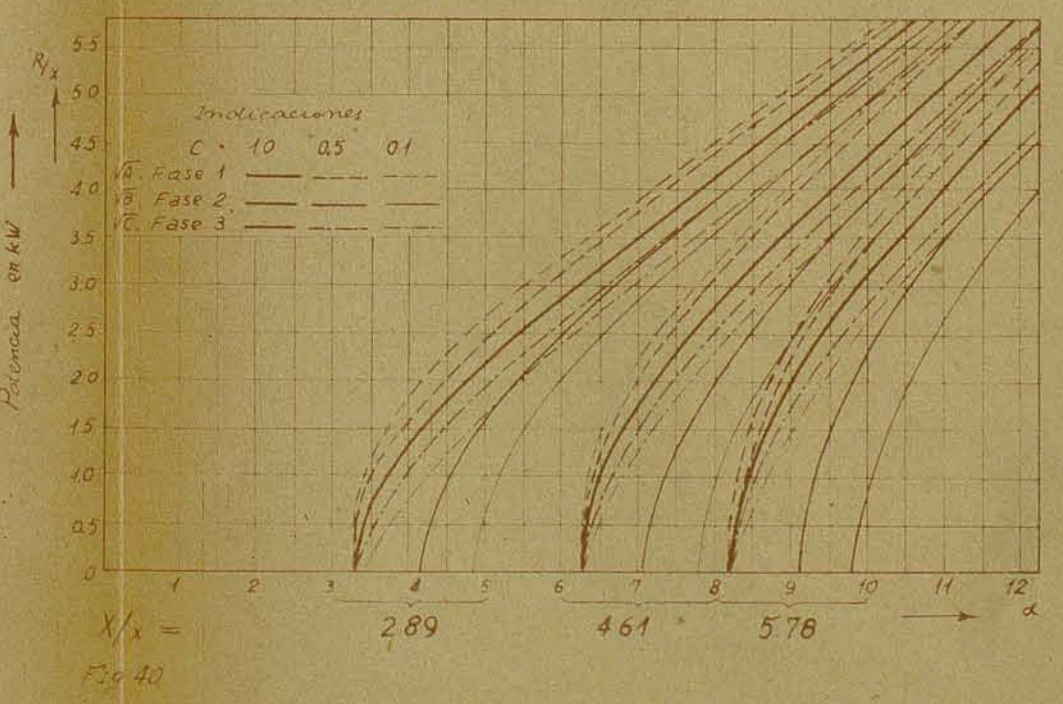
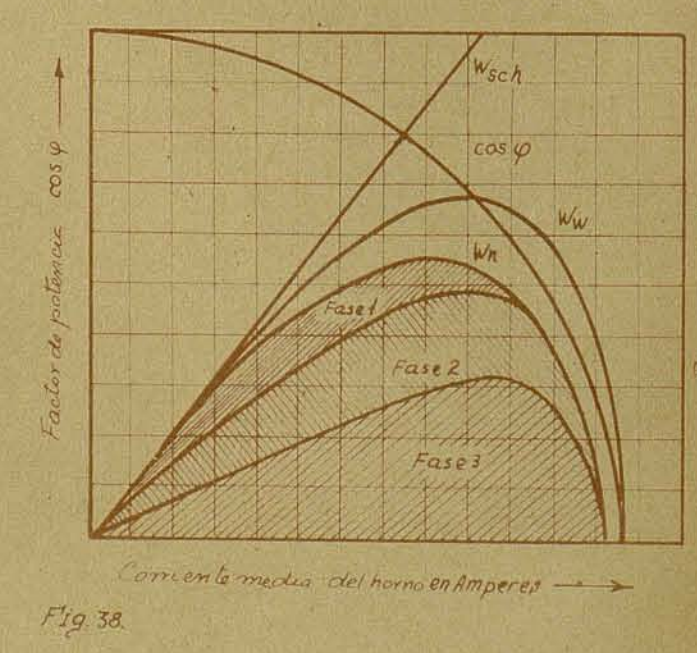
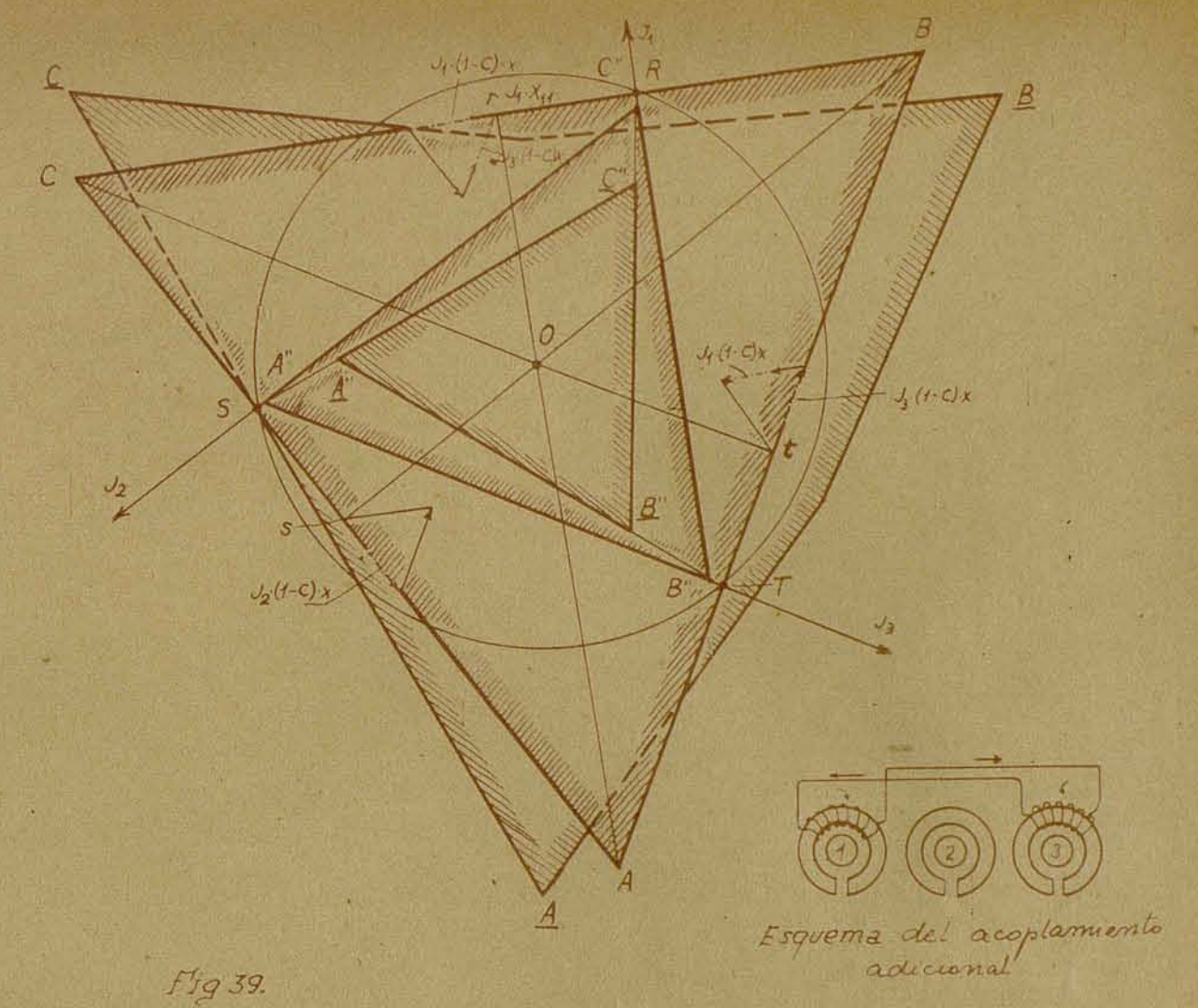
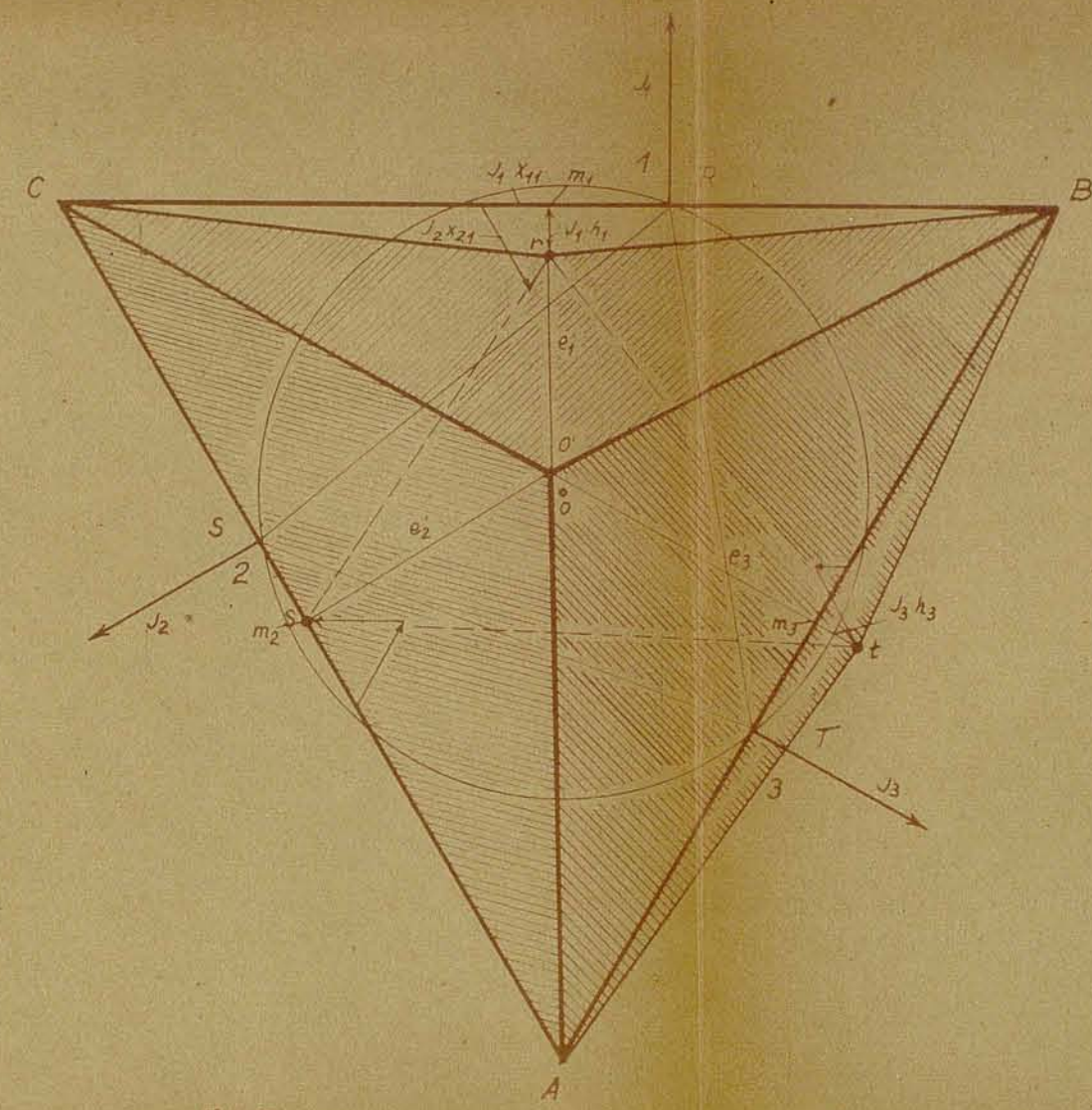
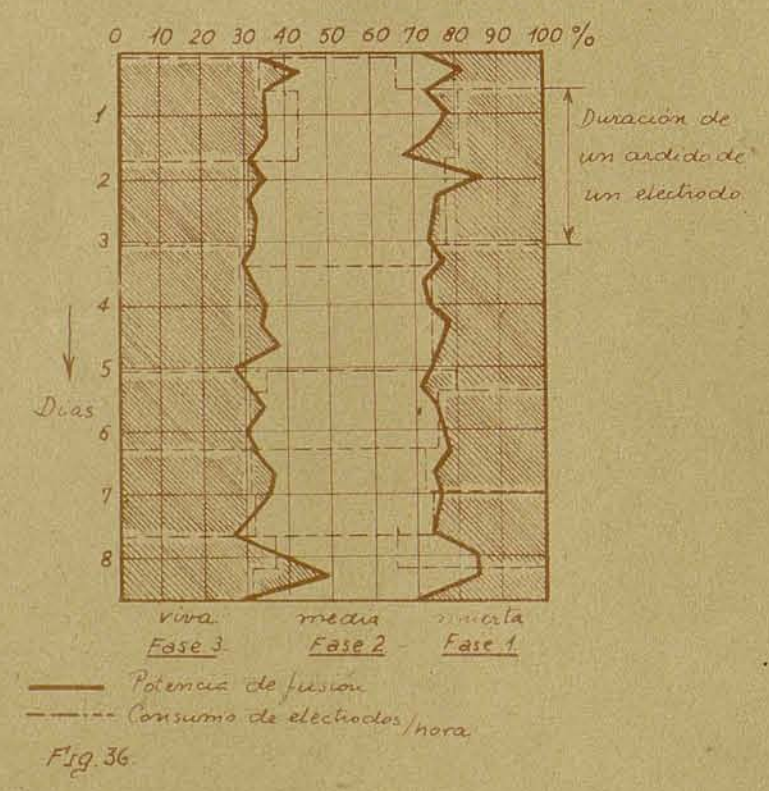
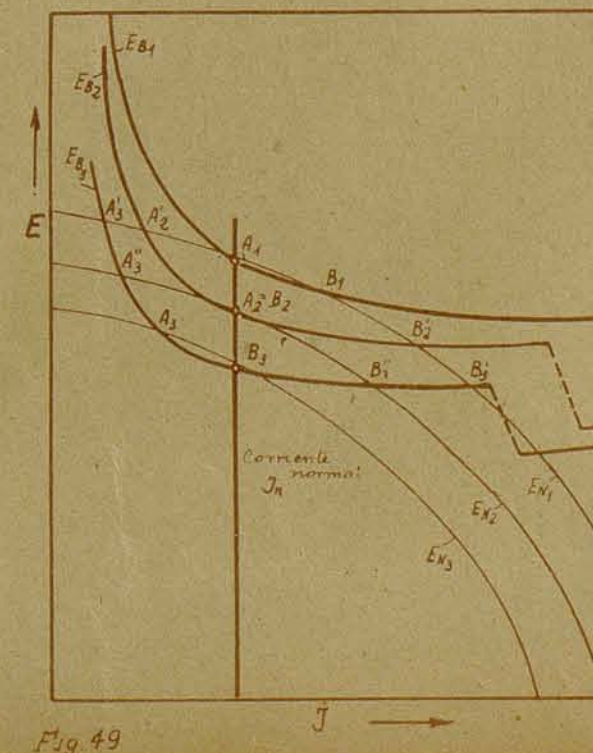
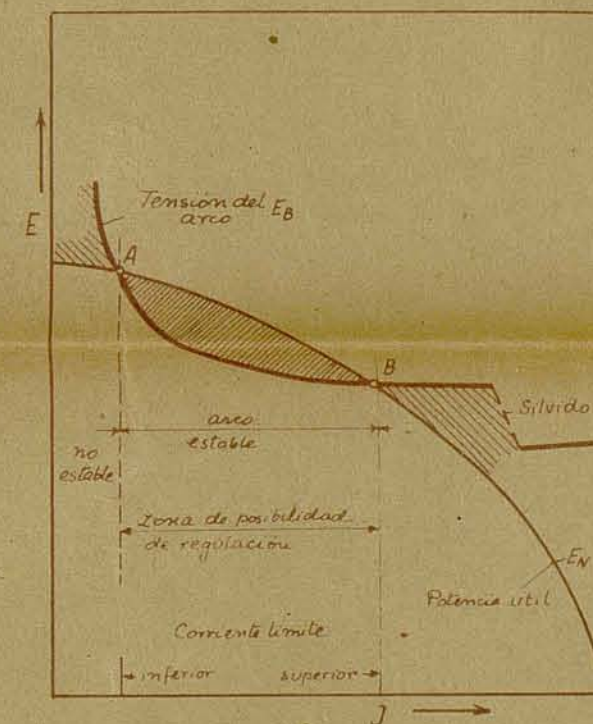
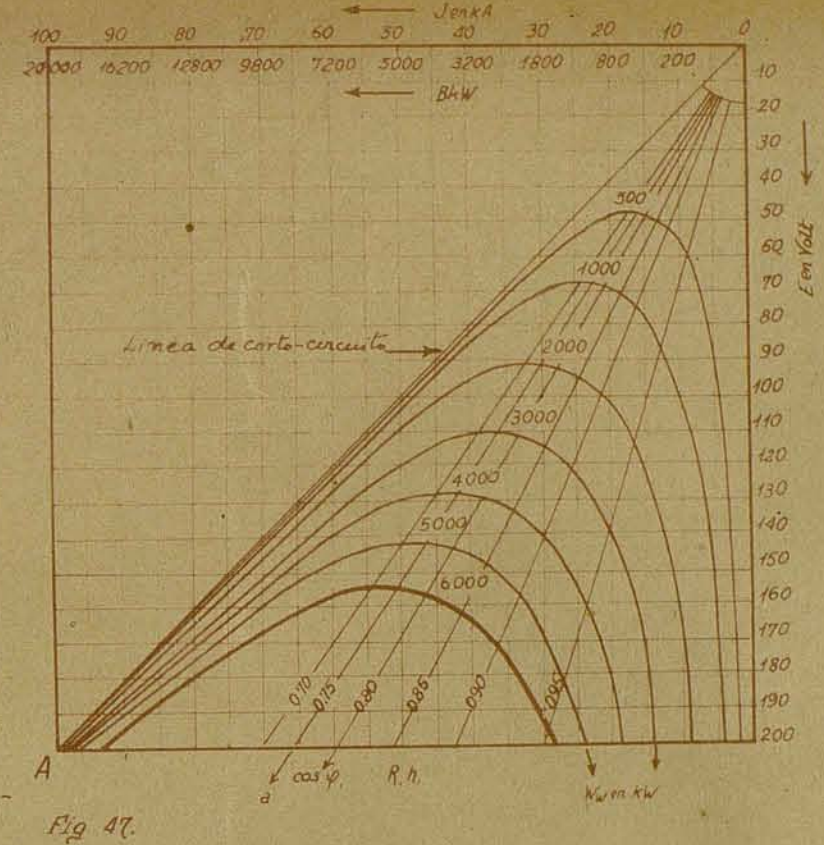
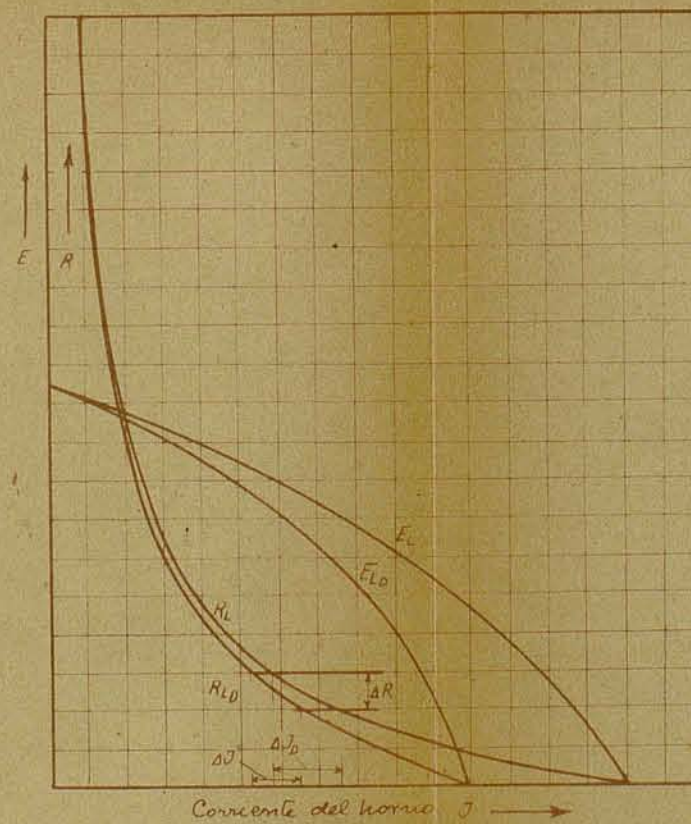
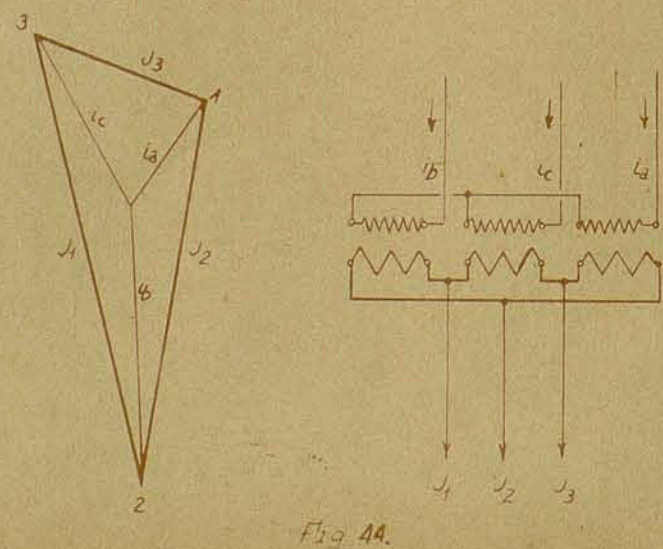
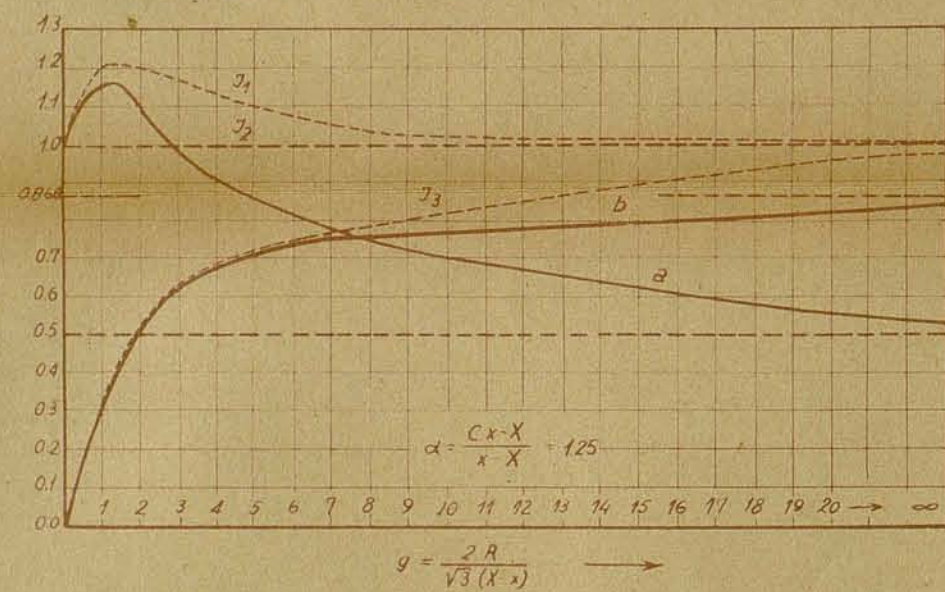
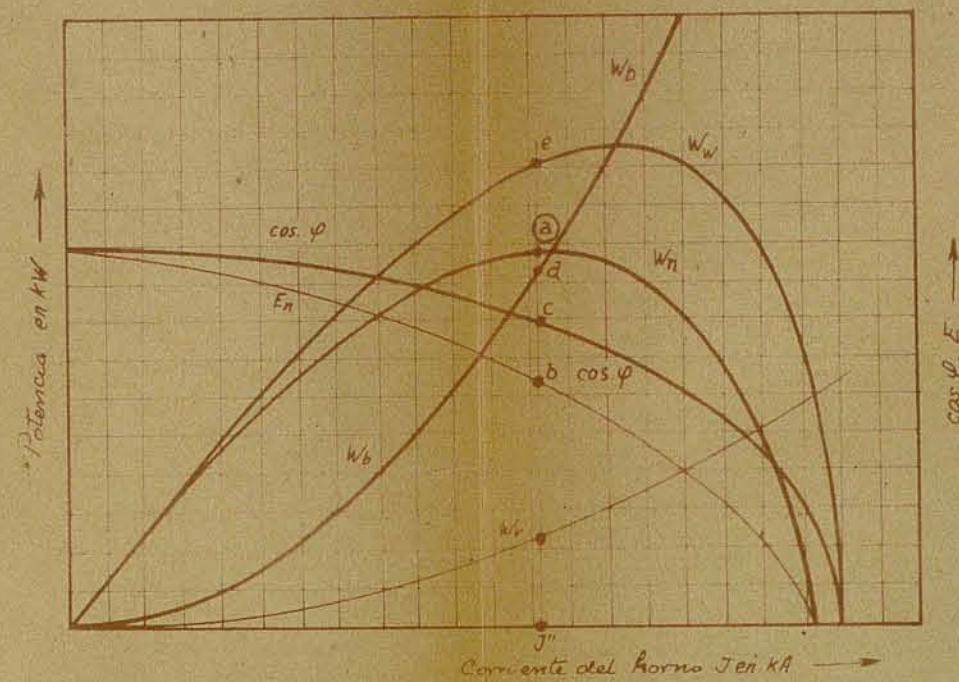
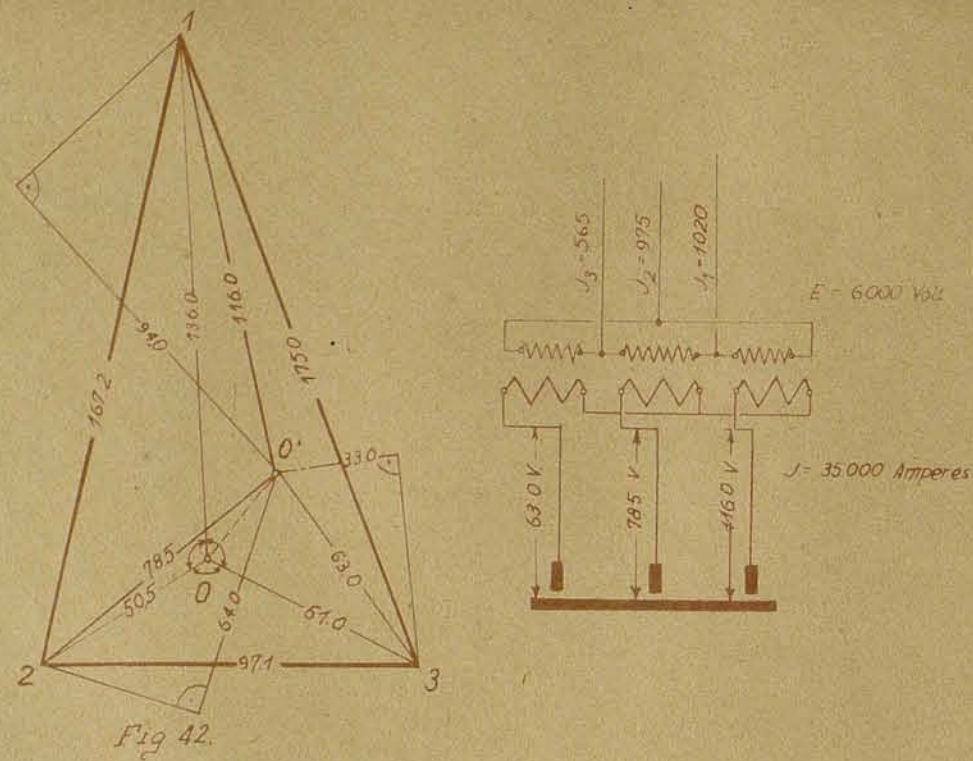


Fig. 32.



—●— Carga simétrica  
—●— Carga asimétrica





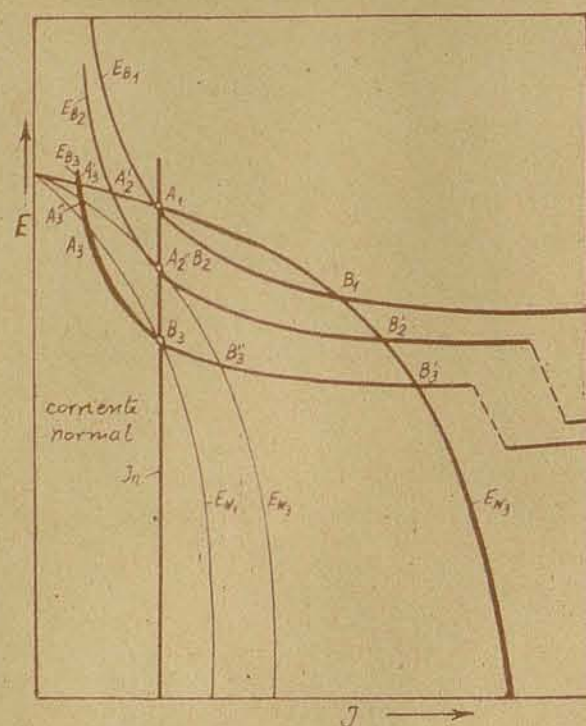


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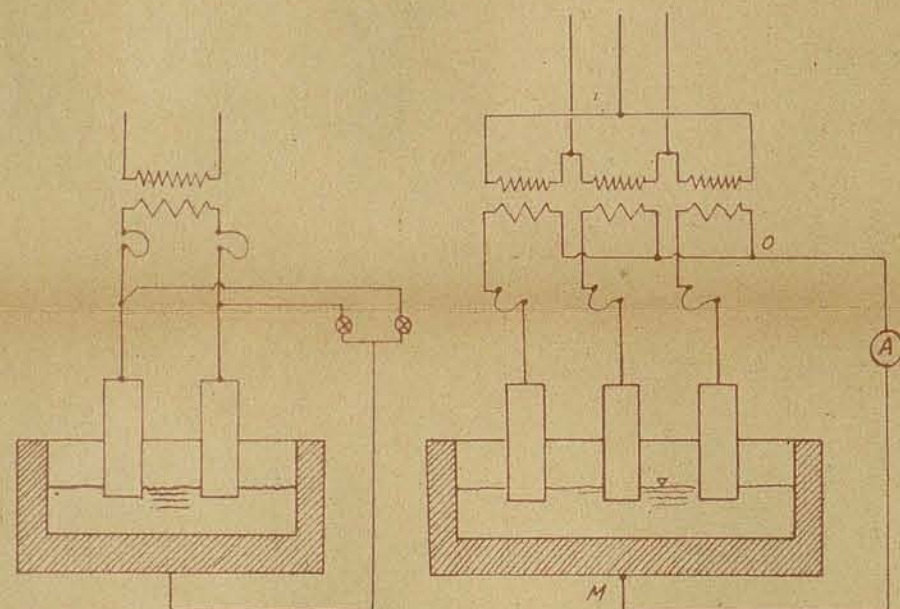


Fig. 51.

Fig. 52.

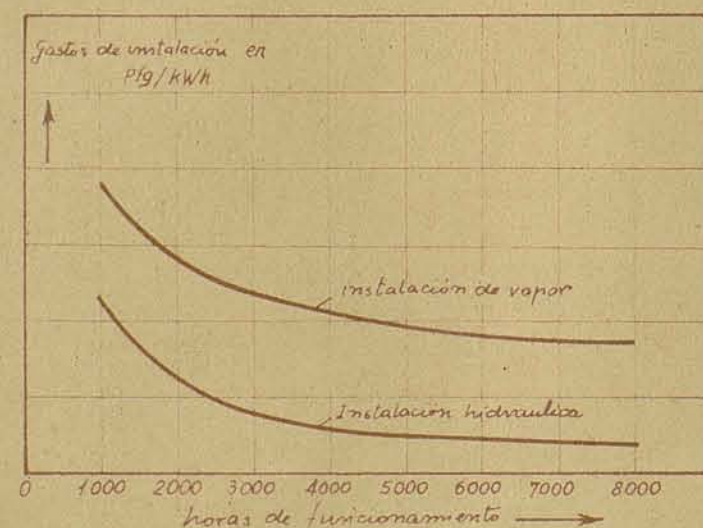


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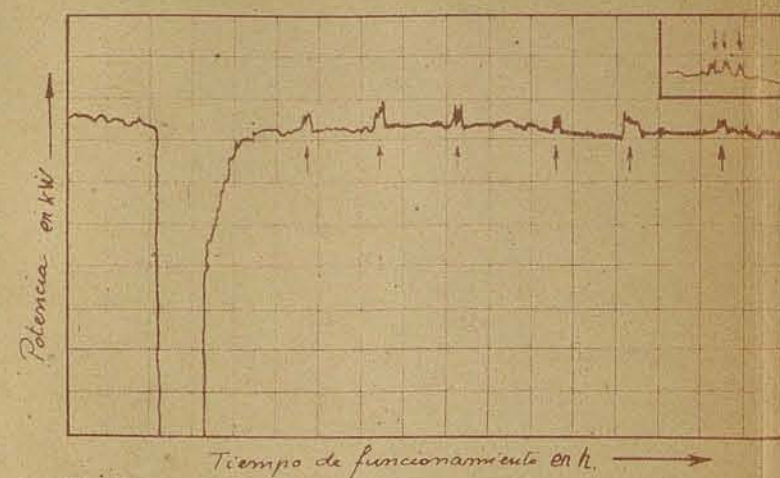


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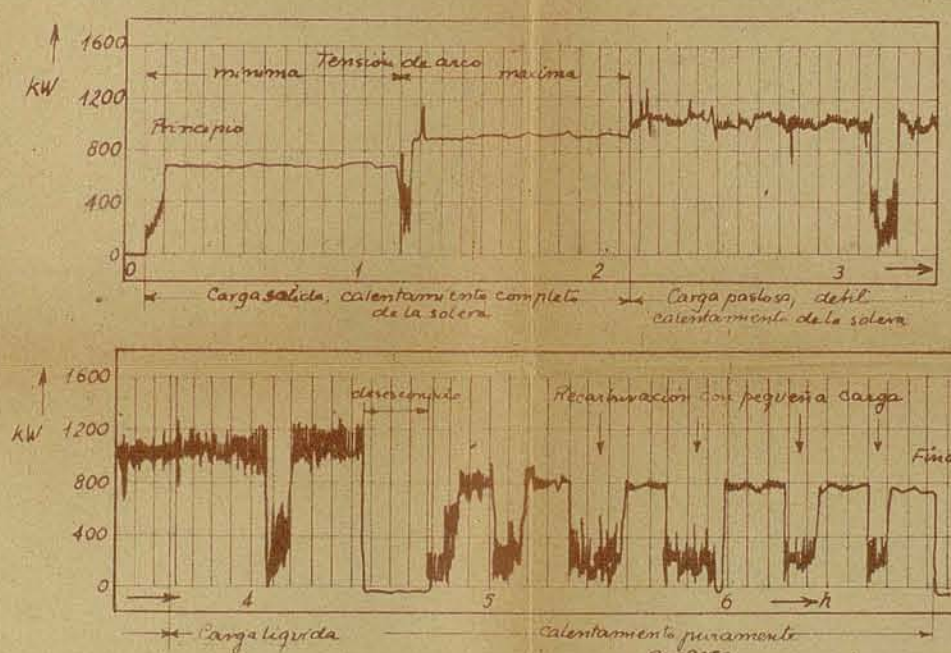


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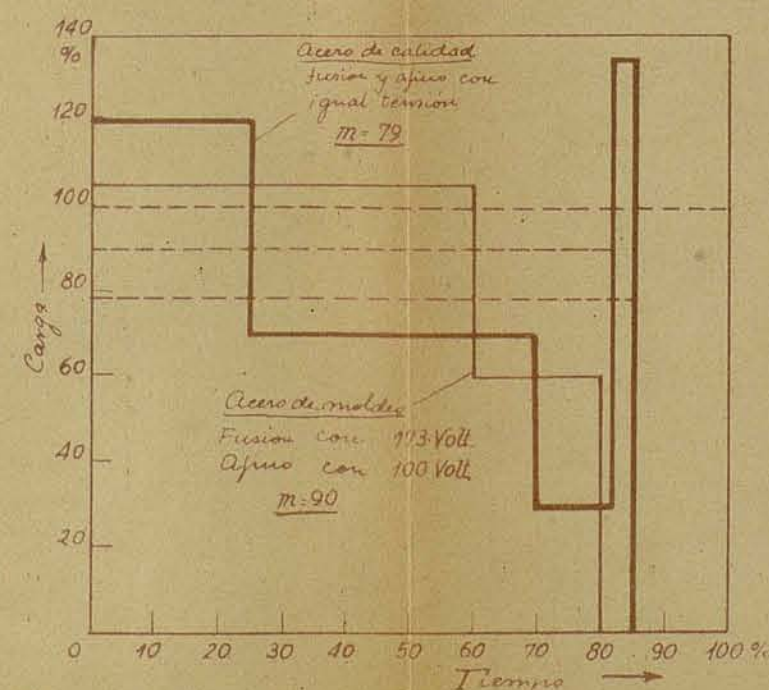


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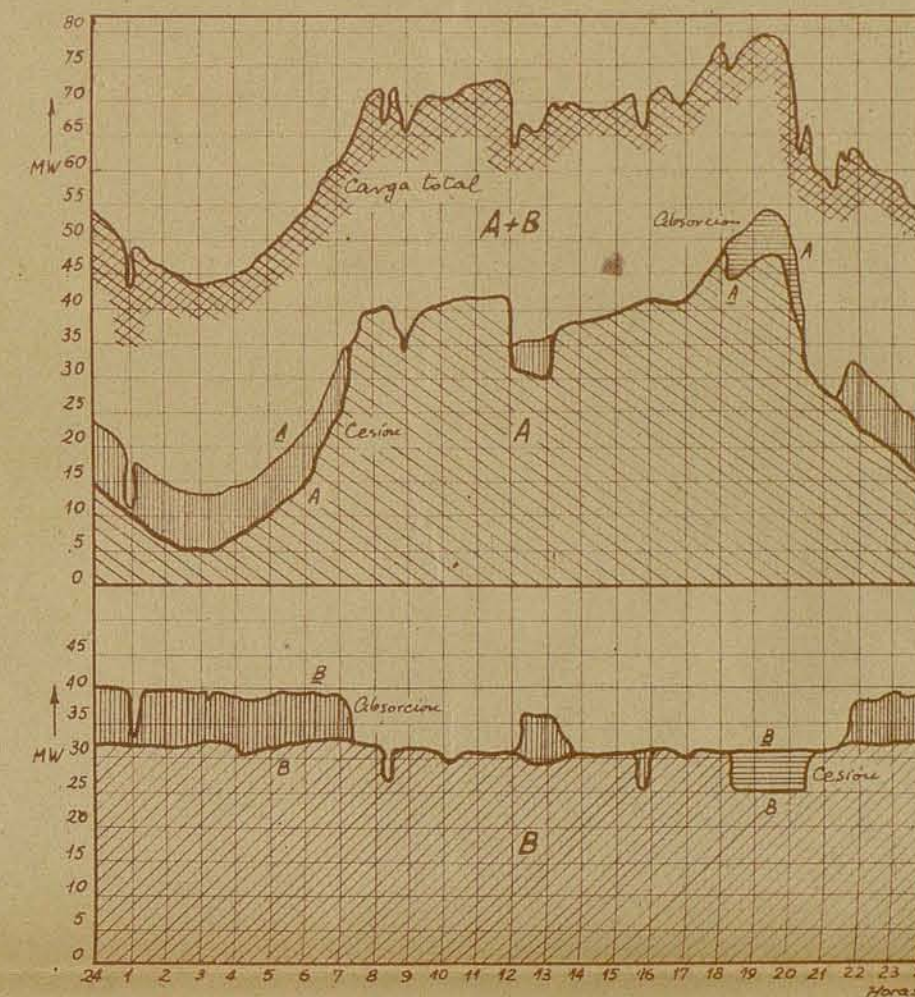


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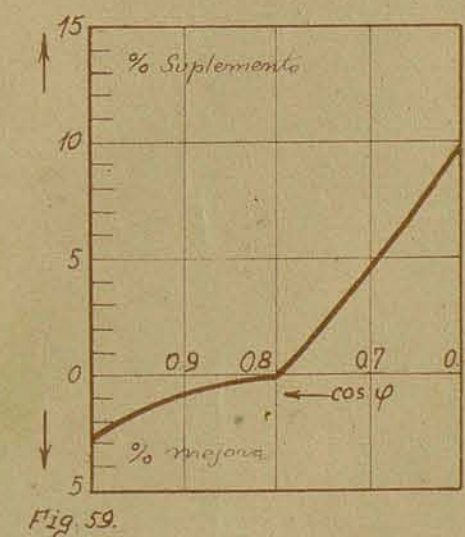
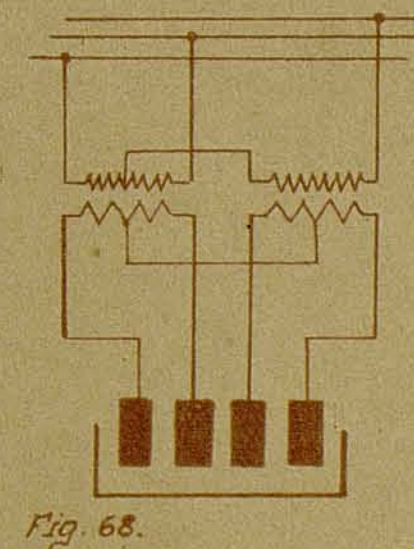
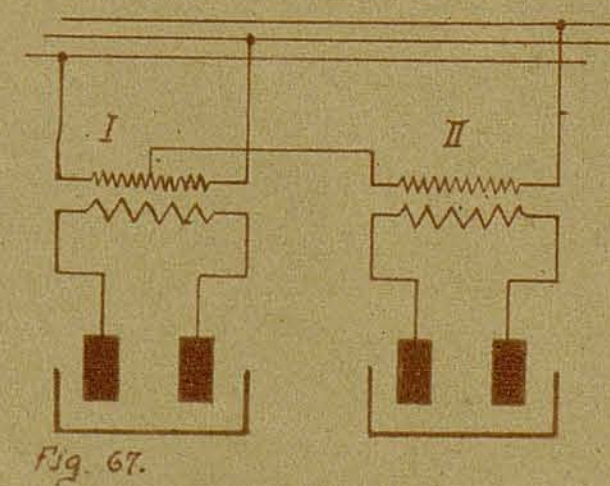
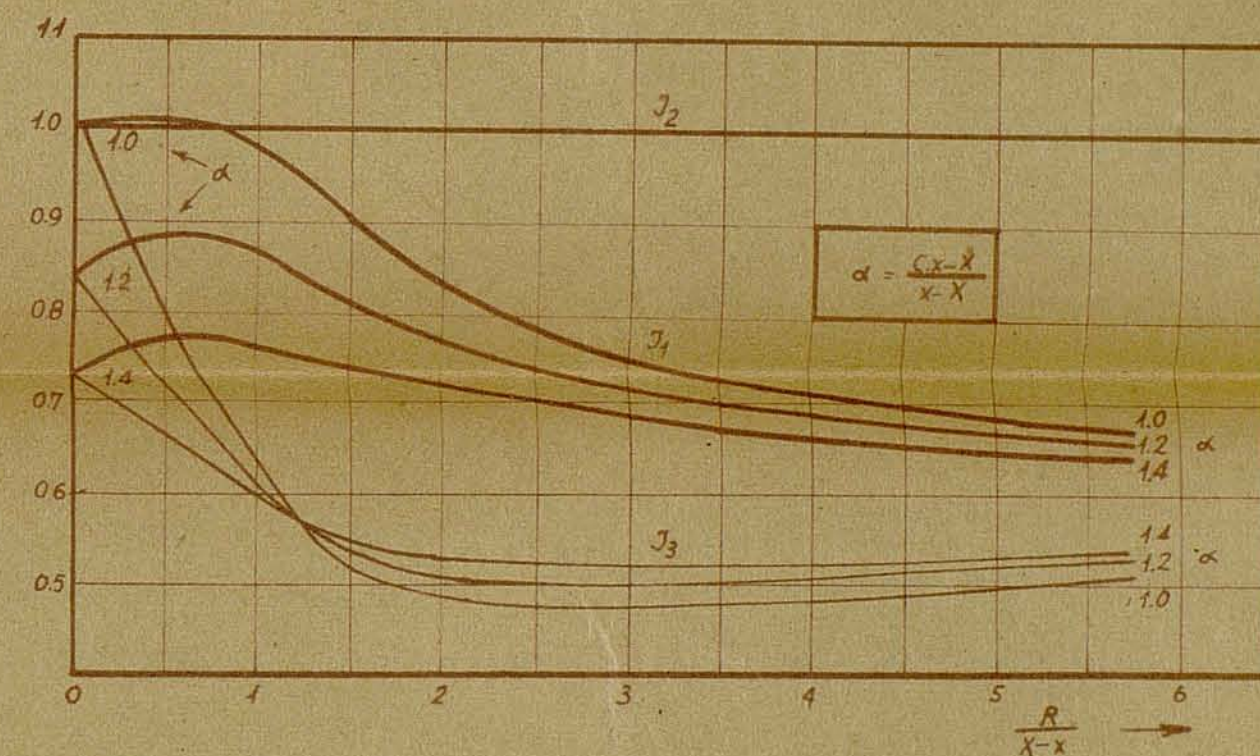
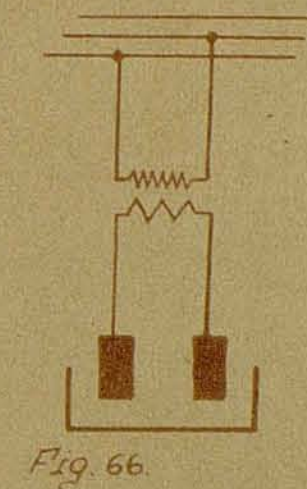
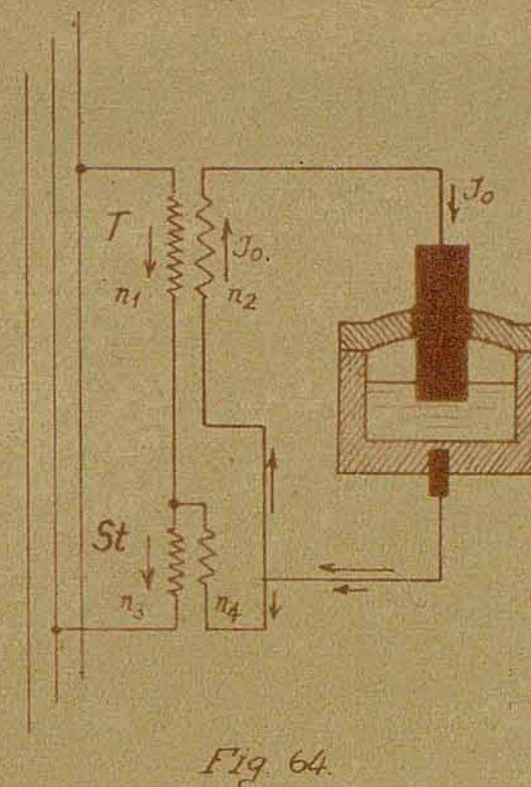
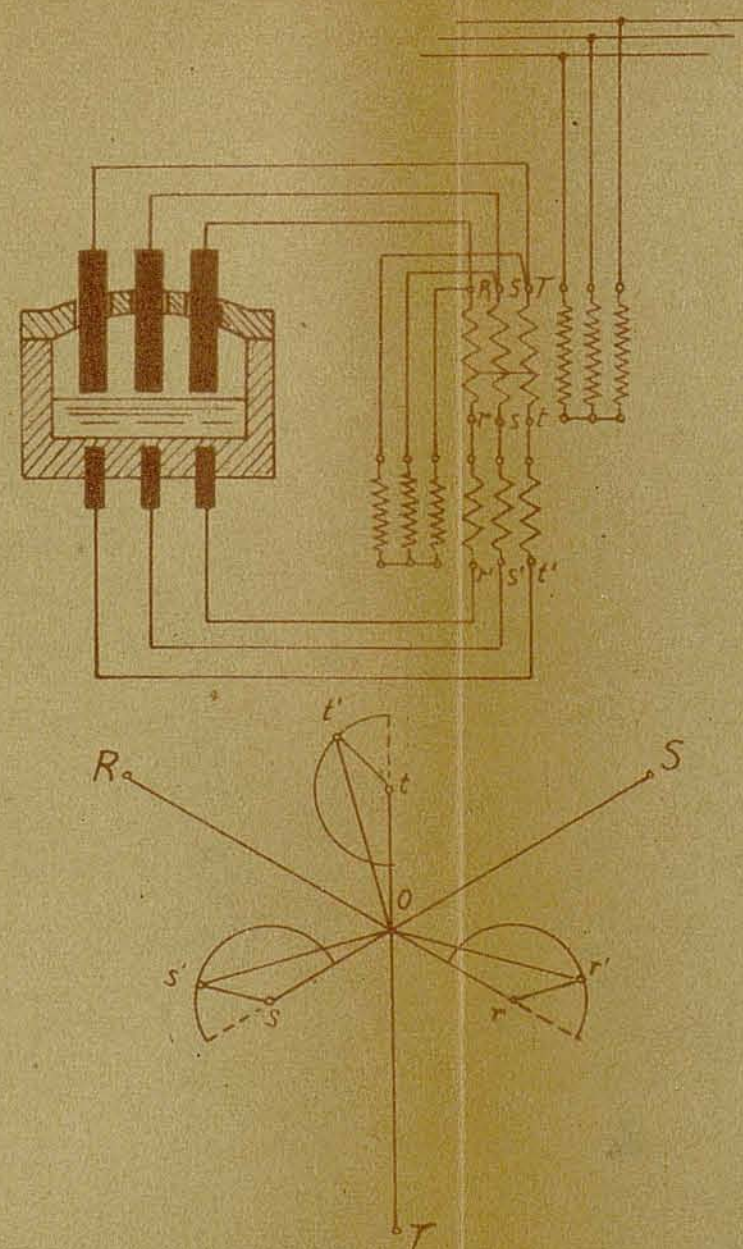
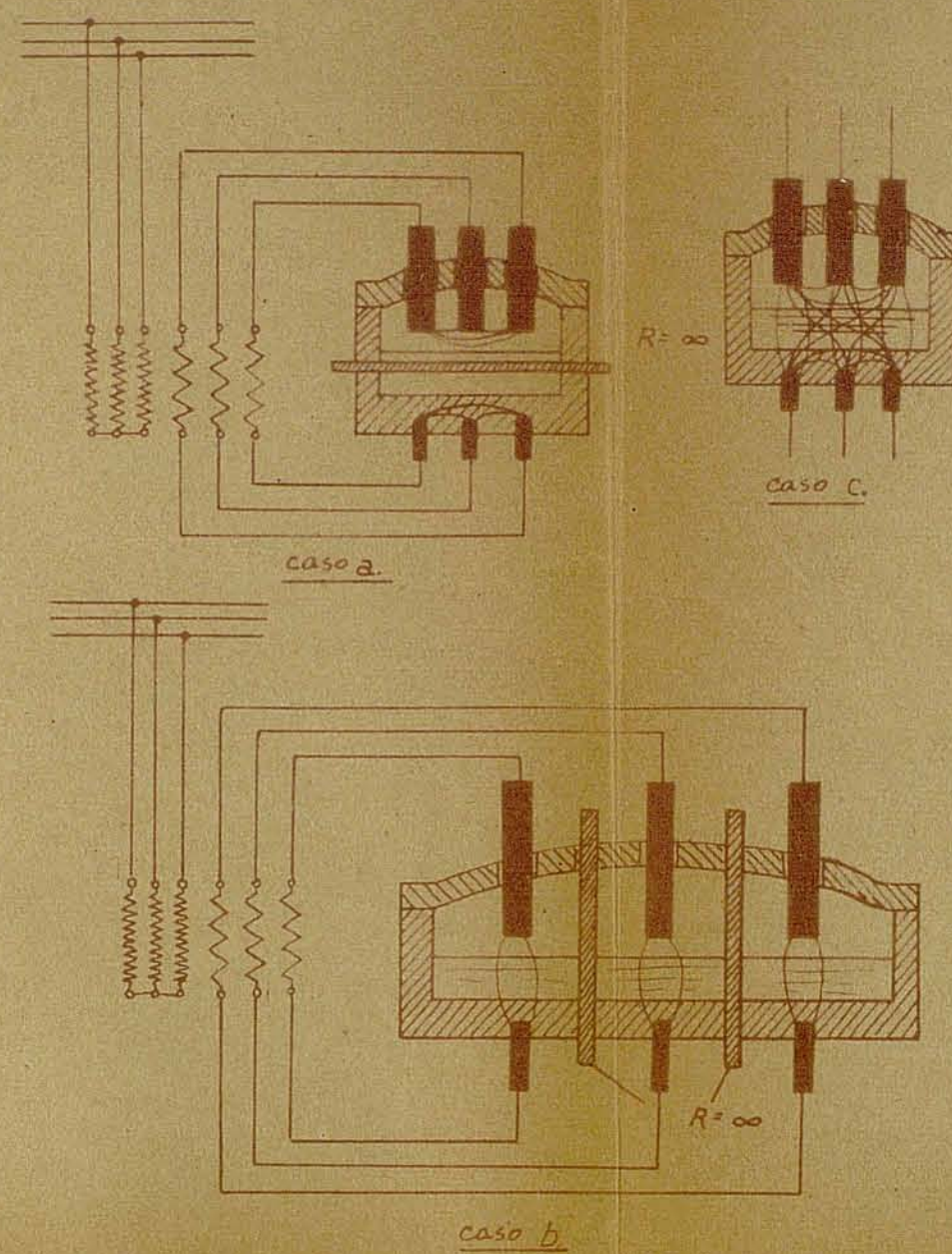
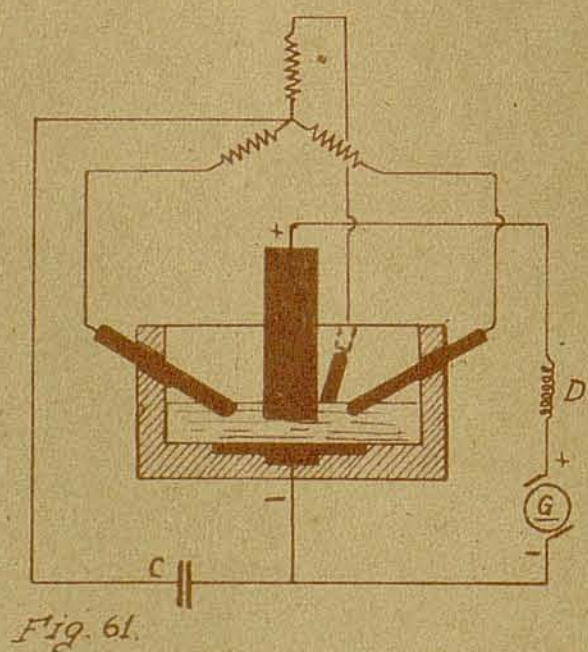
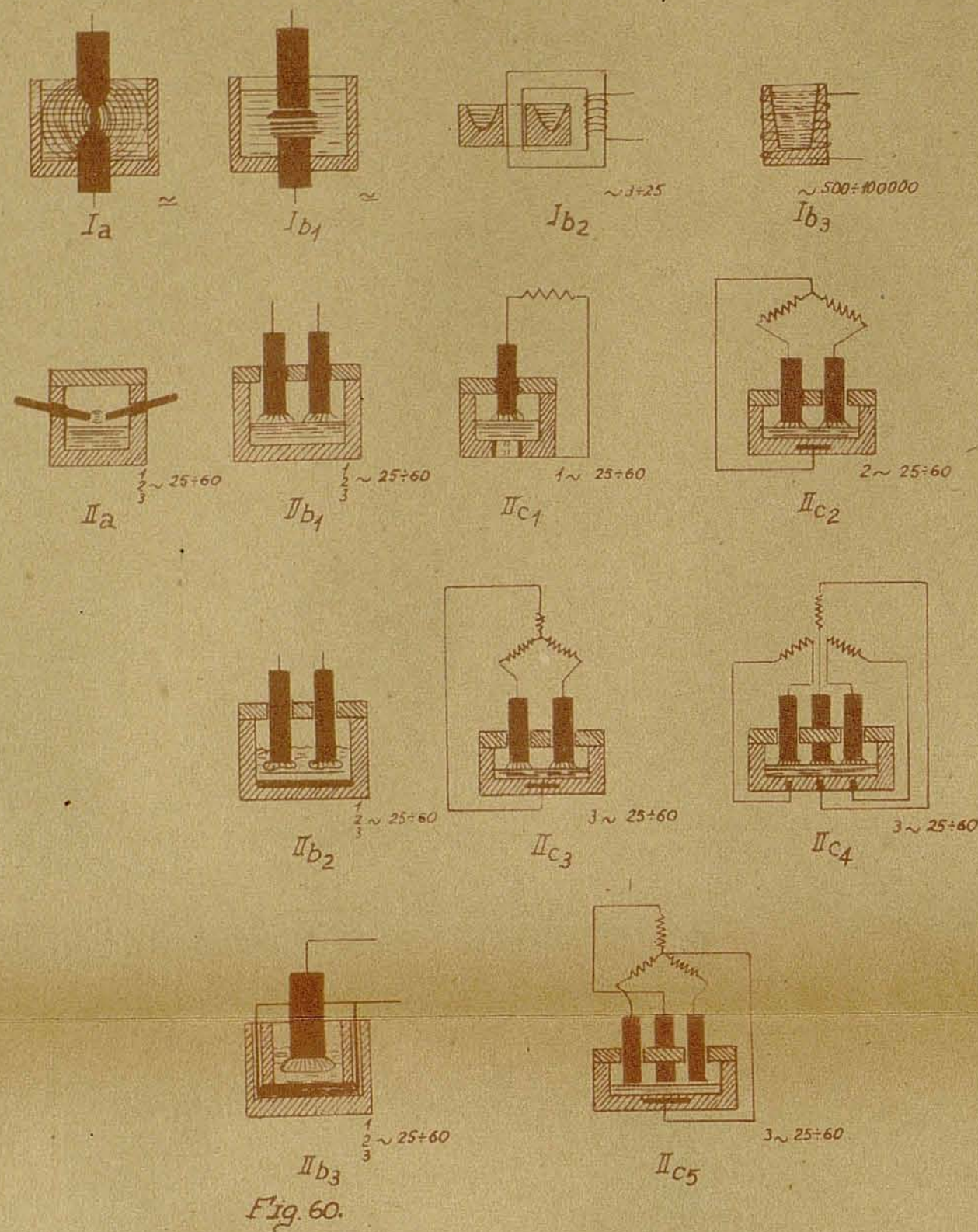


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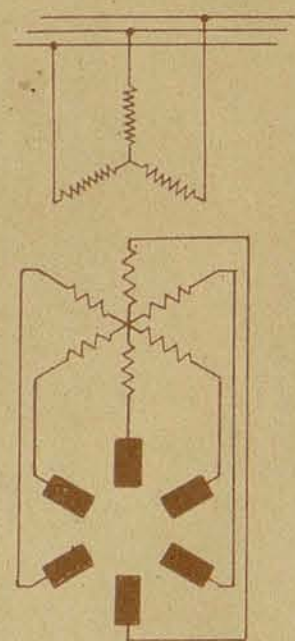


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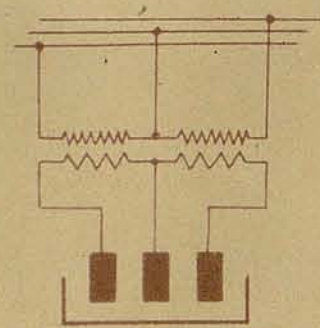


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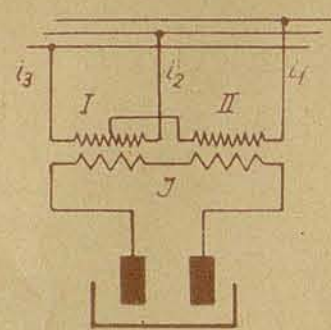


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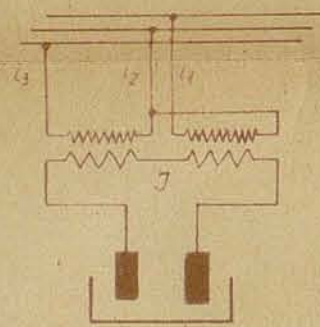


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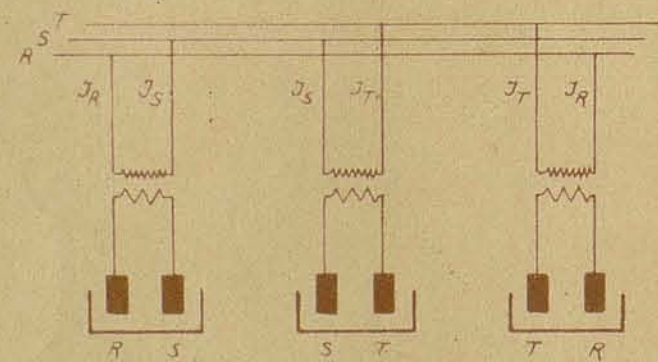


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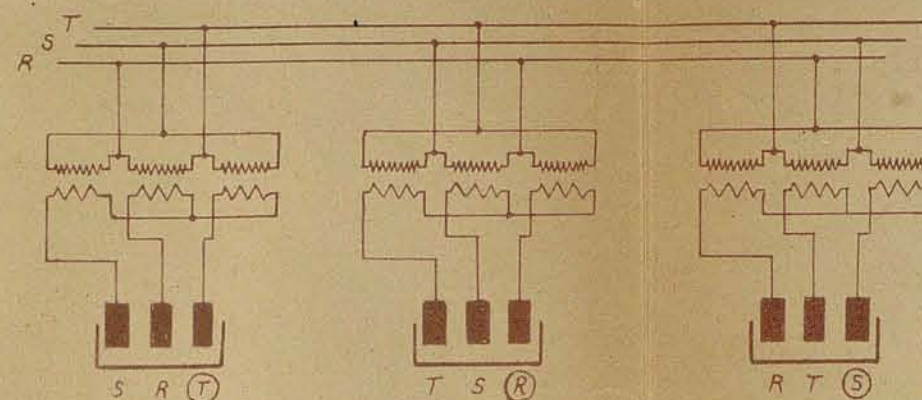


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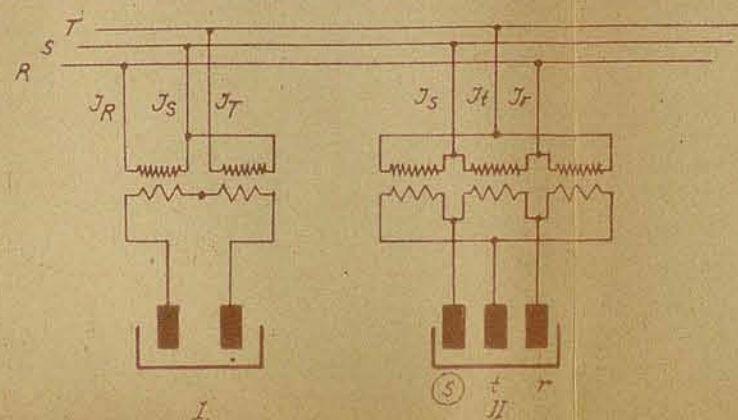


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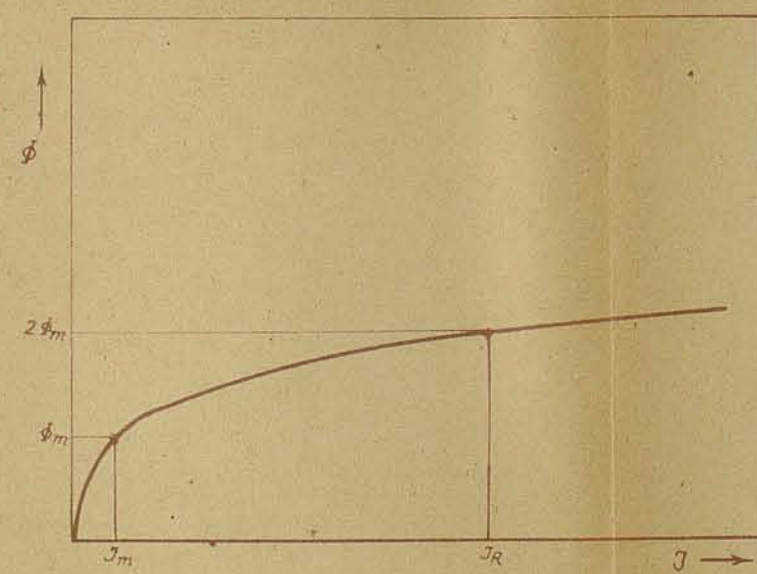


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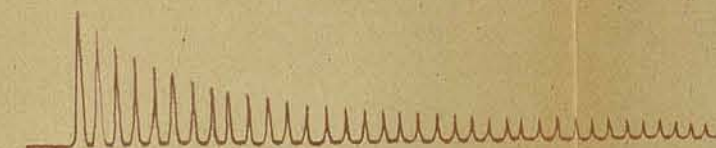


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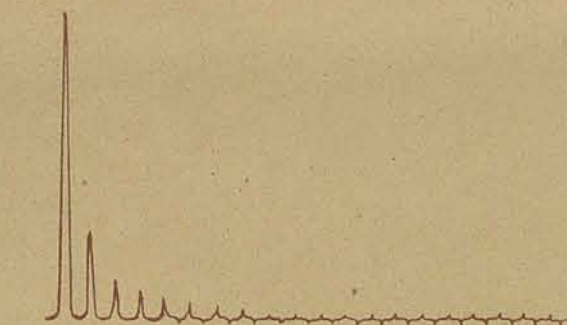


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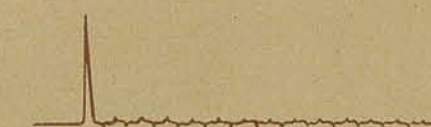


Fig. 79.



Fig. 80.

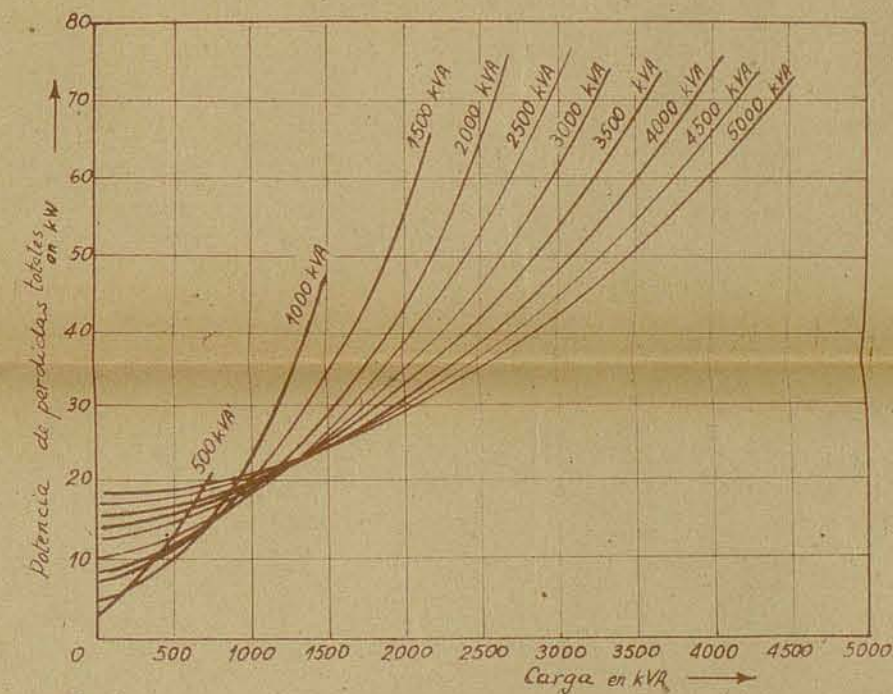


Fig. 81.

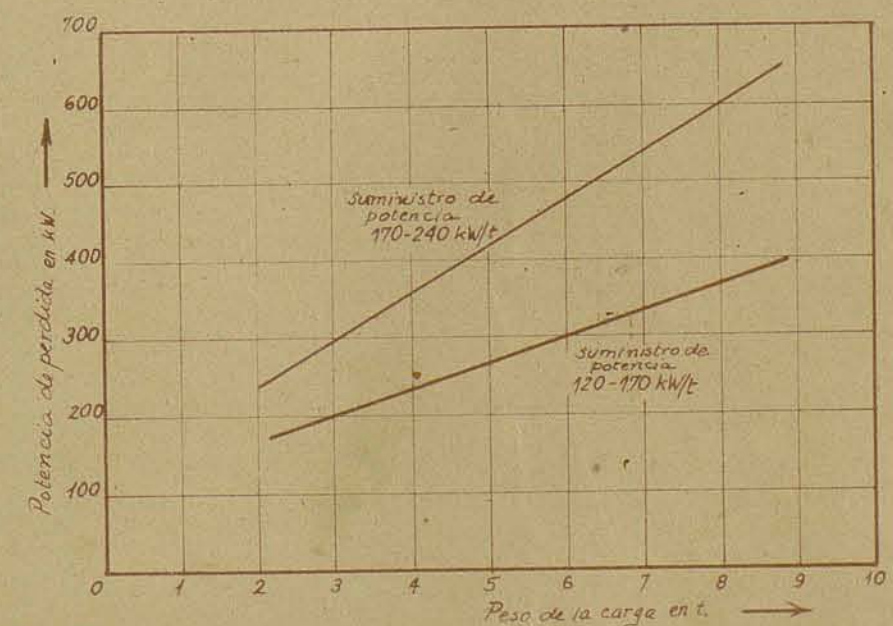
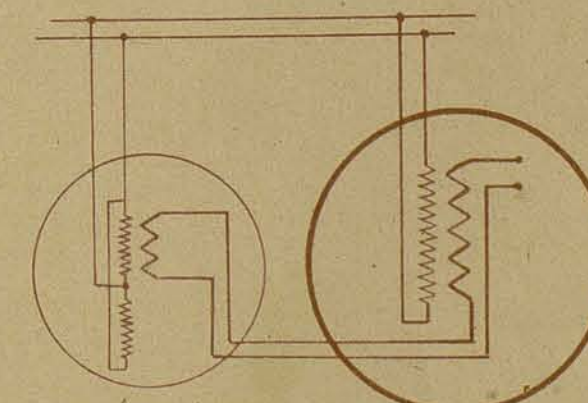
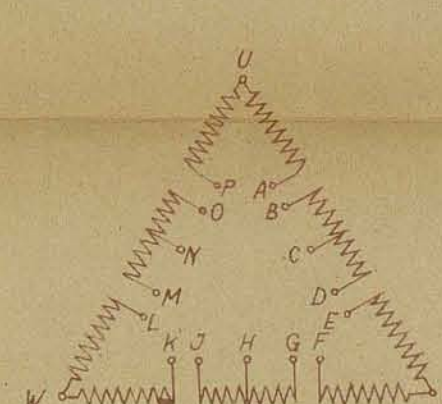
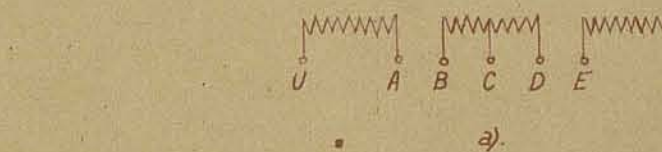
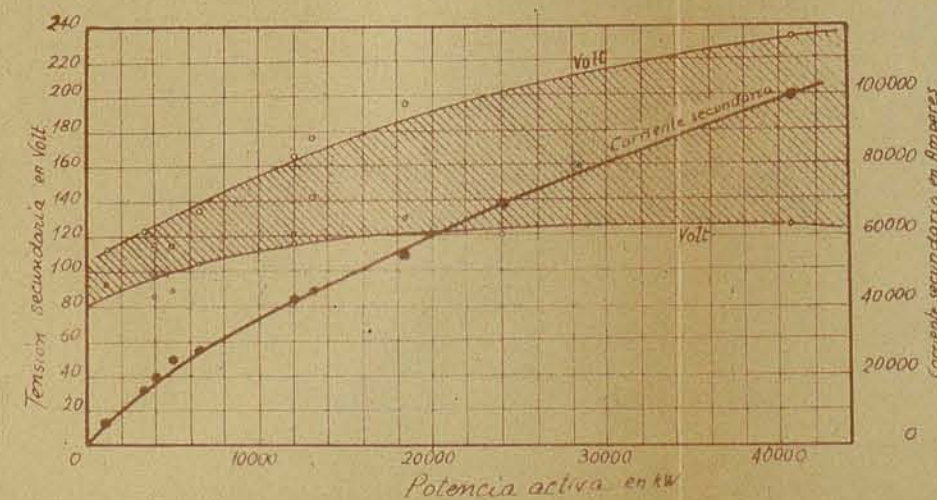
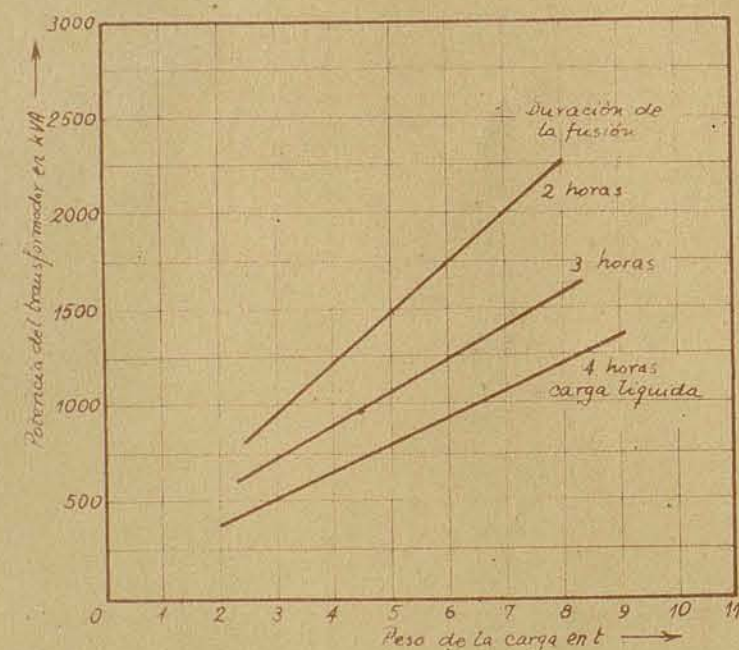
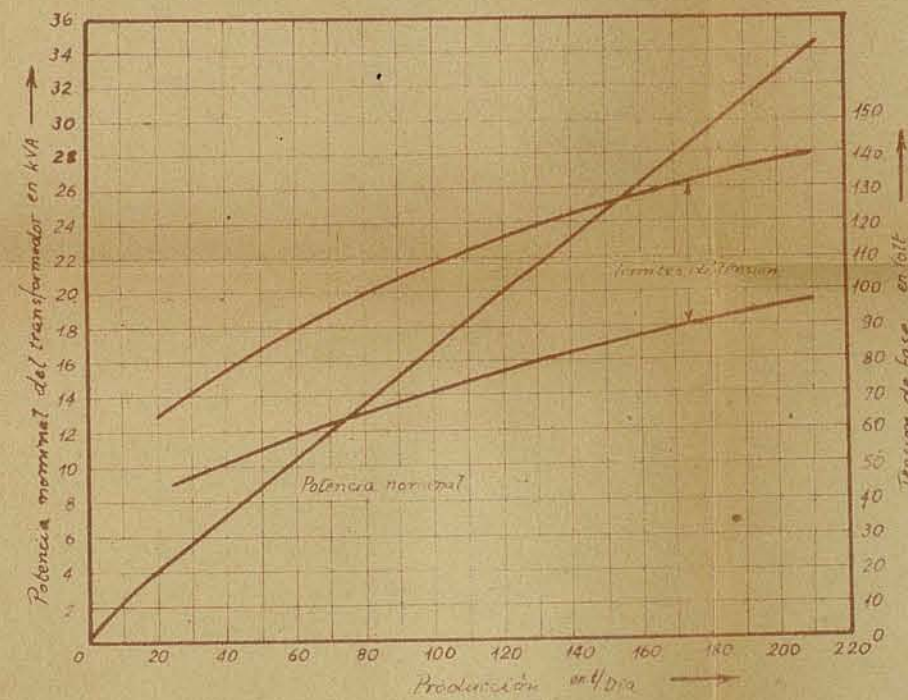
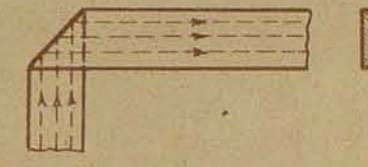
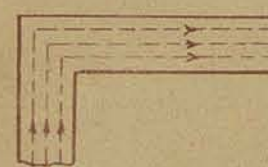
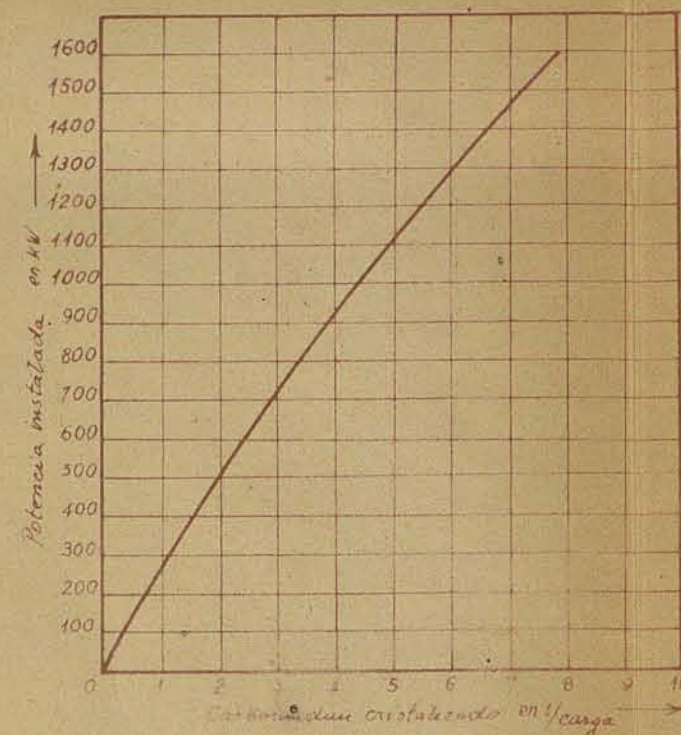
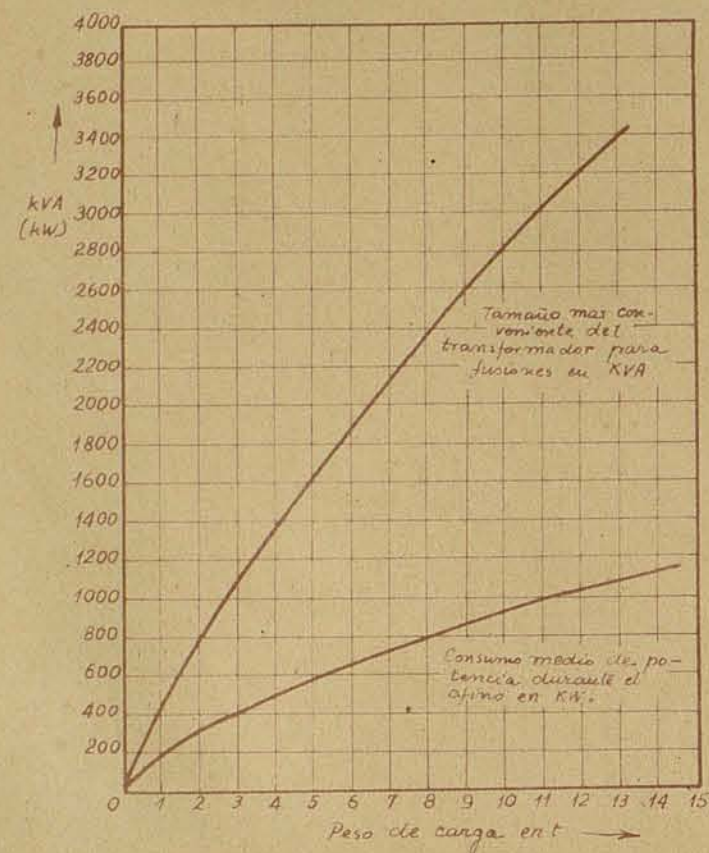


Fig. 82.



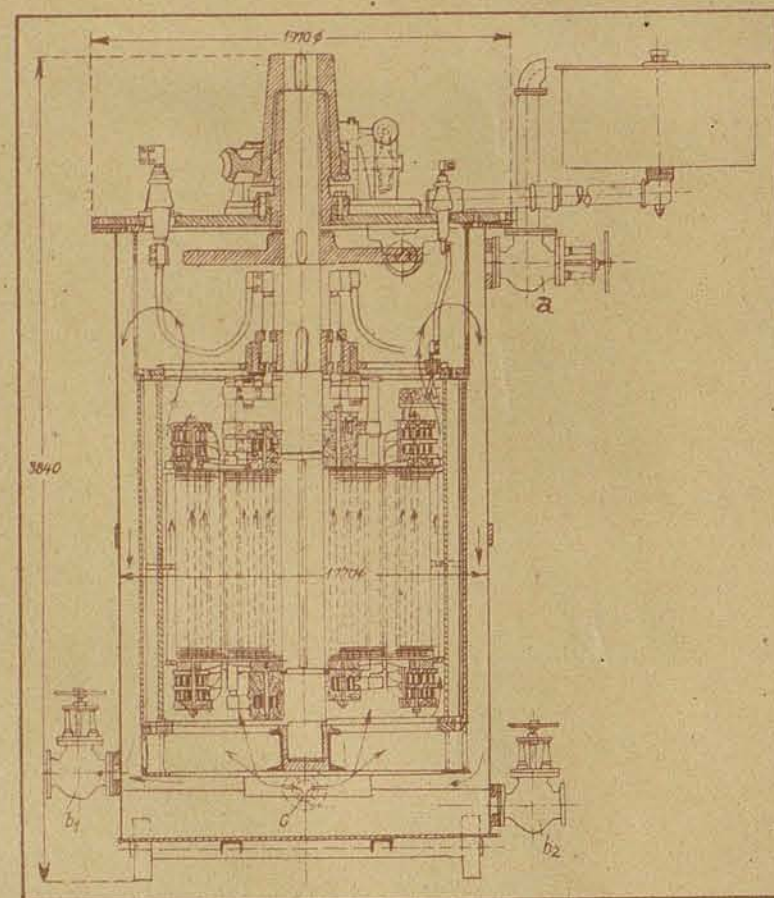


Fig. 94.  
Corte de un gran transformador rotatorio

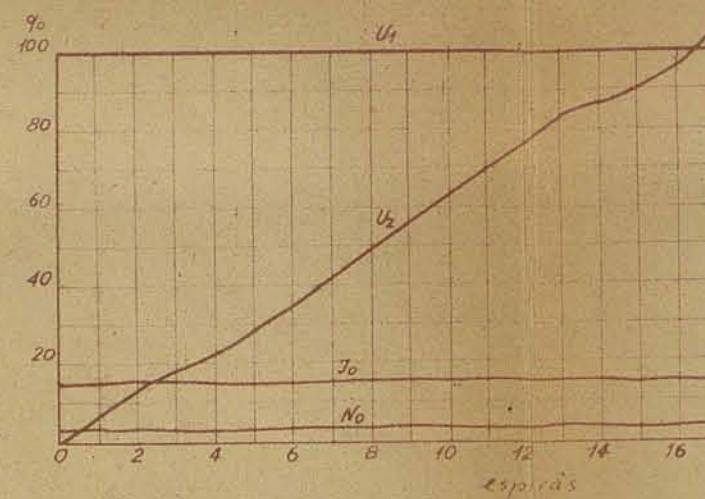


Fig. 96.

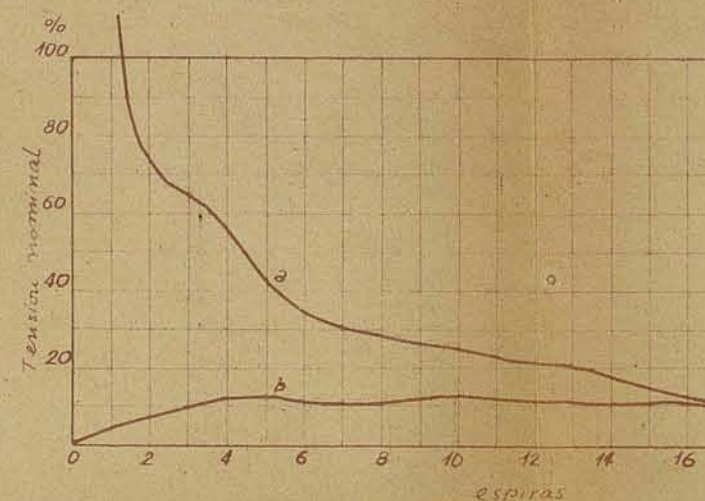


Fig. 97.

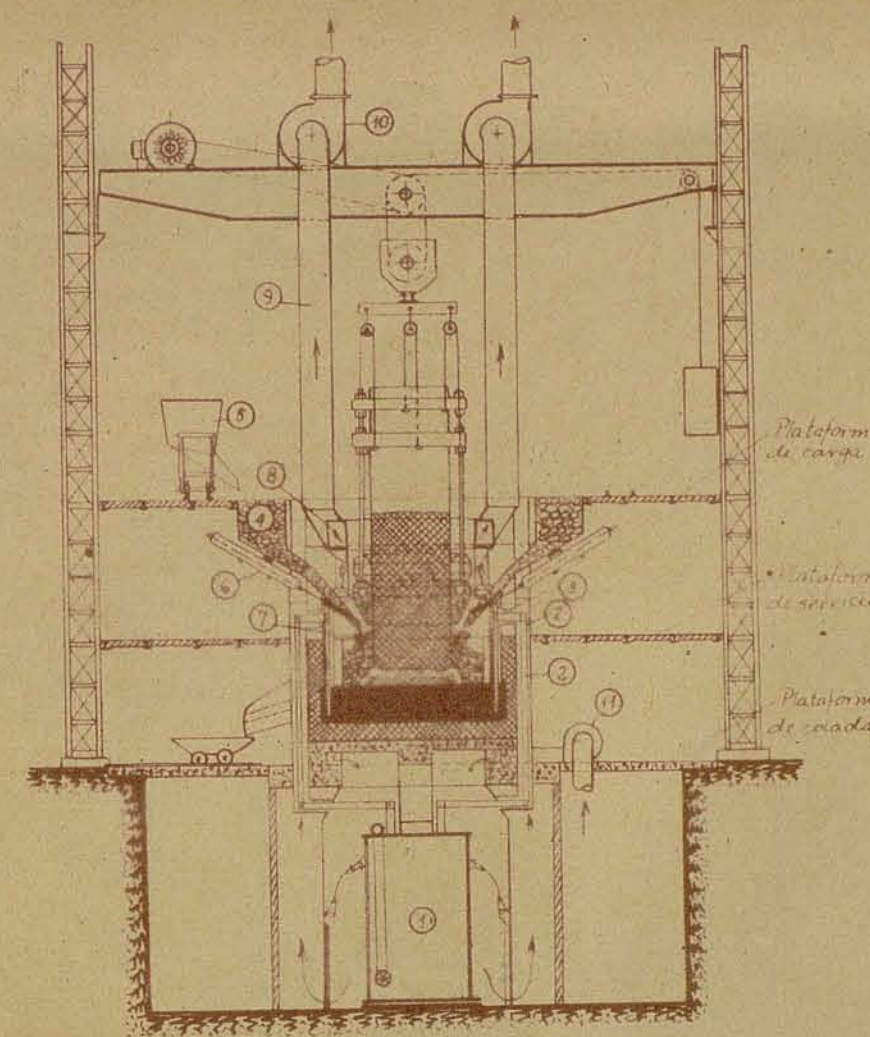


Fig. 106

Corte transversal de un horno monofaseo Miguel  
Legenda: 1. Transformador, 2. conductores secundarios, 3. Tomas, 4. Tapa de carga, 5. Casetilla de carga, 6. Empujador hidraulico, 7. Colector de gases refrigerado por agua, 8. Canal anular de gases, 9. Salida de gases, 10. Ventilador, 11. Aspirador.

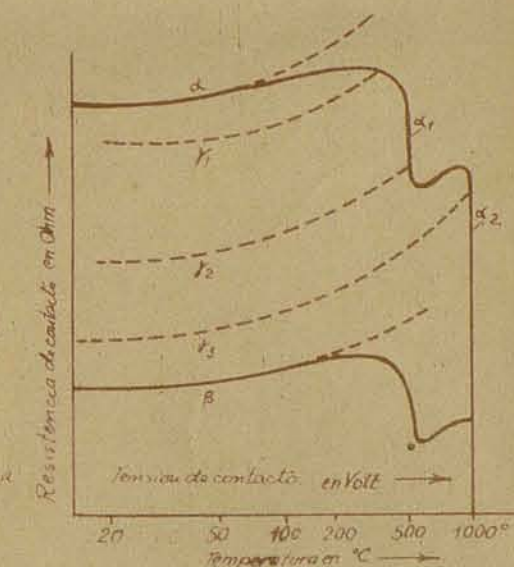


Fig. 107.

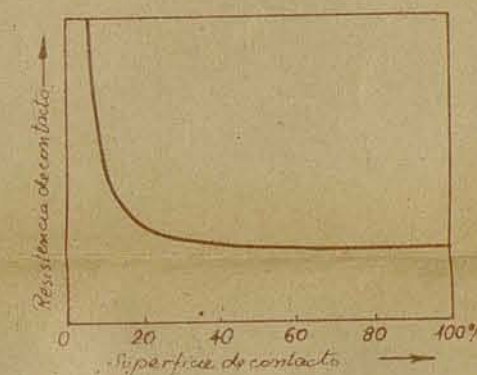


Fig. 108.

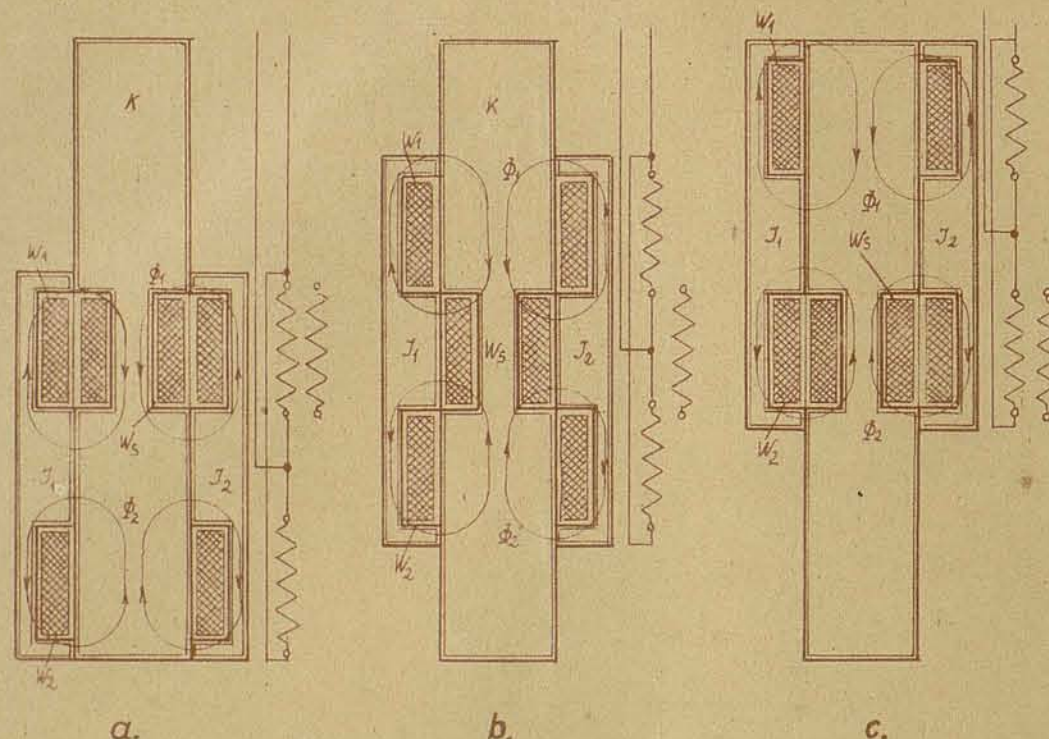


Fig. 95.

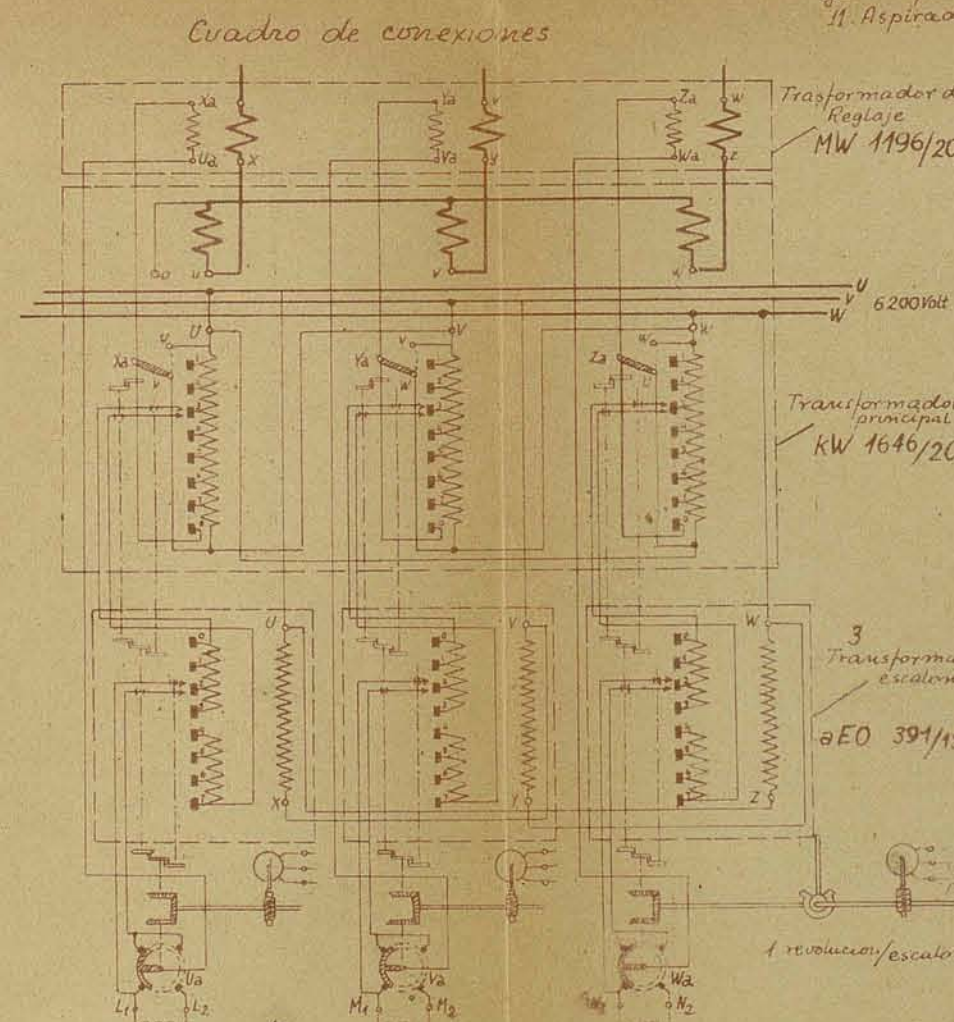


Fig. 105

Esquema de conexiones de un gran transformador de horno para 40.000 kVA

Potencia nominal kVA 40.000  
Frecuencia nominal Hz 50  
Tension nominal V  $\Delta$  6200 234 126  
Corriente nominal A 3720 100.000  
Tension nominal de corto-circuito 7.5 %  
Funcionamiento tipo DB  
Refrigeracion tipo OWA  
Agua de refrigeracion 420 l/min. Tiempo de entrada 25°C  
Engrase 8200 l/min.

Esquema de Regulacion

| Alta tension |       | Baja tension |       |
|--------------|-------|--------------|-------|
| Grado        | Volts | Grado        | Volts |
| 1            | 6200  | 1            | 234   |
| 2            | 6200  | 2            | 234   |
| 3            | 6200  | 3            | 234   |
| 4            | 6200  | 4            | 234   |
| 5            | 6200  | 5            | 234   |
| 6            | 6200  | 6            | 234   |
| 7            | 6200  | 7            | 234   |
| 8            | 6200  | 8            | 234   |
| 9            | 6200  | 9            | 234   |
| 10           | 6200  | 10           | 234   |
| 11           | 6200  | 11           | 234   |
| 12           | 6200  | 12           | 234   |
| 13           | 6200  | 13           | 234   |
| 14           | 6200  | 14           | 234   |
| 15           | 6200  | 15           | 234   |
| 16           | 6200  | 16           | 234   |
| 17           | 6200  | 17           | 234   |
| 18           | 6200  | 18           | 234   |
| 19           | 6200  | 19           | 234   |
| 20           | 6200  | 20           | 234   |
| 21           | 6200  | 21           | 234   |
| 22           | 6200  | 22           | 234   |
| 23           | 6200  | 23           | 234   |
| 24           | 6200  | 24           | 234   |
| 25           | 6200  | 25           | 234   |
| 26           | 6200  | 26           | 234   |
| 27           | 6200  | 27           | 234   |
| 28           | 6200  | 28           | 234   |
| 29           | 6200  | 29           | 234   |
| 30           | 6200  | 30           | 234   |
| 31           | 6200  | 31           | 234   |
| 32           | 6200  | 32           | 234   |
| 33           | 6200  | 33           | 234   |
| 34           | 6200  | 34           | 234   |
| 35           | 6200  | 35           | 234   |
| 36           | 6200  | 36           | 234   |
| 37           | 6200  | 37           | 234   |
| 38           | 6200  | 38           | 234   |
| 39           | 6200  | 39           | 234   |
| 40           | 6200  | 40           | 234   |

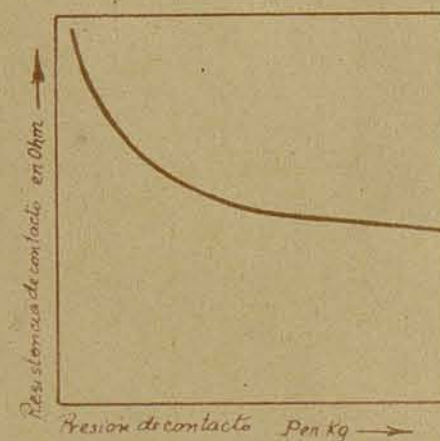


Fig. 109.

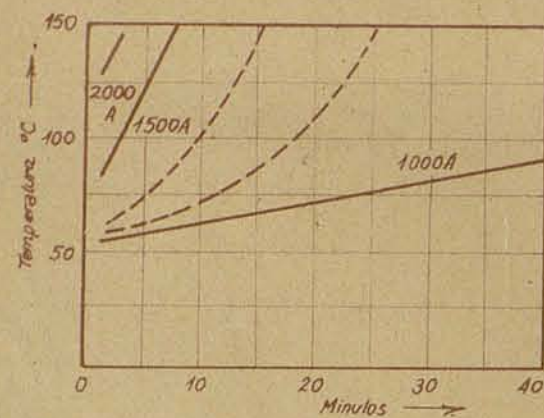


Fig. 110.

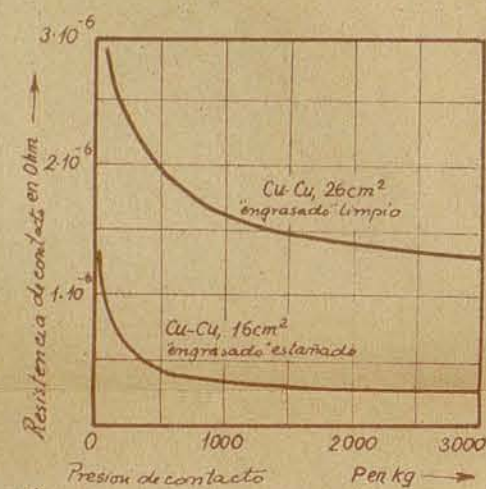


Fig. 111.

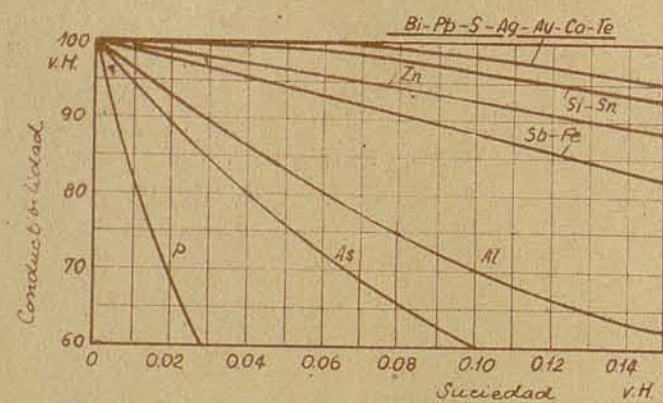


Fig. 112.

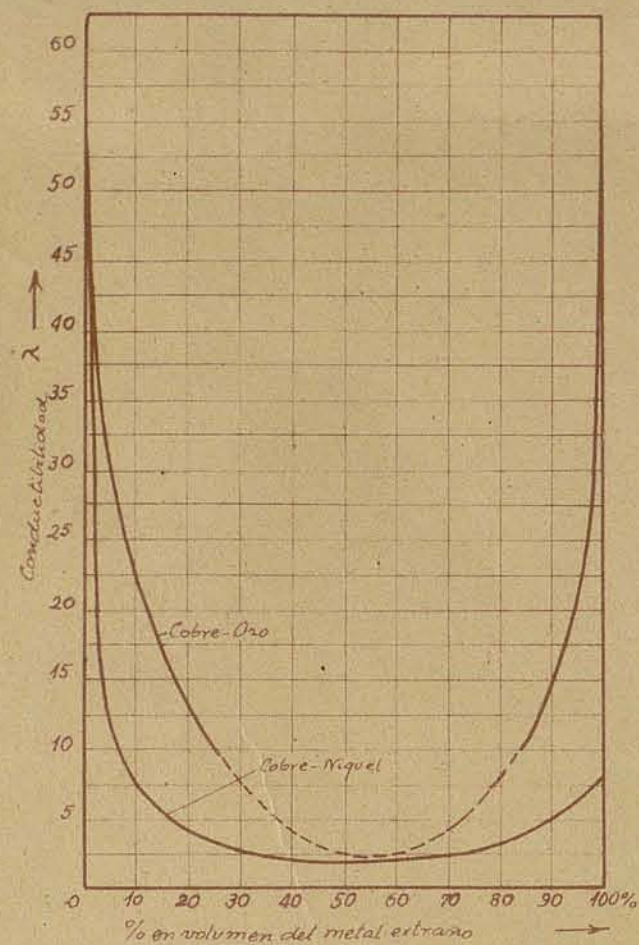


Fig. 113.

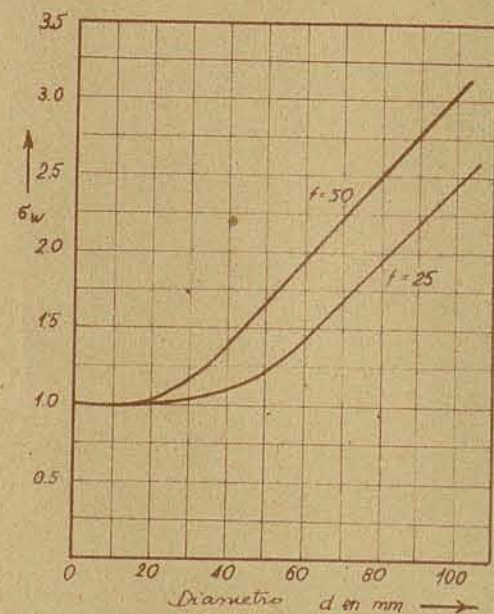


Fig. 115.

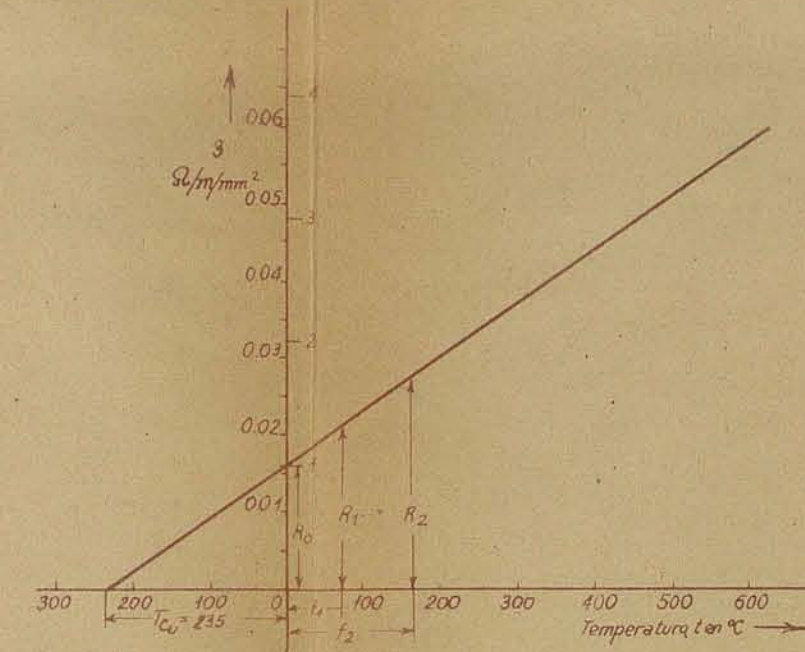


Fig. 114.

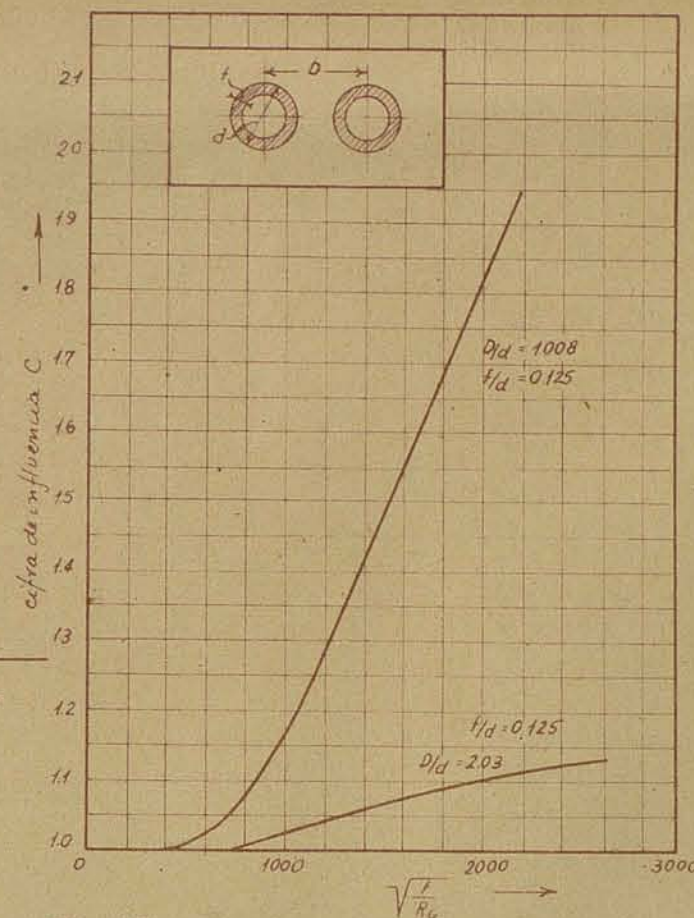


Fig. 117.

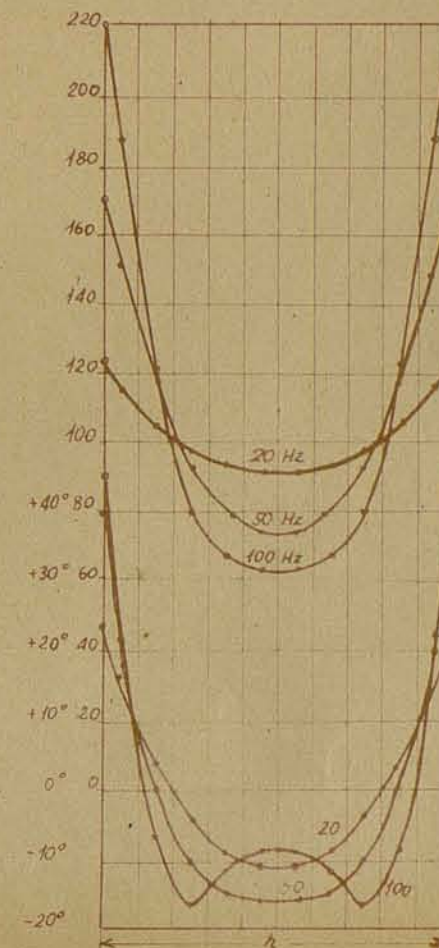


Fig. 118.

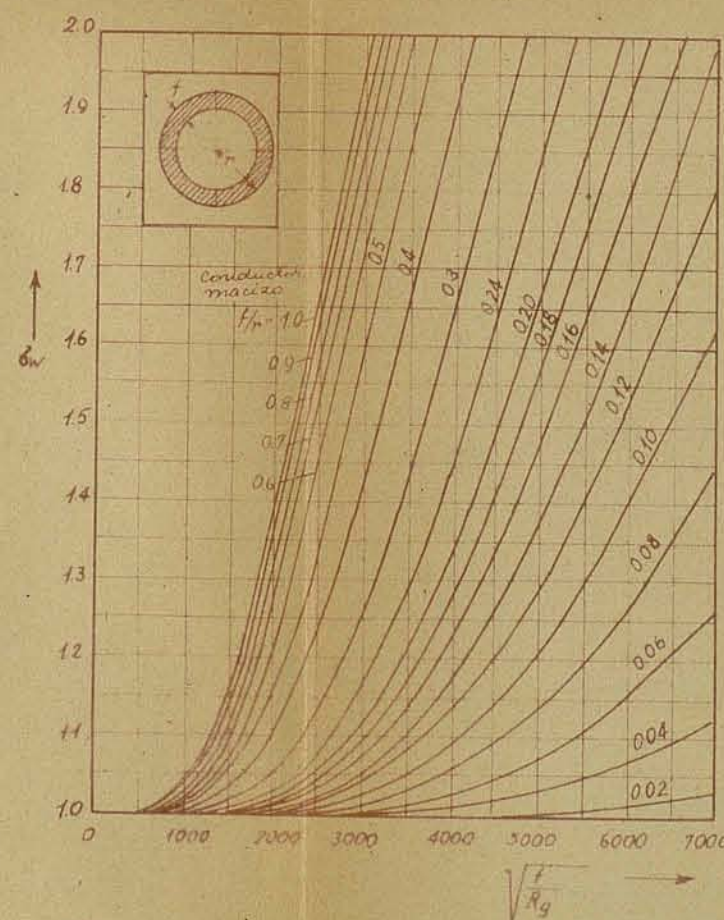


Fig. 116.

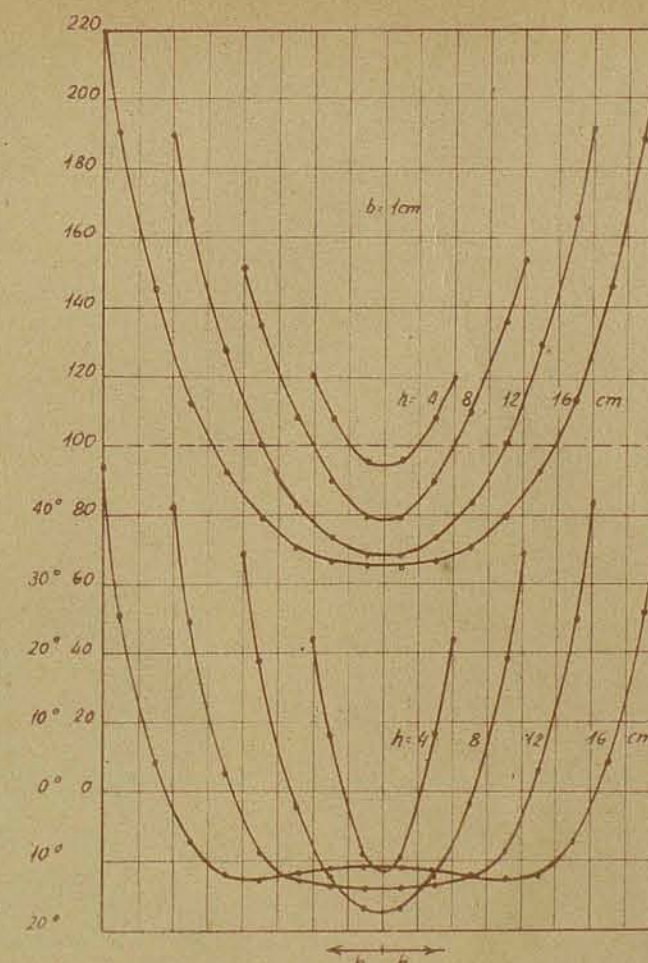


Fig. 119.

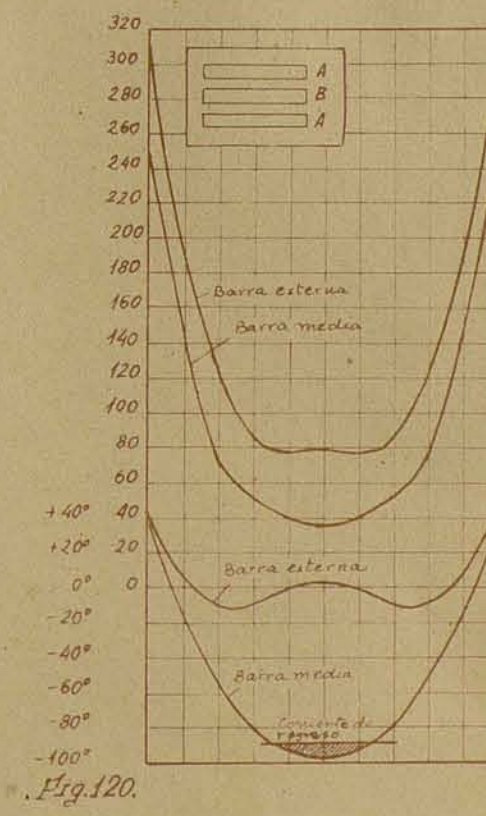


Fig. 120.

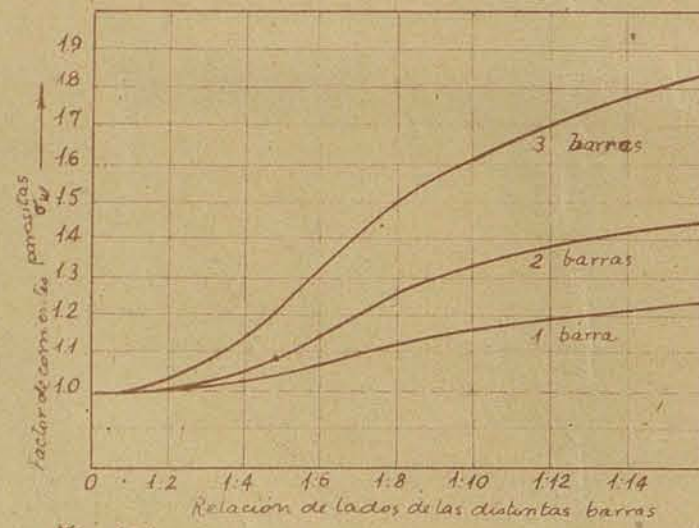


Fig. 121.

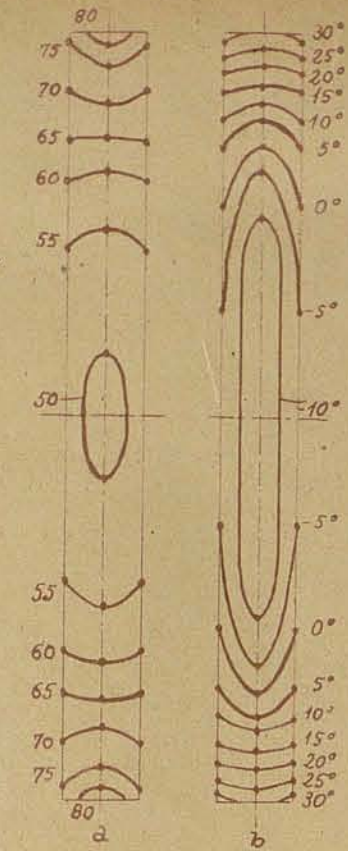


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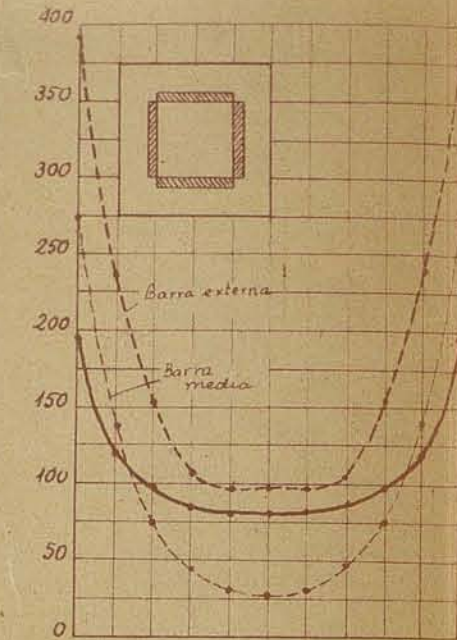


Fig. 123.

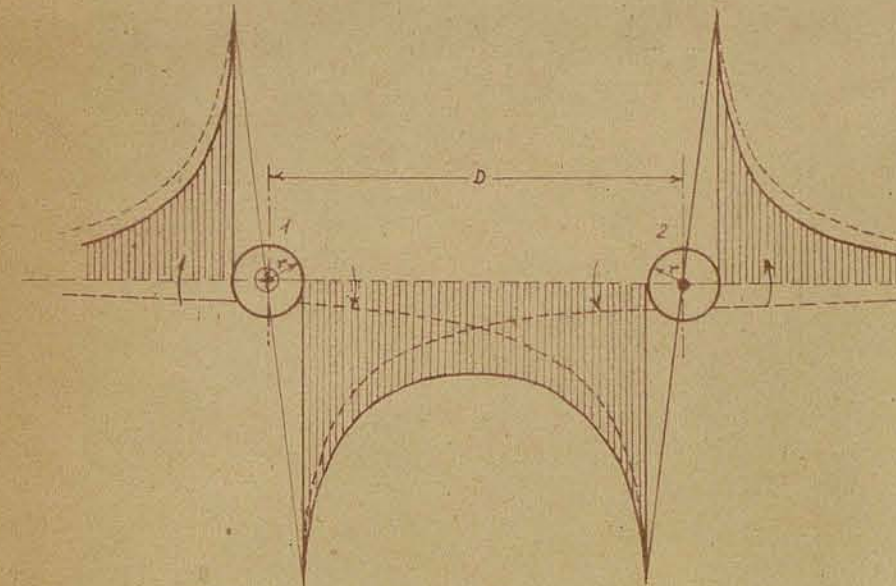


Fig. 135.

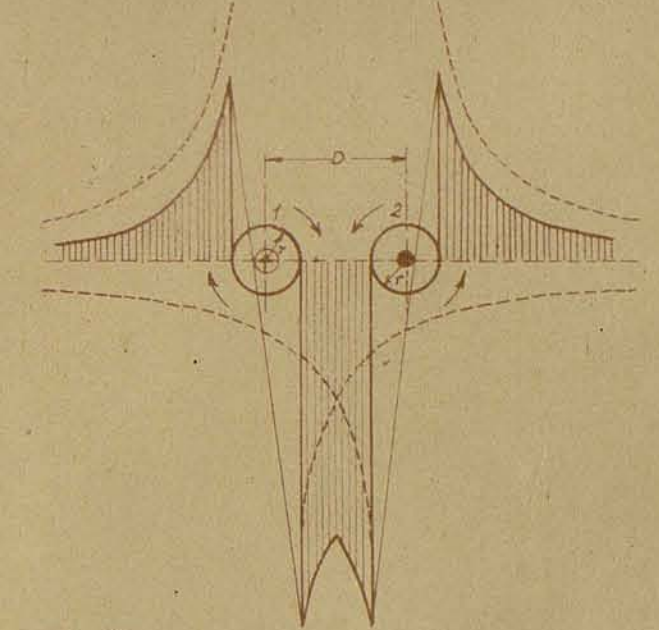


Fig. 136.

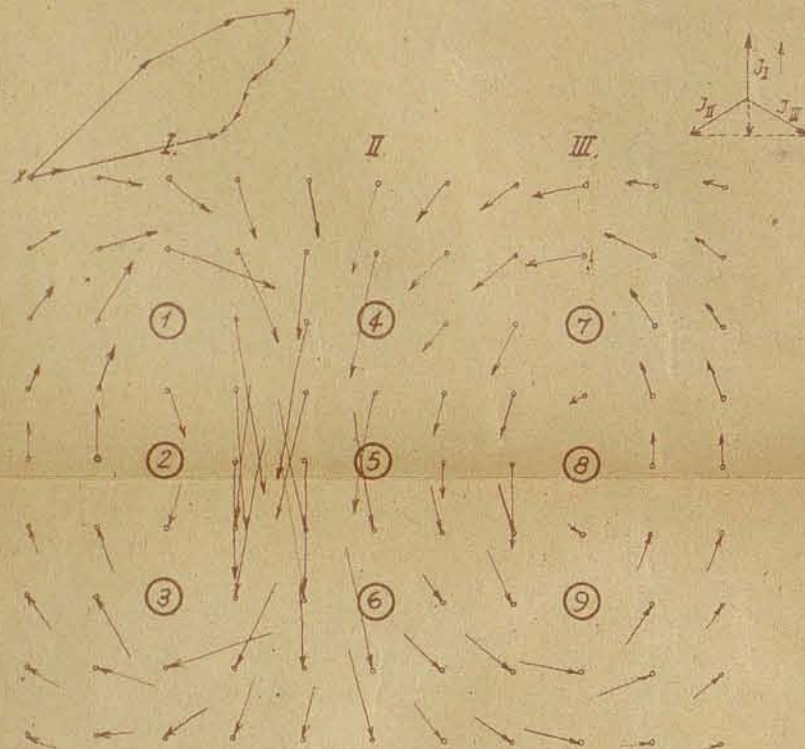


Fig. 124.

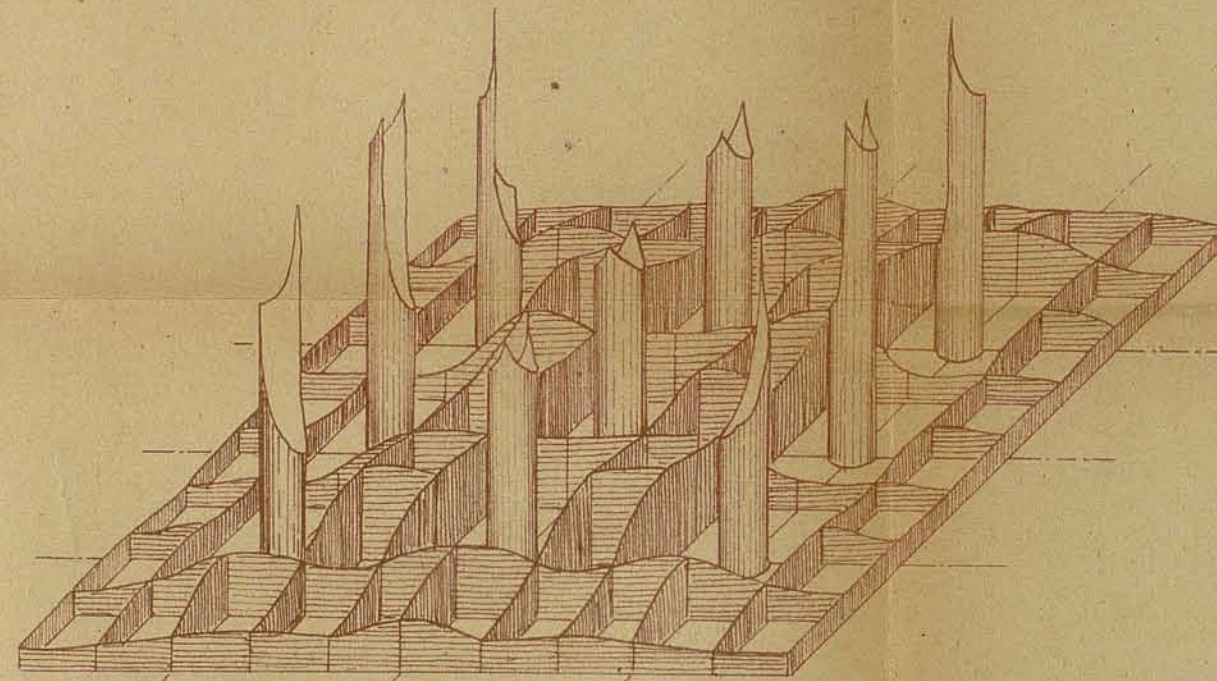


Fig. 126.

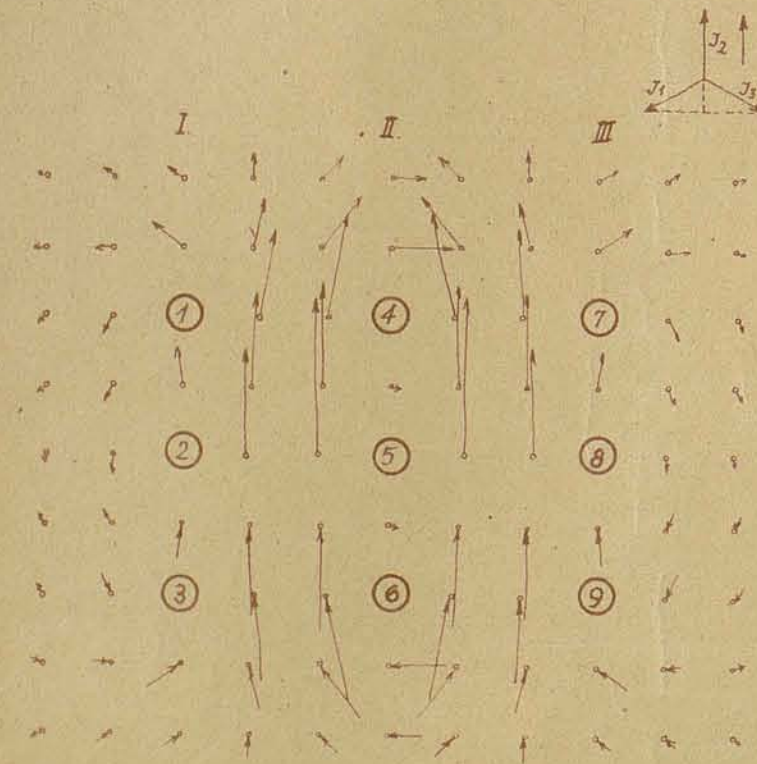


Fig. 125.

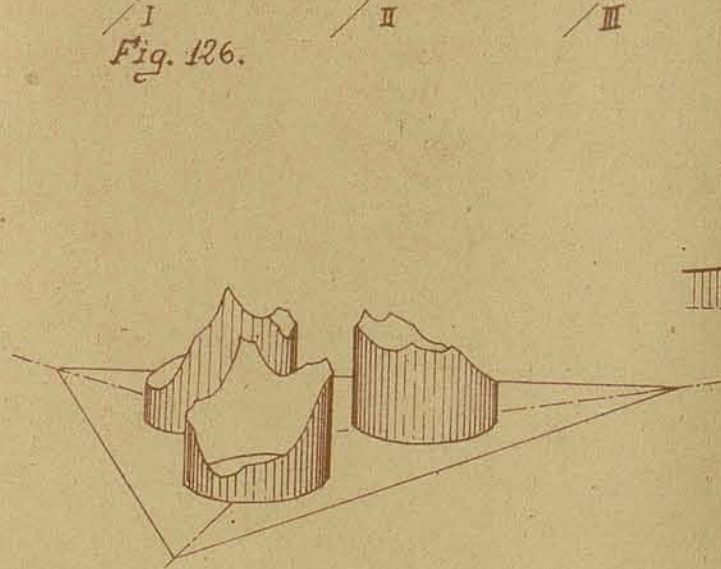


Fig. 127.

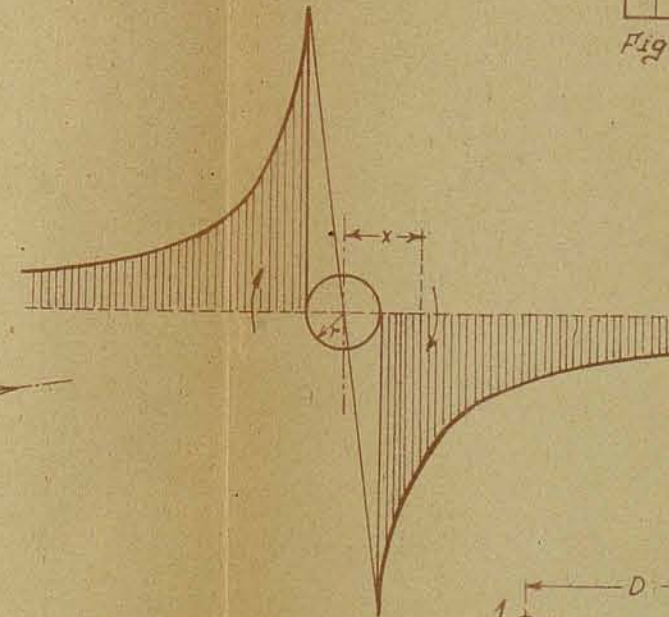


Fig. 134.

| Forma del Conductor                     |  | L(Henry)% |
|-----------------------------------------|--|-----------|
| 1. Circulo d= 102m                      |  | 100.0     |
| 2. idem partido en dos en angulo recto  |  | 99.1      |
| 3. Cuadrado, lado 0.80m                 |  | 99.2      |
| 4. idem dividido en dos en angulo recto |  | 93.6      |
| 5. Rectangulo 0.80x1.10m                |  | 94.7      |
| 6. idem dividido en dos en angulo recto |  | 89.3      |
| 7. Rectangulo 0.40x1.2m                 |  | 88.5      |
| 8. idem partido en tres en angulo recto |  | 81.5      |
| 9. Triangulo equilatero lados de 1.07m  |  | 94.0      |
| 10. idem partido en dos en angulo recto |  | 90.3      |

Fig. 137.

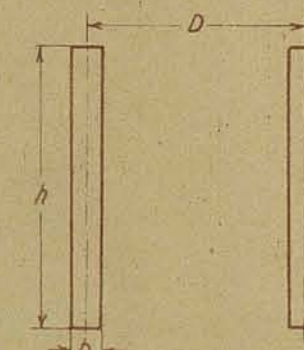


Fig. 140.

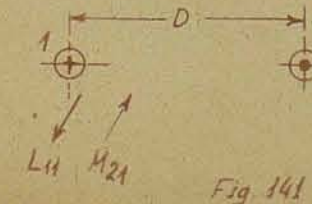


Fig. 141.

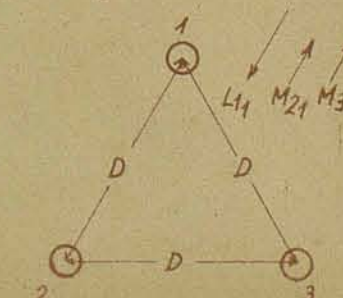


Fig. 142.

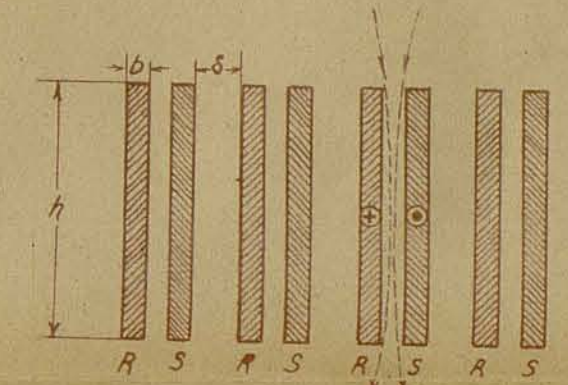


Fig. 138.

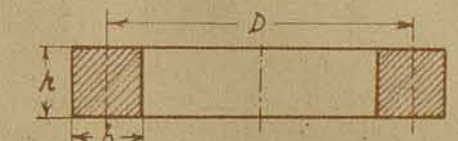


Fig. 139.

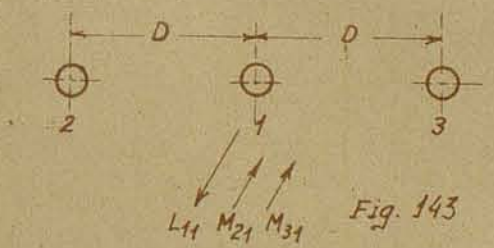


Fig. 143.

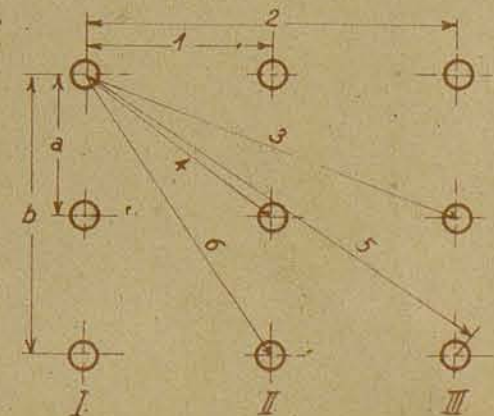
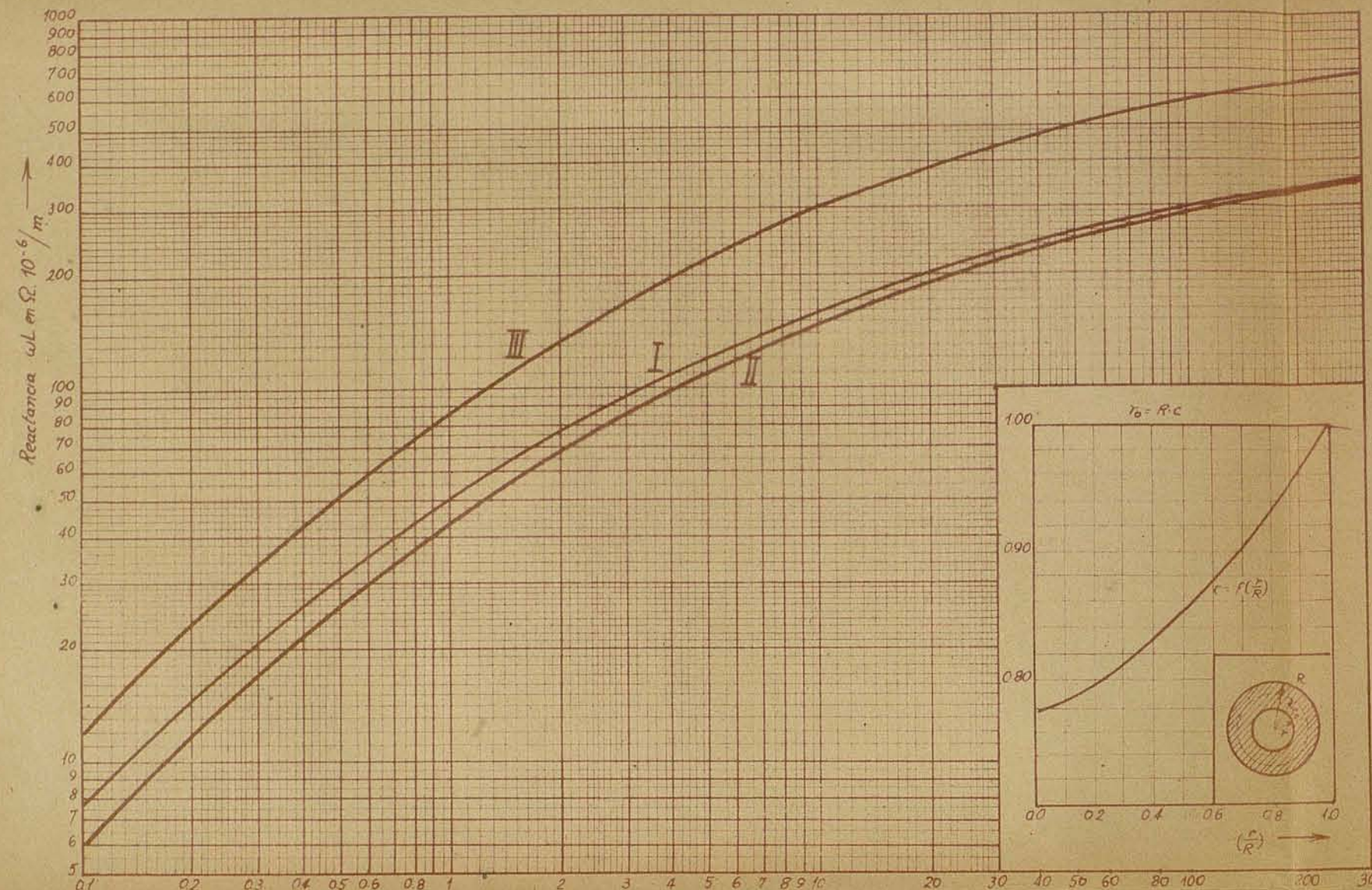


Fig. 144.



$D$  = Distancia entre conductores en cm  
 $r_0$  = Radio mag. equivalente en cm  
 $L$  = Longitud del conductor en m.

I. C. trifásica  $\omega L = 48.1 \lg \frac{(D+r_0)^2 (2D+r_0)}{r_0^3} \cdot 10^{-6} = 48.1 \lg \left[ 1 + 4 \left( \frac{D}{r_0} \right) + 5 \left( \frac{D}{r_0} \right)^2 + 2 \left( \frac{D}{r_0} \right)^3 \right] \cdot 10^{-6} \Omega$   
 II. C. monofásica conductor de ida  $\omega L = 144.1 \lg \left( 1 + \frac{D}{r_0} \right) \cdot 10^{-6} \Omega$   
 III. C. monofásica conductor ida y vuelta  $\omega L = 288.1 \lg \left( 1 + \frac{D}{r_0} \right) \cdot 10^{-6} \Omega$

Fig. 145. Table para el cálculo de la inductancia por el método de corte.

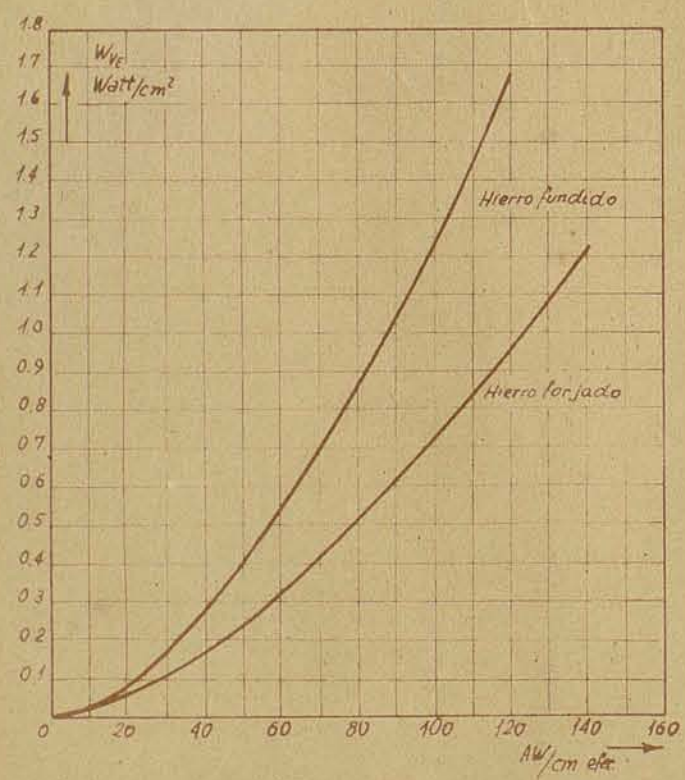


Fig. 153

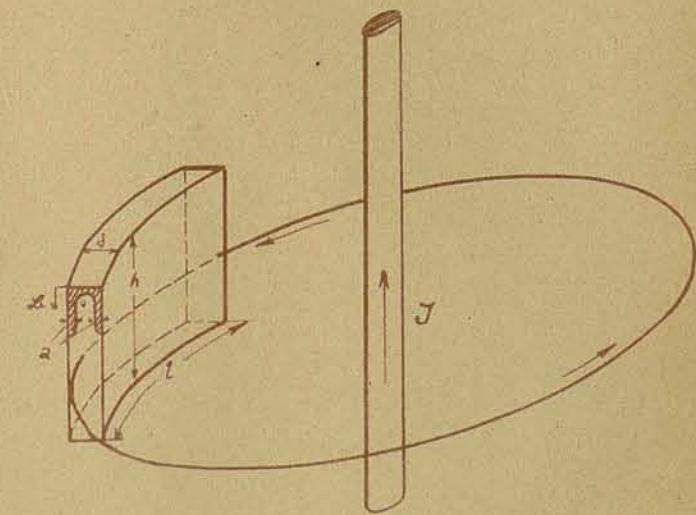


Fig. 154

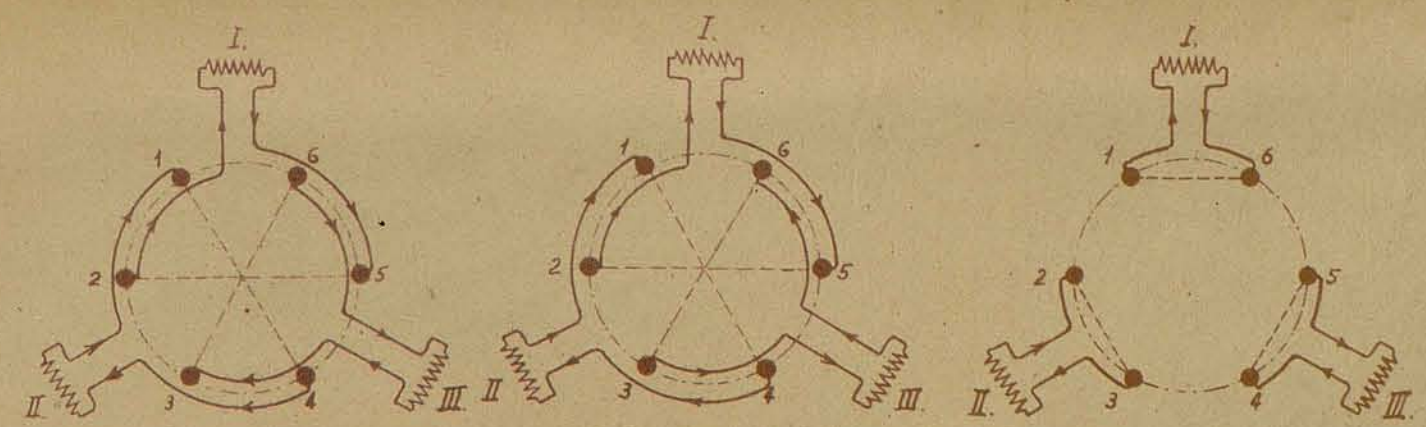


Fig. 146

Fig. 147

Fig. 148

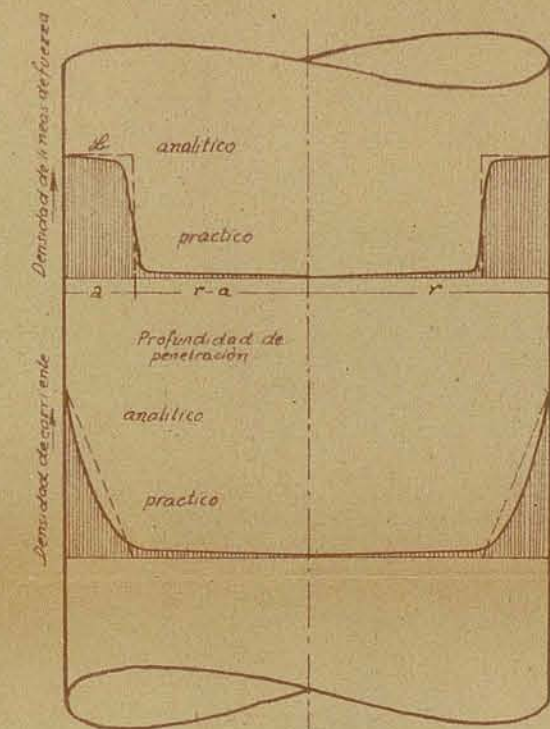


Fig. 151

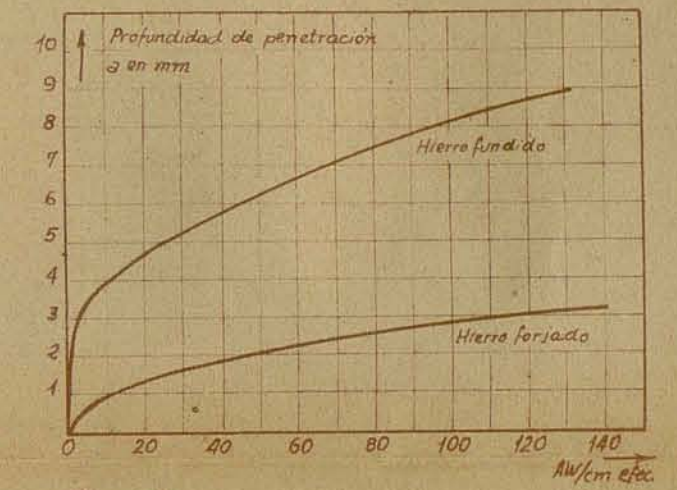


Fig. 152

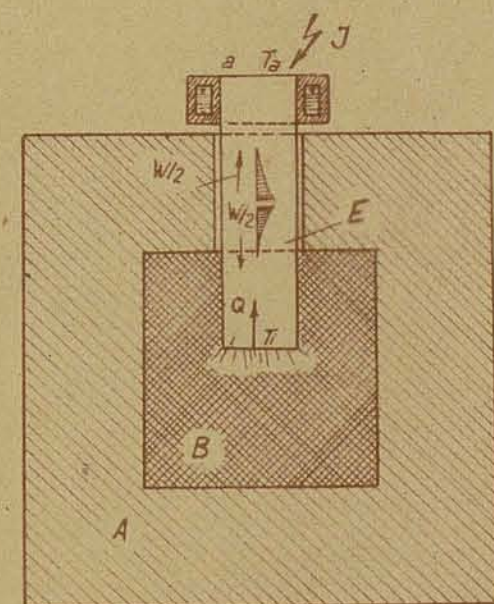


Fig. 159

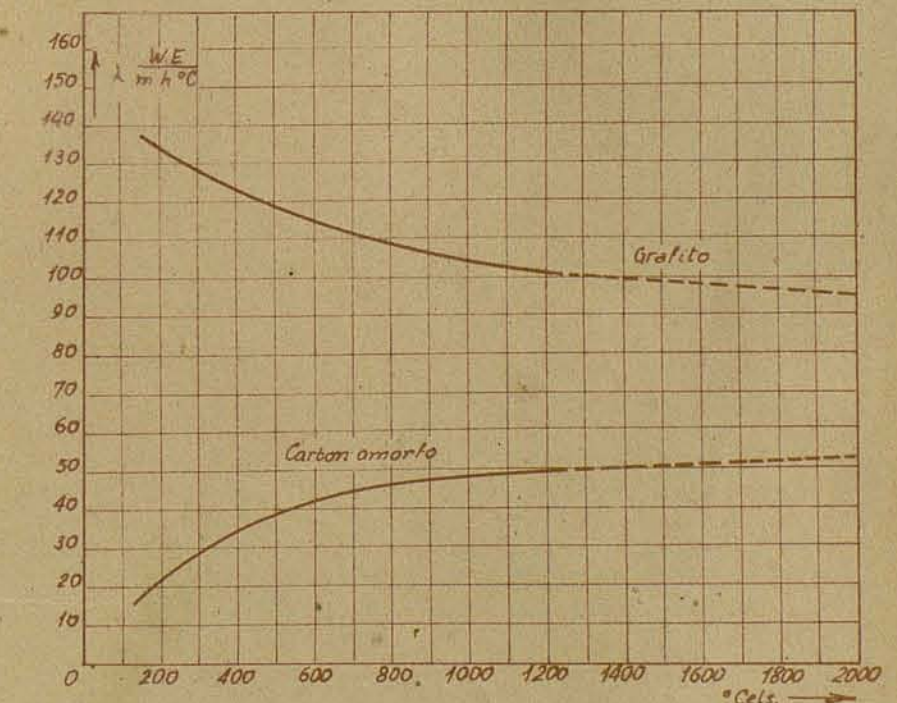


Fig. 160

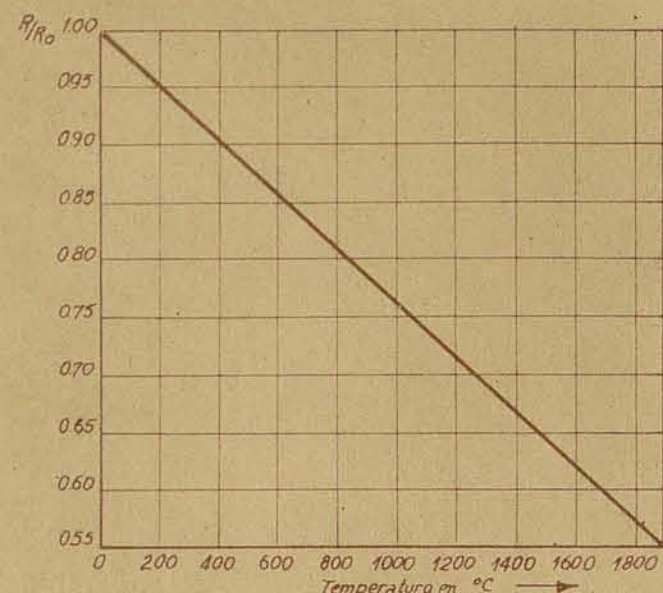


Fig. 161

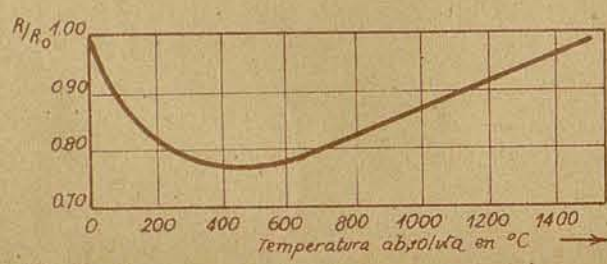


Fig. 162

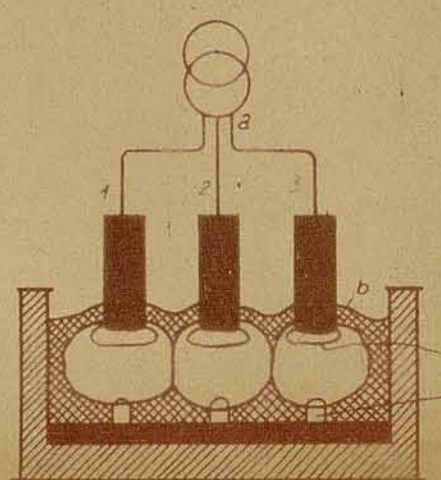
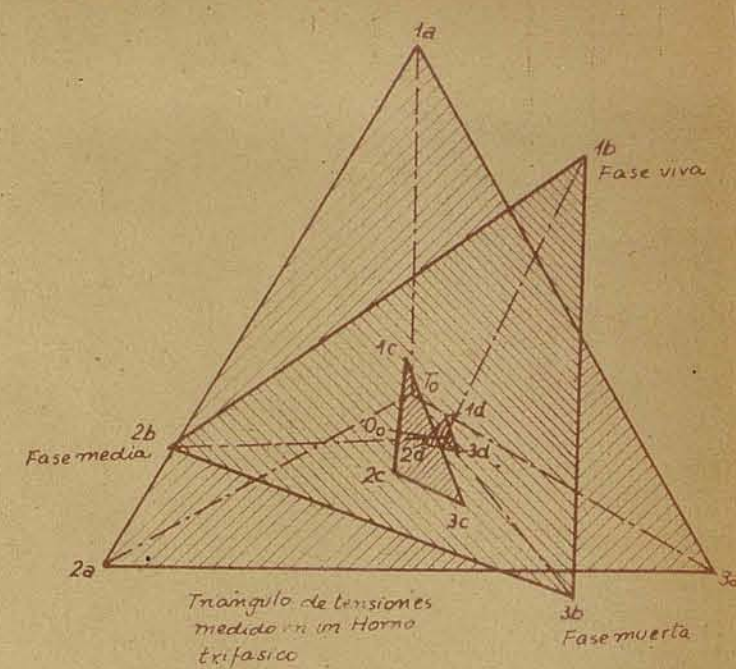


Fig. 164

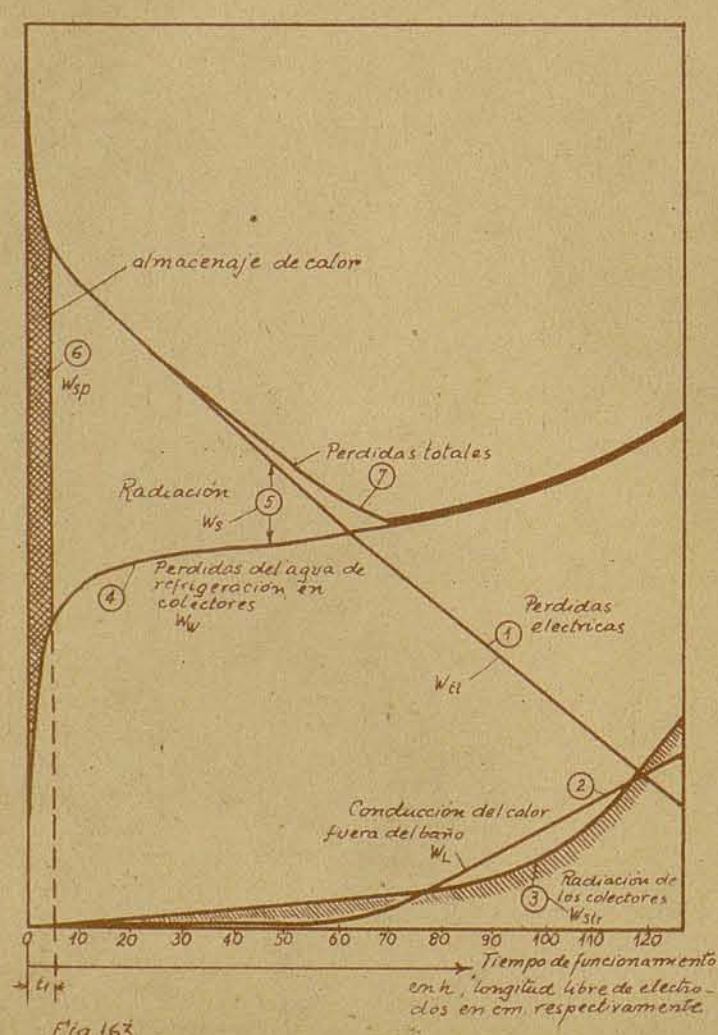


Fig. 163

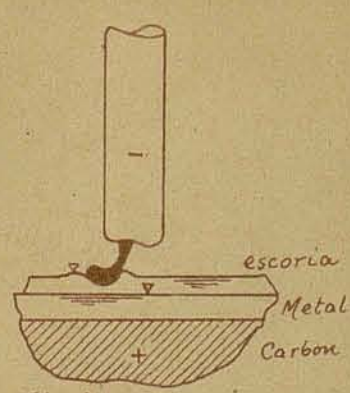


Fig. 165

Arco normal en un Horno de metal para corriente continua (según Kelleher)

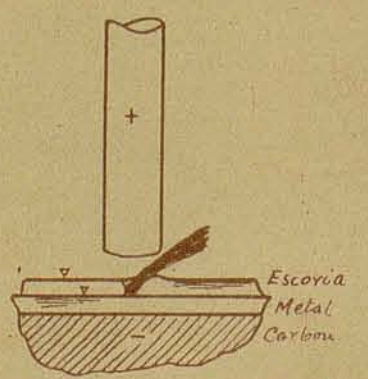


Fig. 166 Arco con polaridad falsa en un Horno como Fig. 165

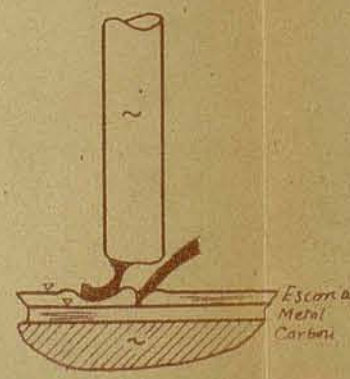


Fig. 167 Arco de calterna en debidas condiciones en un Horno de metal (según Kelleher)

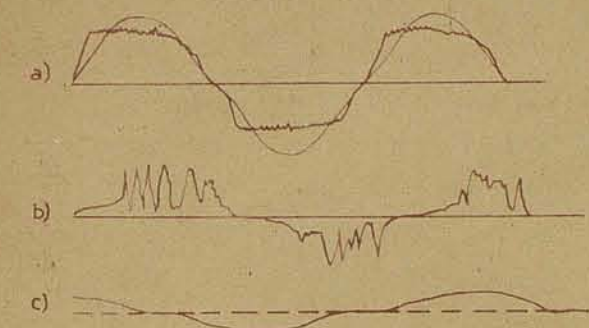


Fig. 168

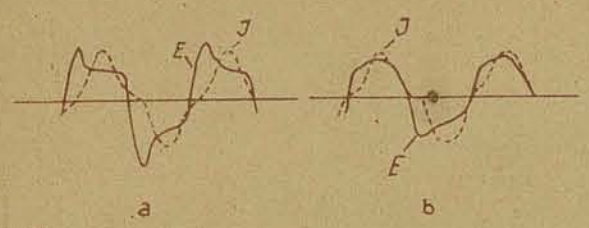


Fig. 169

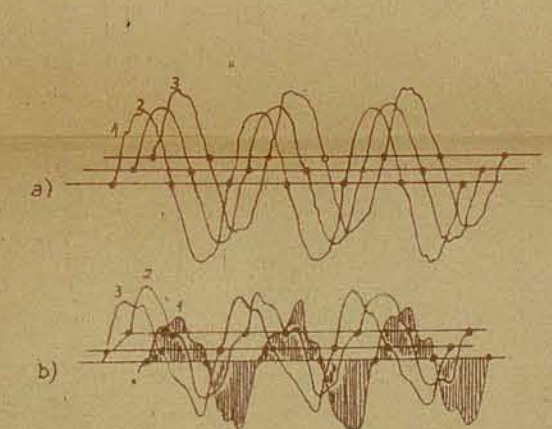


Fig. 170

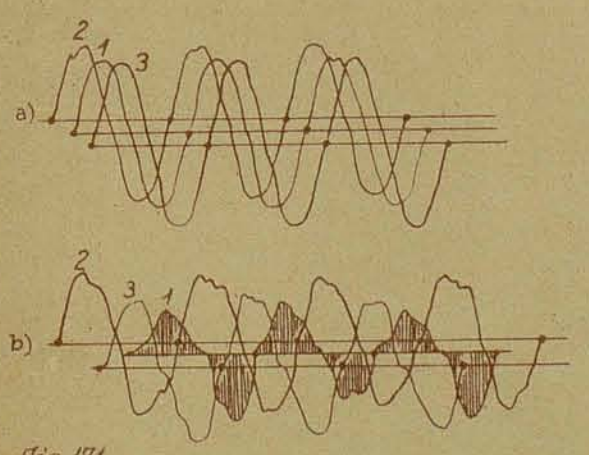


Fig. 171

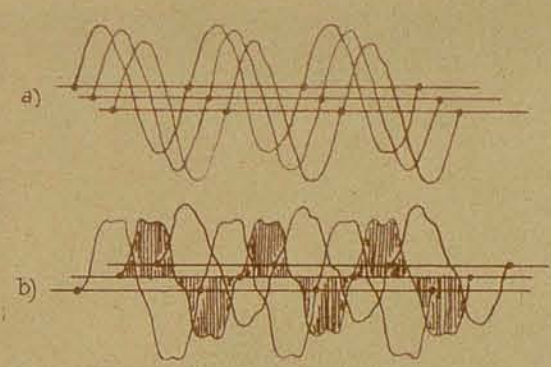


Fig. 172

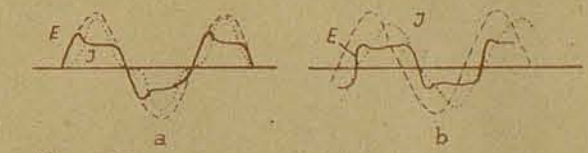


Fig. 173

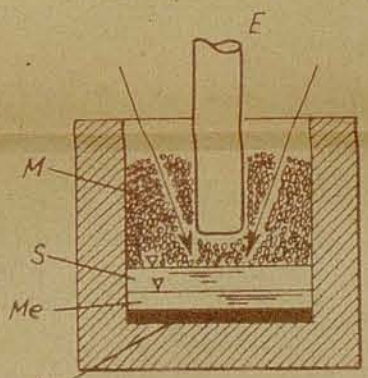


Fig. 174

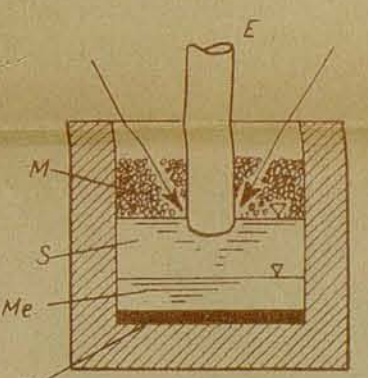


Fig. 175

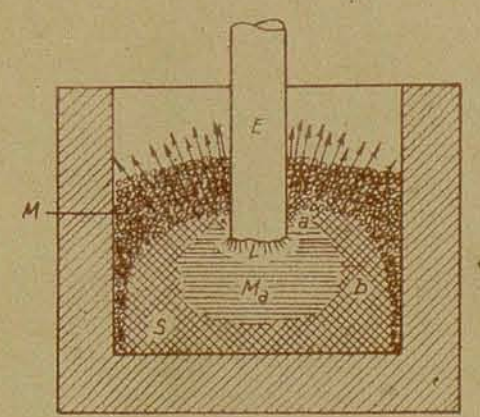


Fig. 176

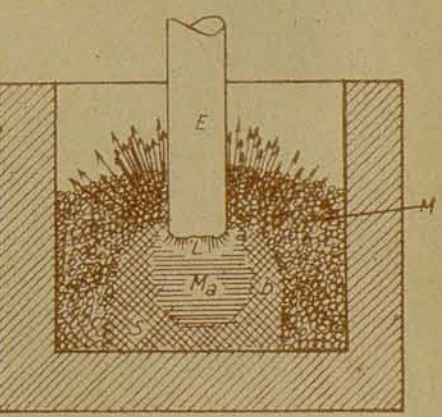


Fig. 177

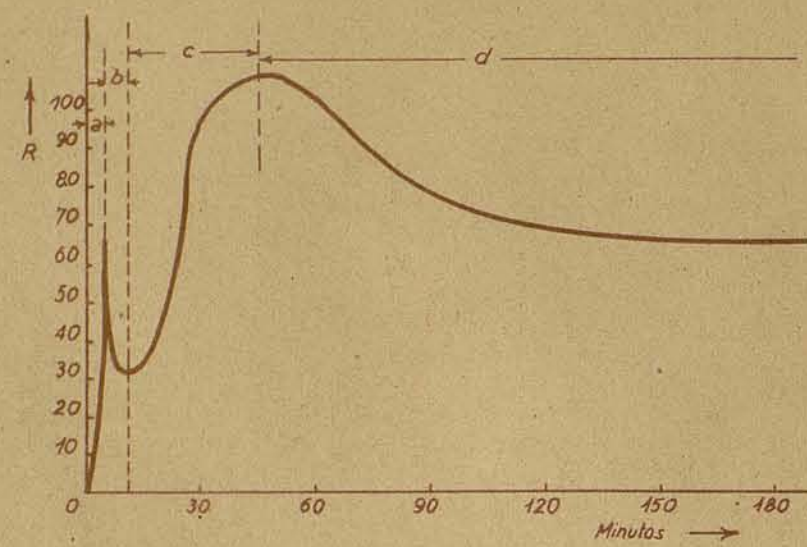


Fig. 178

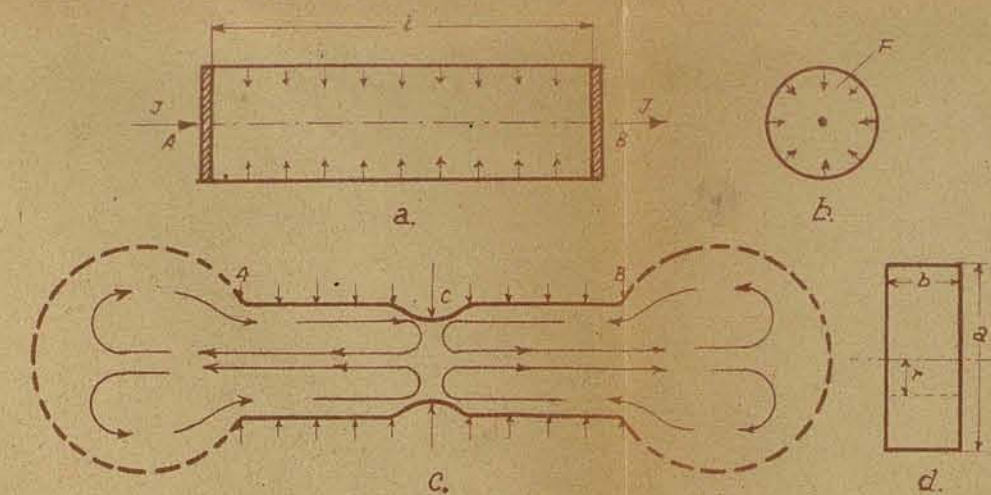


Fig. 181. Fenómenos de fuerzas de la corriente

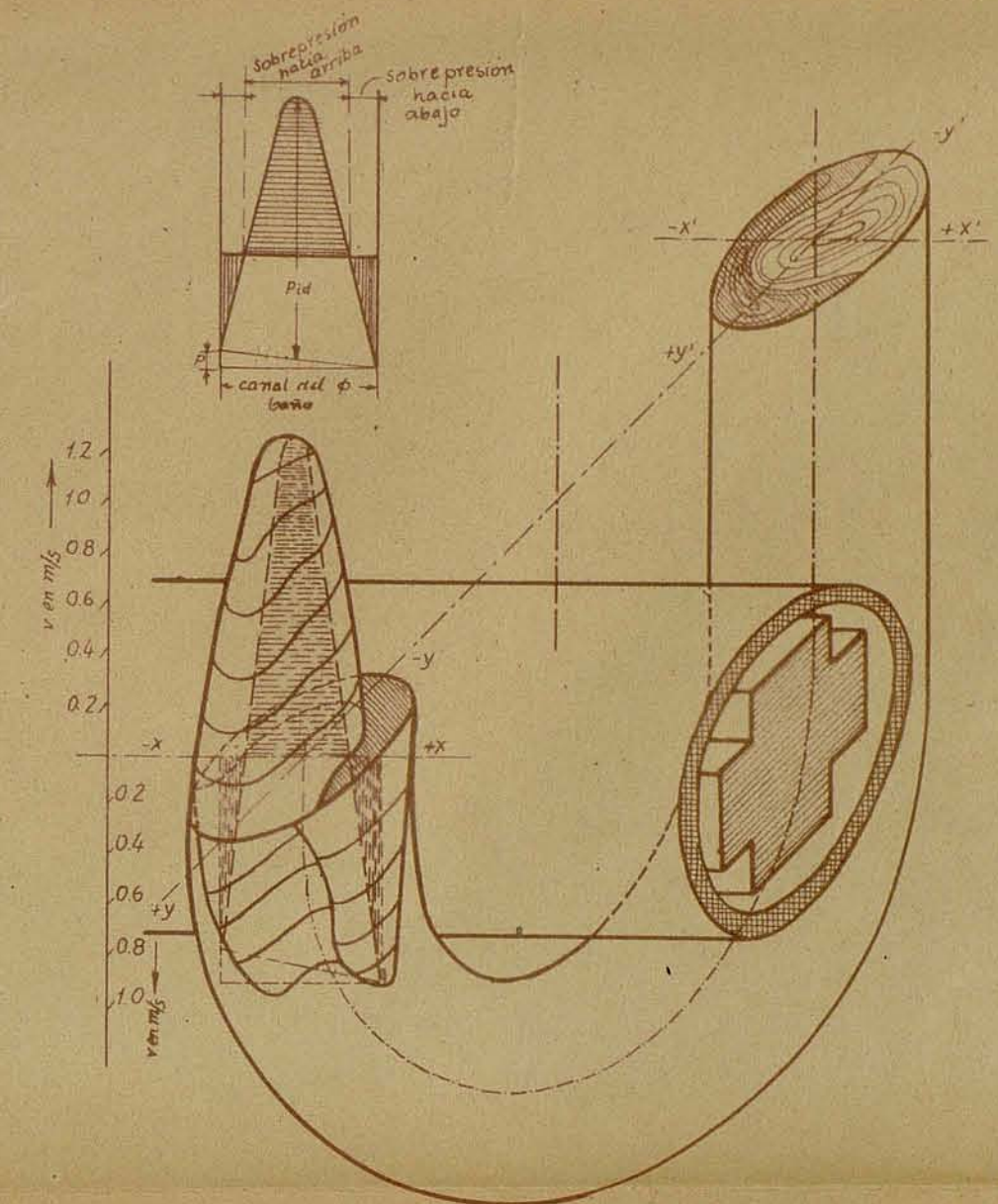


Fig. 184. gráfico de corrientes en un Horno de inducción

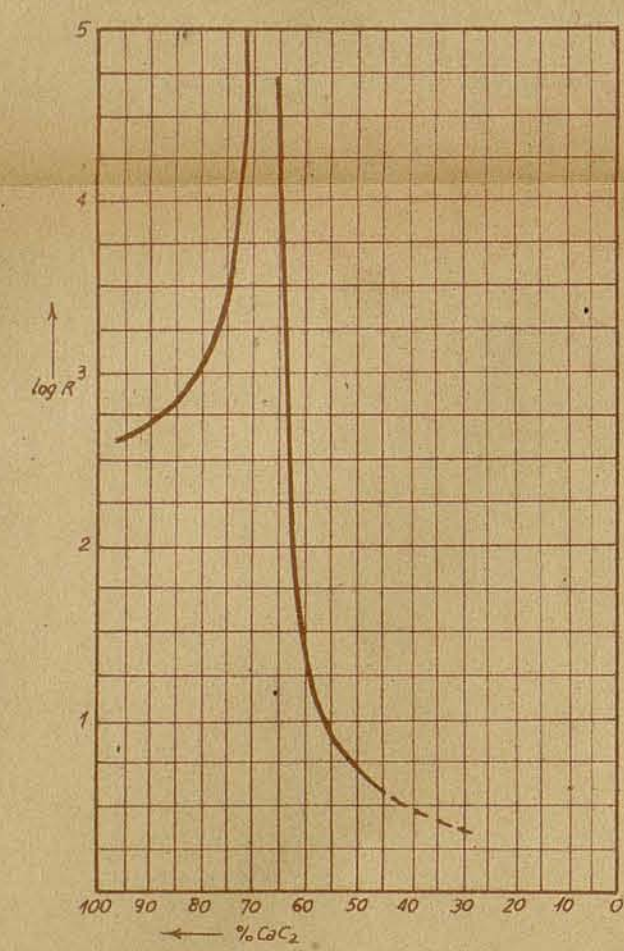


Fig. 180.

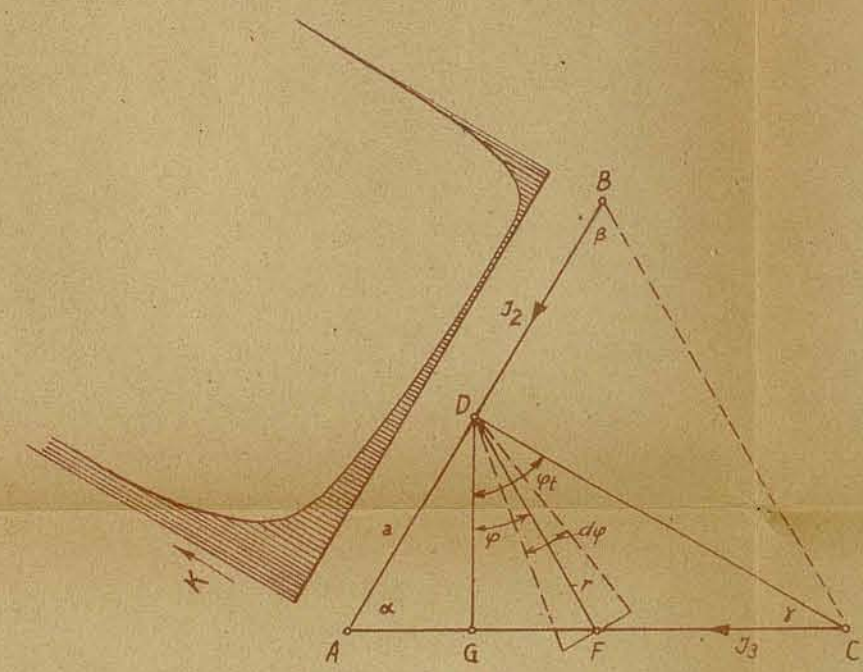


Fig. 182

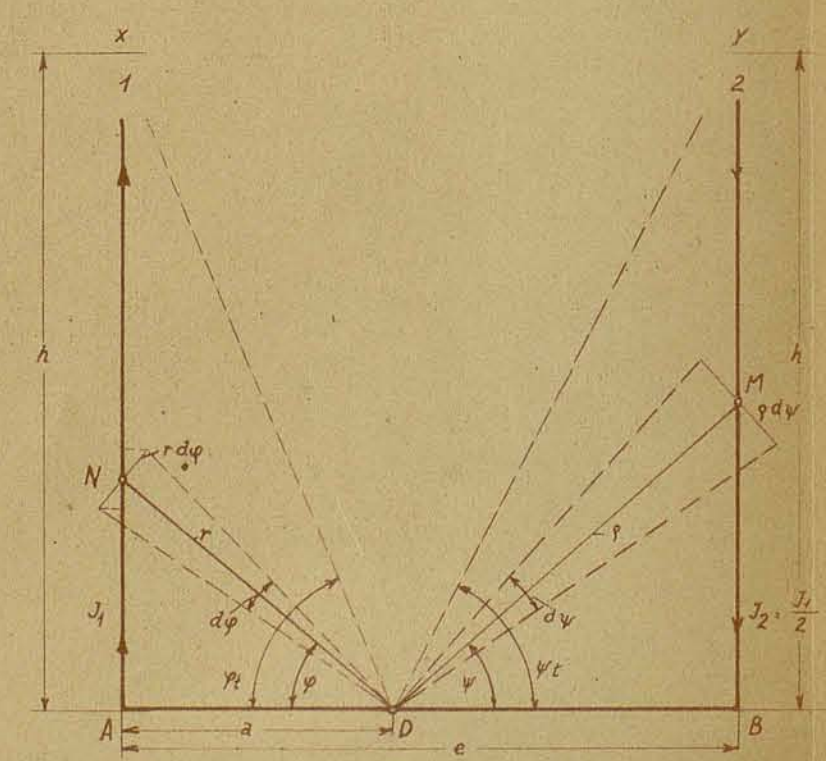


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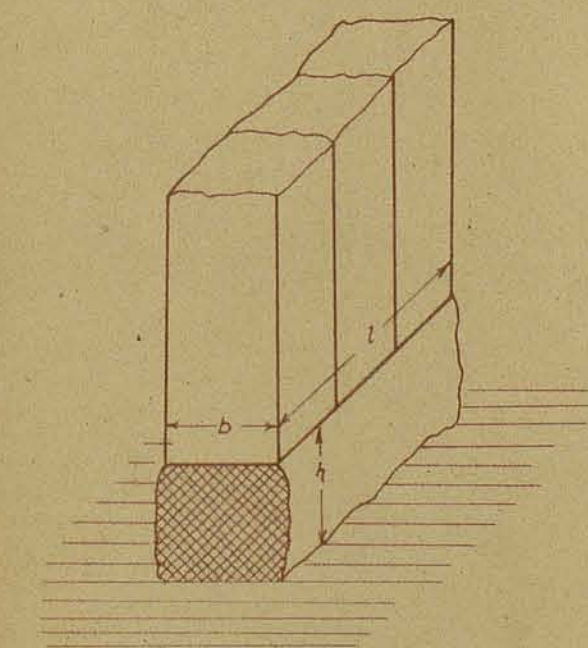


Fig. 185. Volumen de baño de un electrodo rectangular.

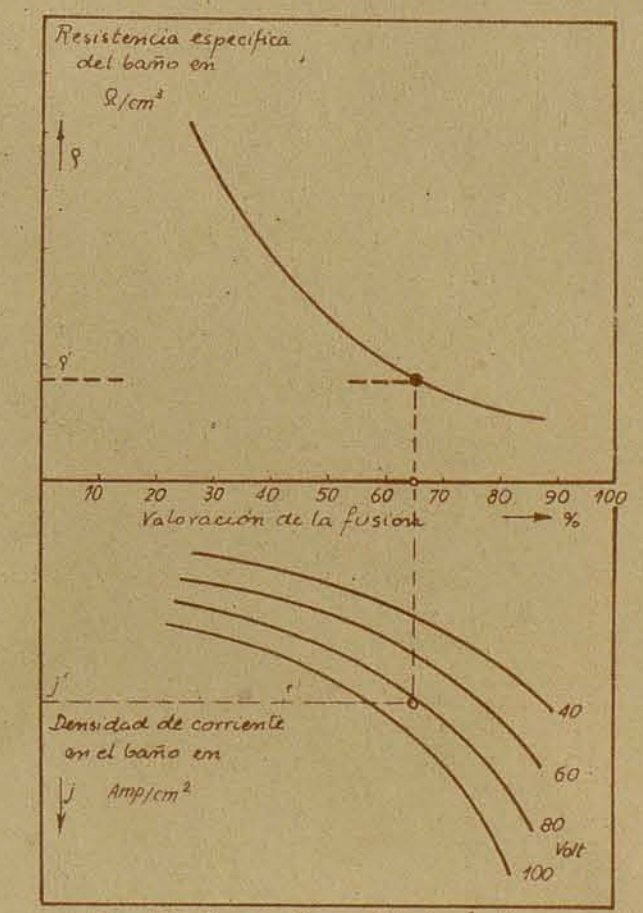
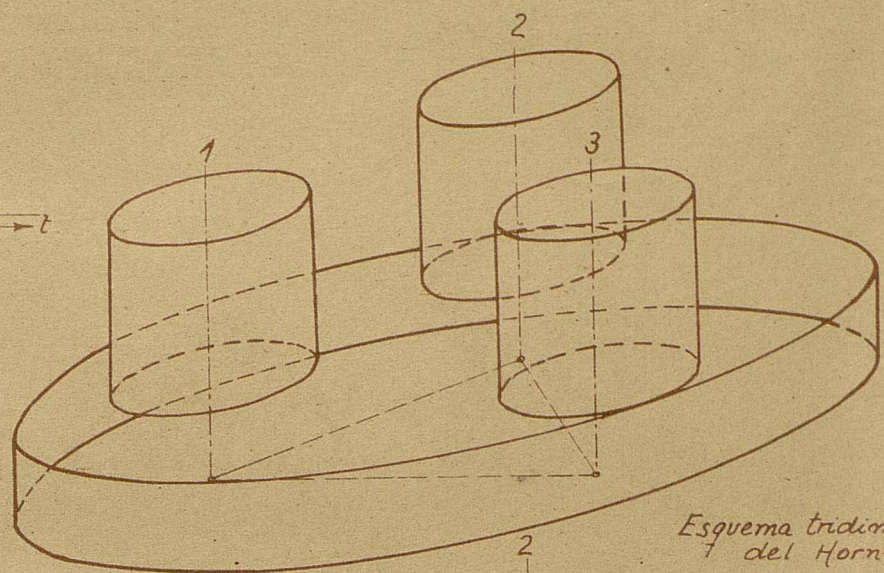
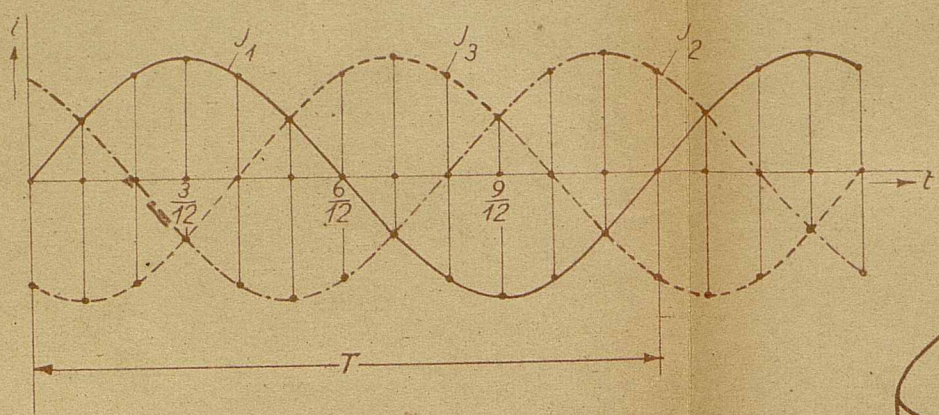


Fig. 186. Curvas de una electrofusión



Esquema tridimensional  
del Horno

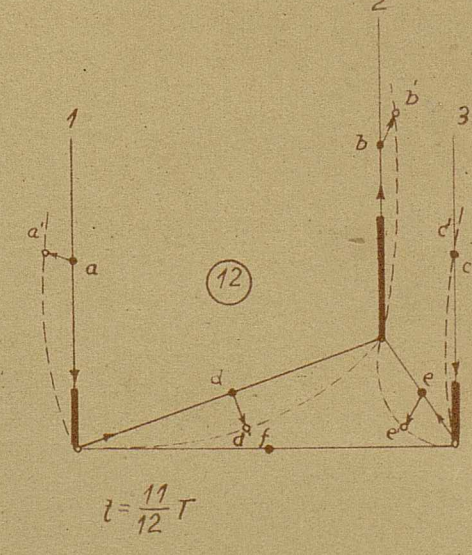
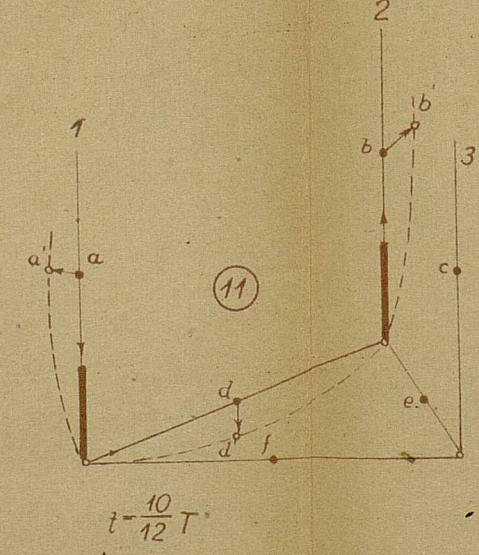
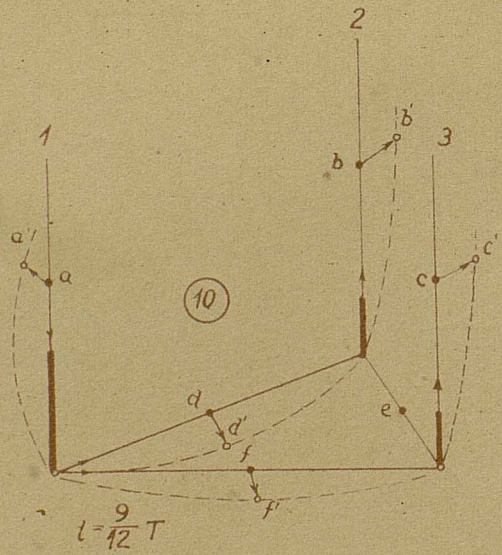
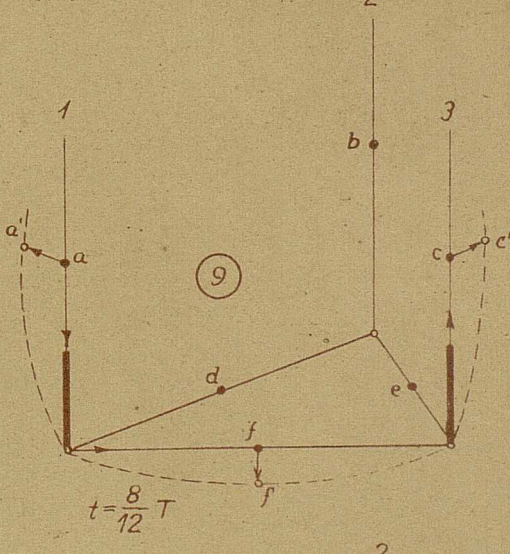
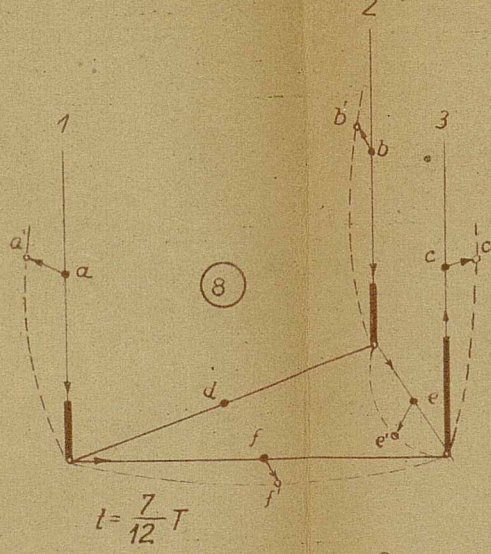
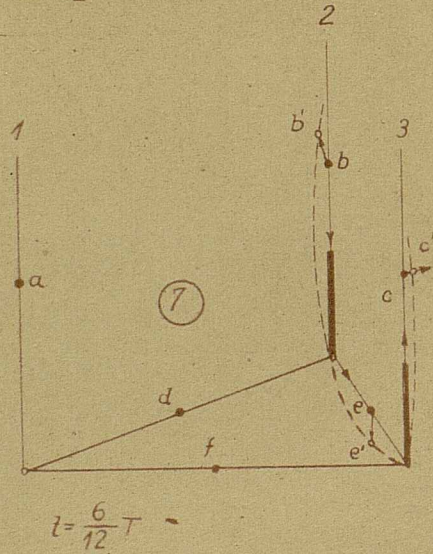
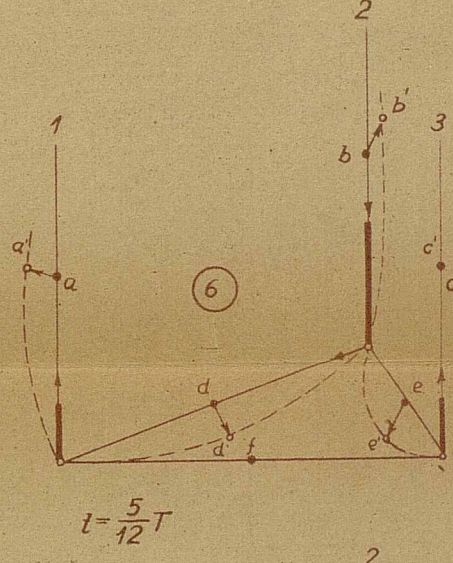
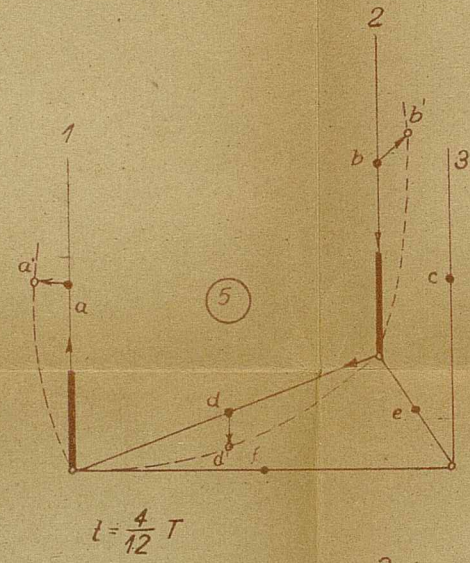
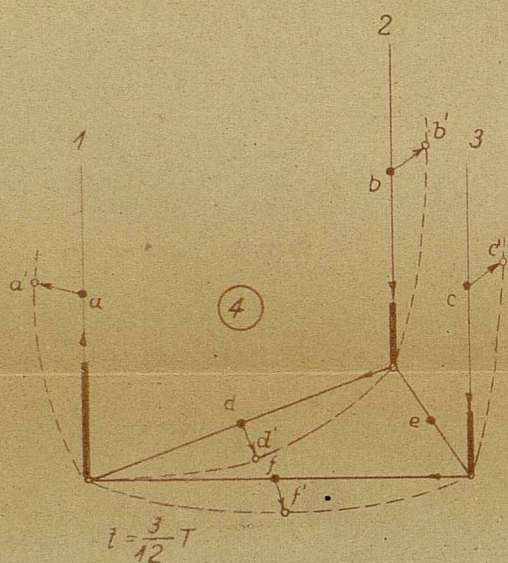
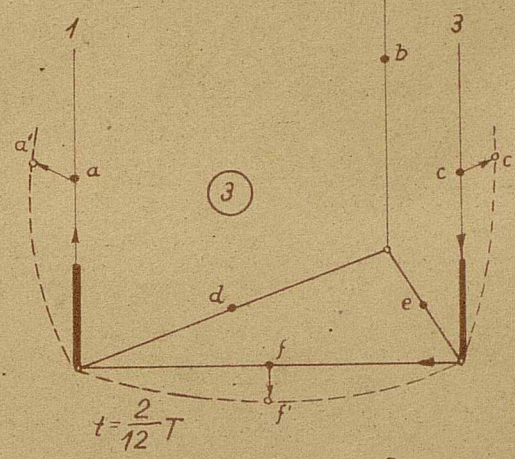
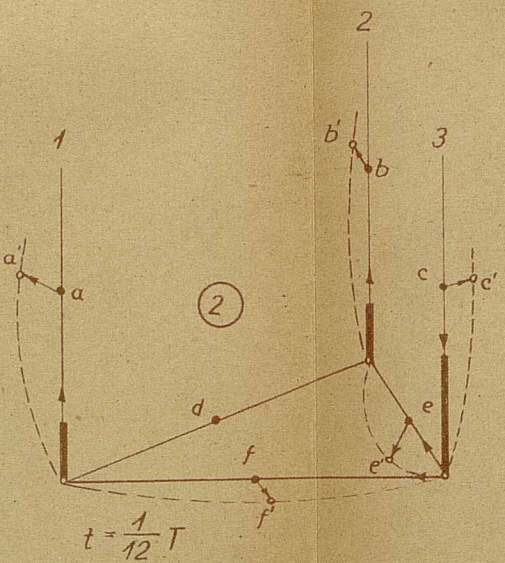
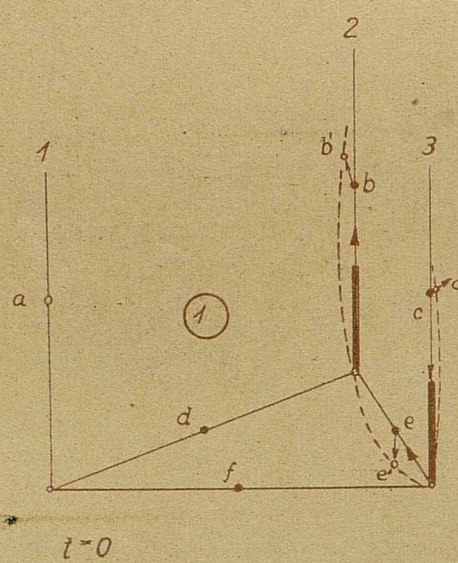


Tabla I. Marcha de corriente en Horno trifasico en las  
diferentes fases de un periodo.

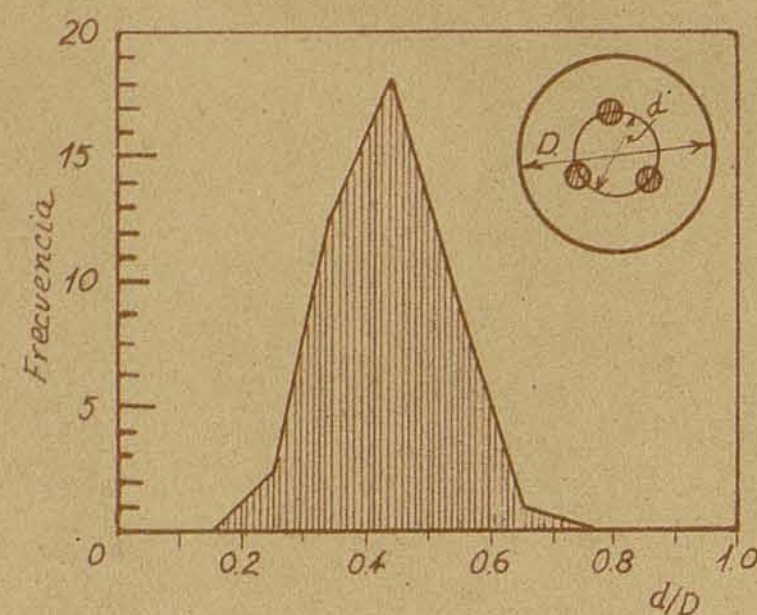
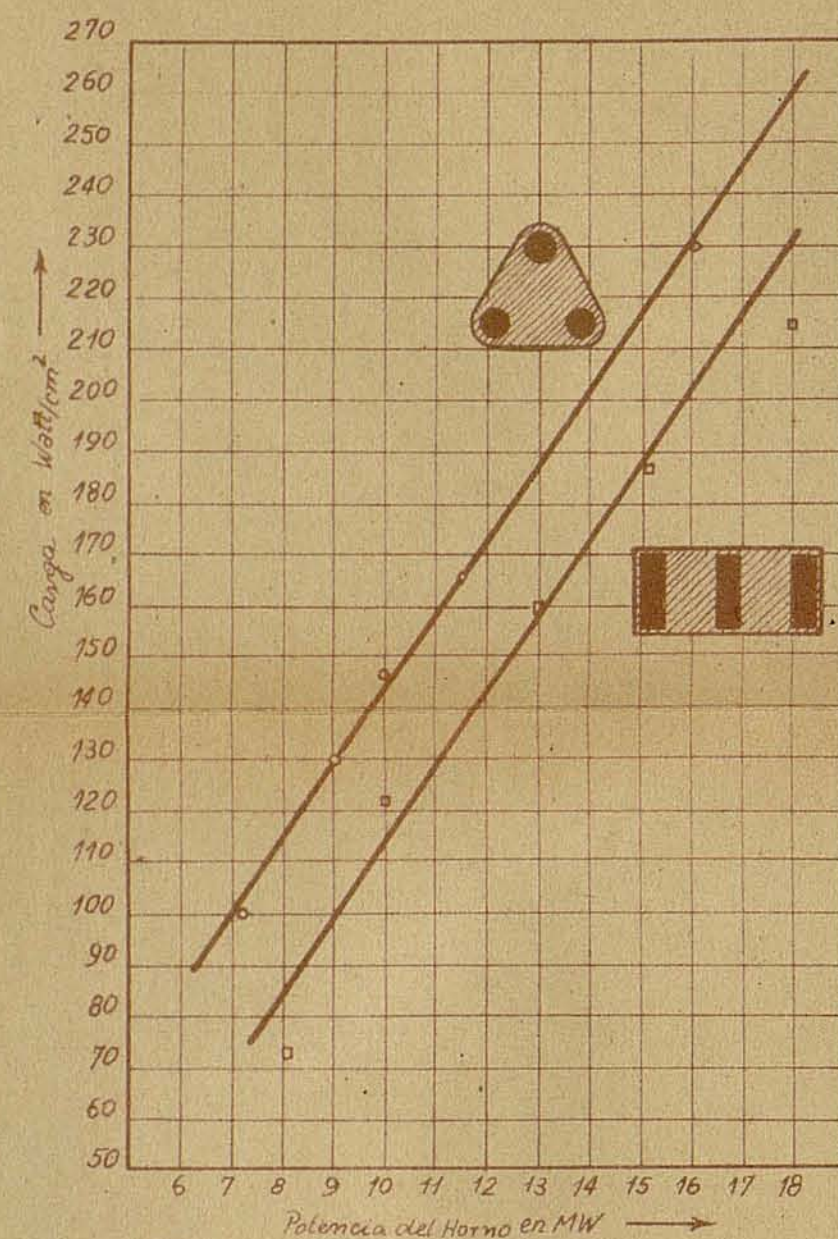
Fig. 187. Relación  $d/D$  en los Hornos eléctricos alemanes

Fig. 188. Carga eléctrica en los Hornos de Carburo de distintas disposiciones de electrodos.

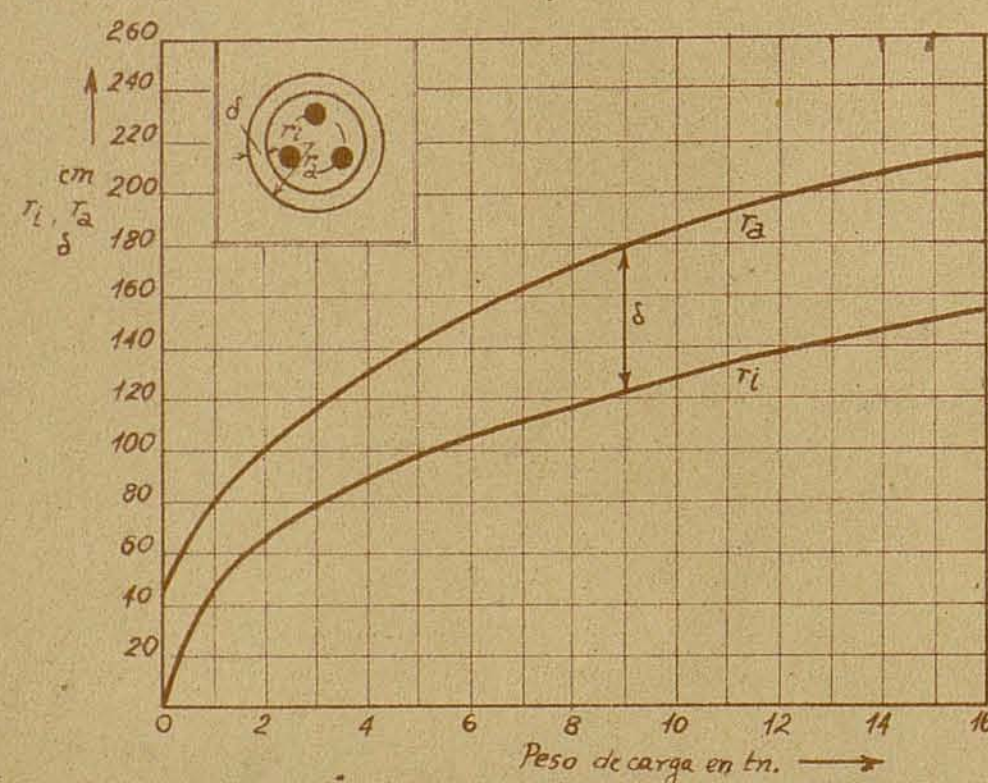


Fig. 189. Radios interno, externo y espesor de paredes

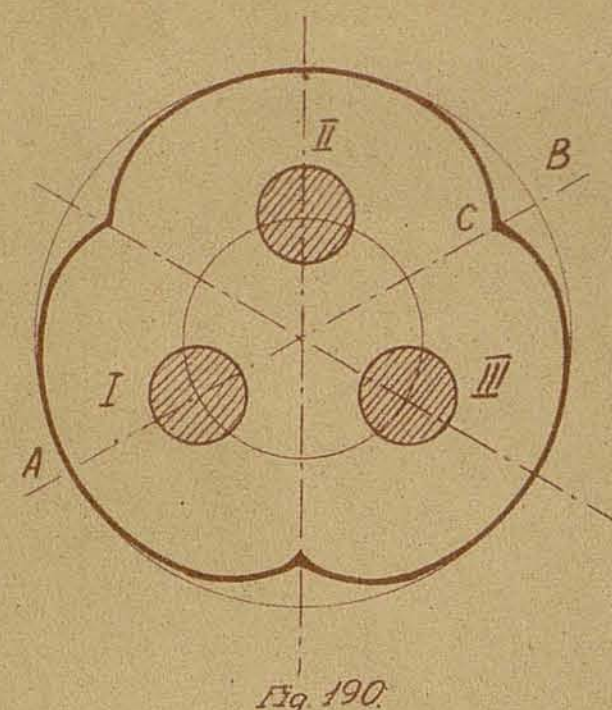


Fig. 190.

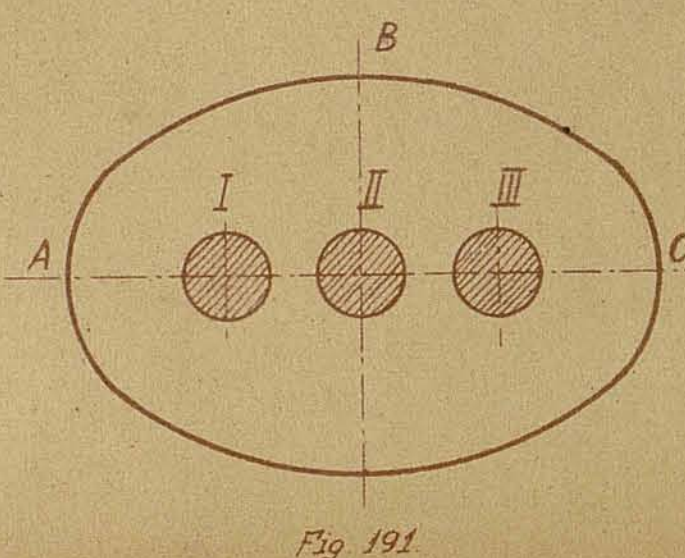


Fig. 191.

| Cuerpo | Volumen | Superficie |
|--------|---------|------------|
|        | 1.00    | 4.83       |
|        | 1.00    | 5.50       |
|        | 1.00    | 6.00       |
|        | 1.00    | 6.16       |
|        | 1.00    | 6.68       |

Fig. 192.

Relación Superficie a Volumen en crisoles de distintas formas.

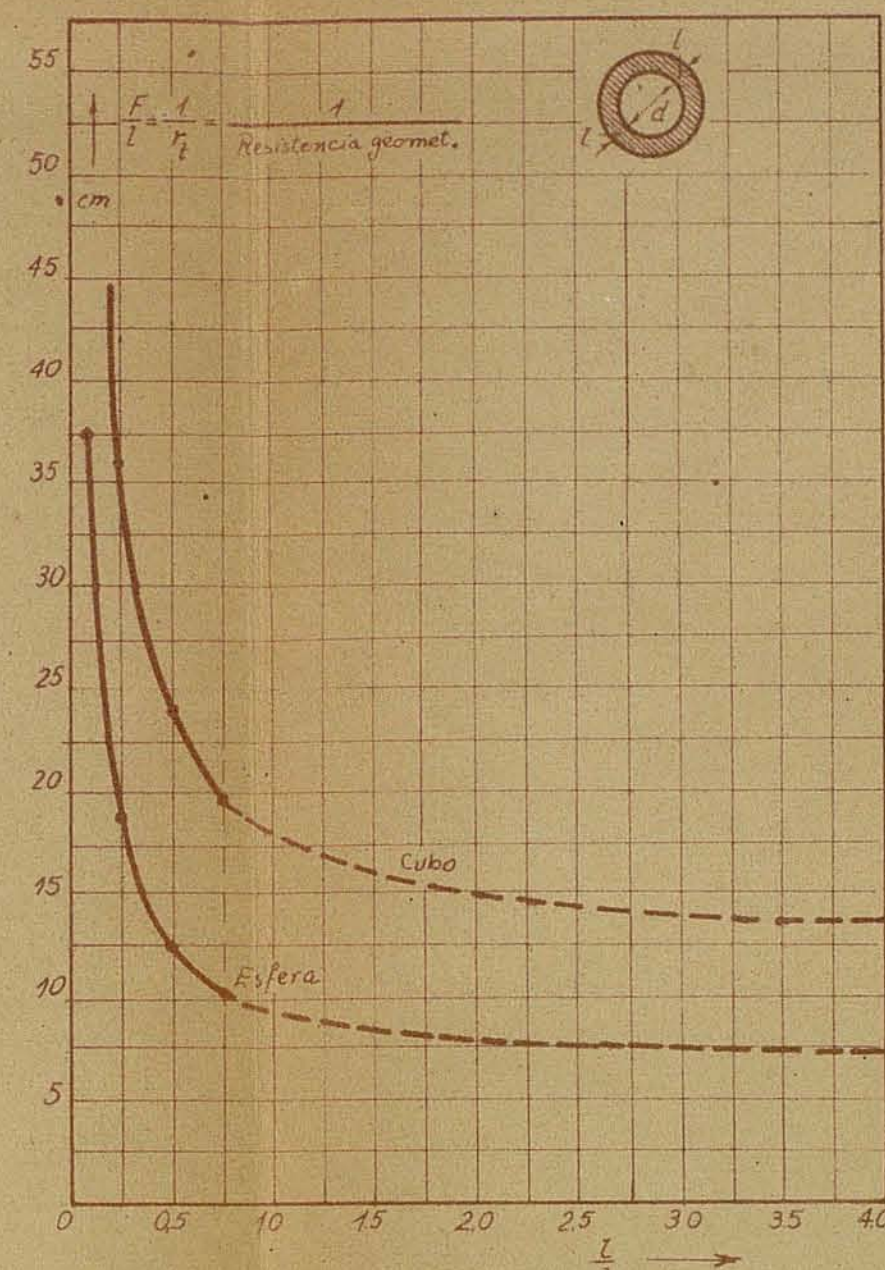


Fig. 195. "Conductibilidad geométrica" o factor de forma para esferas huecas y cubos

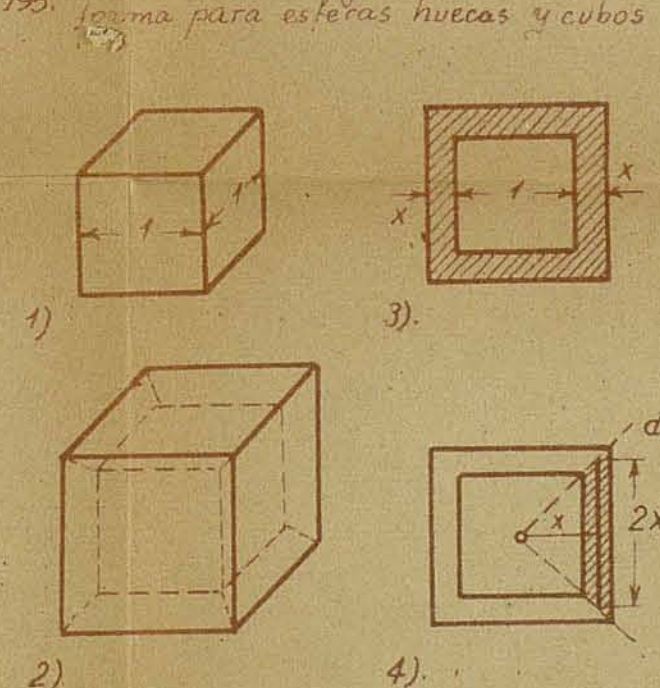


Fig. 196. Determinación de la resistencia geométrica

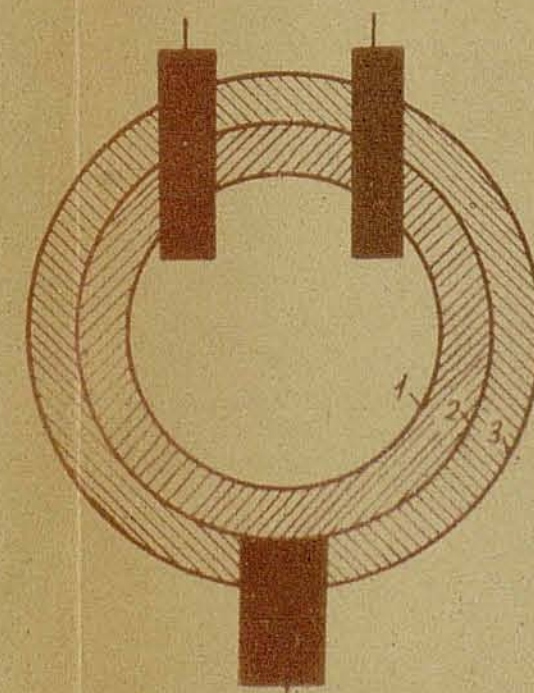


Fig. 198. Crisol con paso parcial de corriente a través del aislante térmico al electrodo de solera.

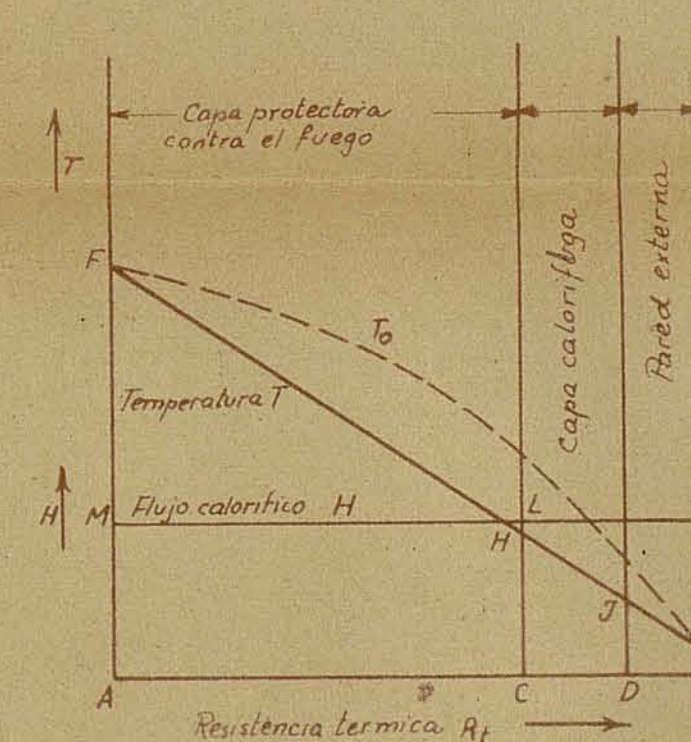


Fig. 199. Esquema de la potencia térmica de un horno eléctrico (Kawasaki)

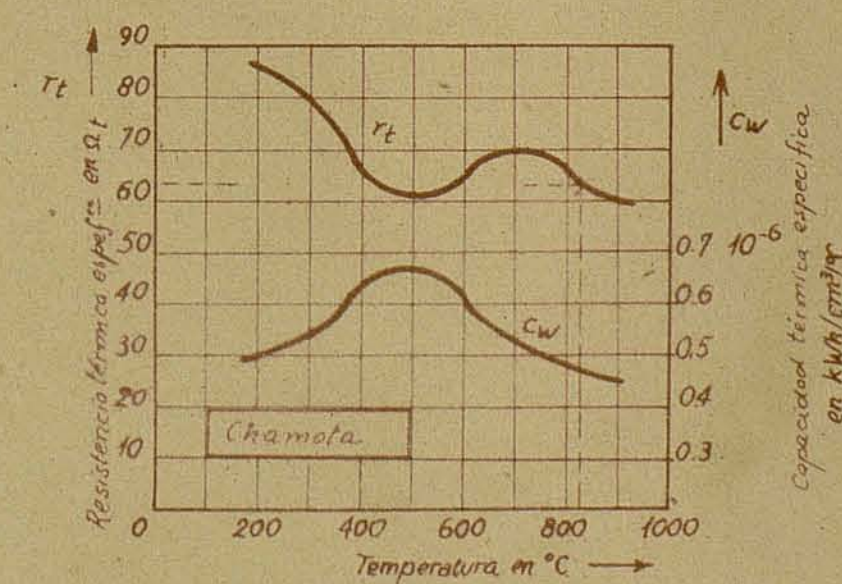


Fig. 204. Característica para la chamota (Ejemplo de Kawasaki)

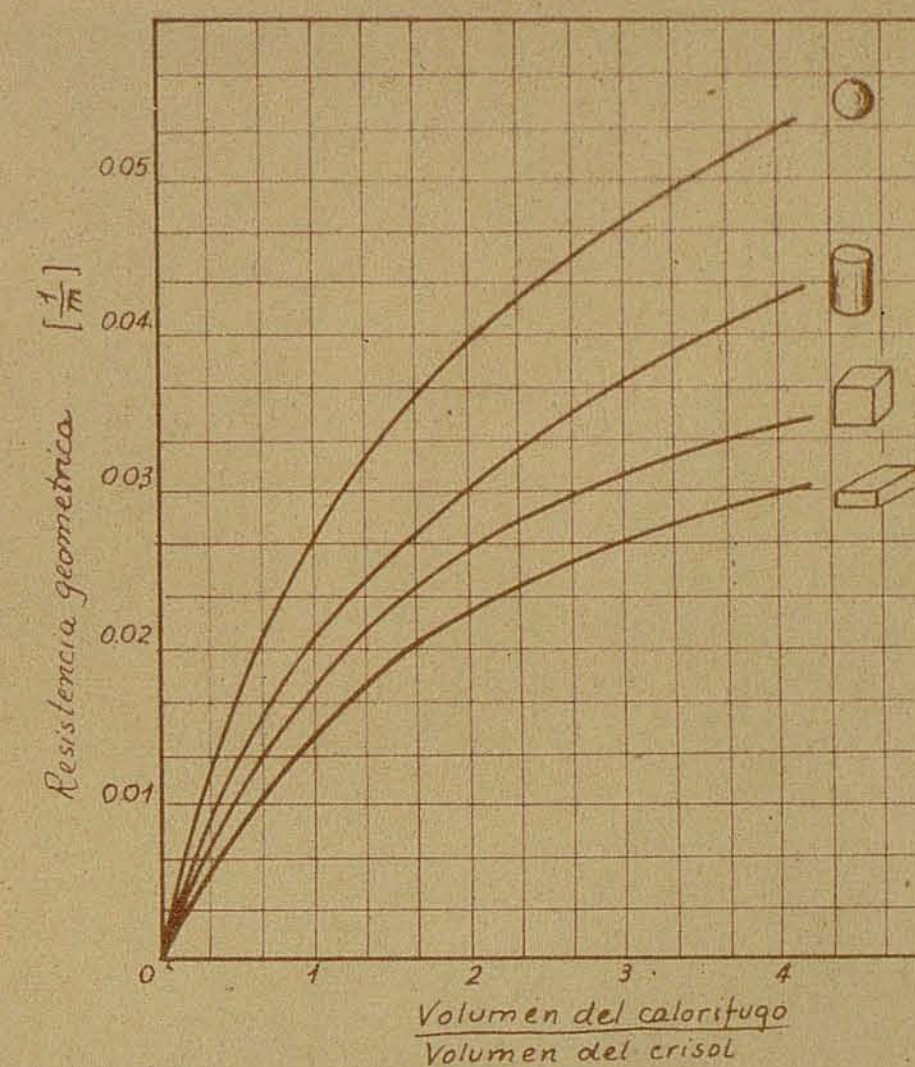


Fig. 197.

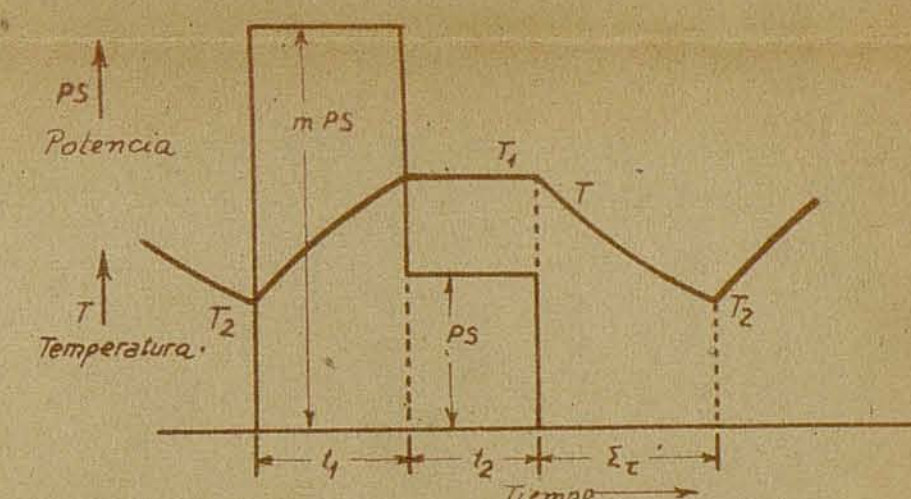


Fig. 200. Esquema termico

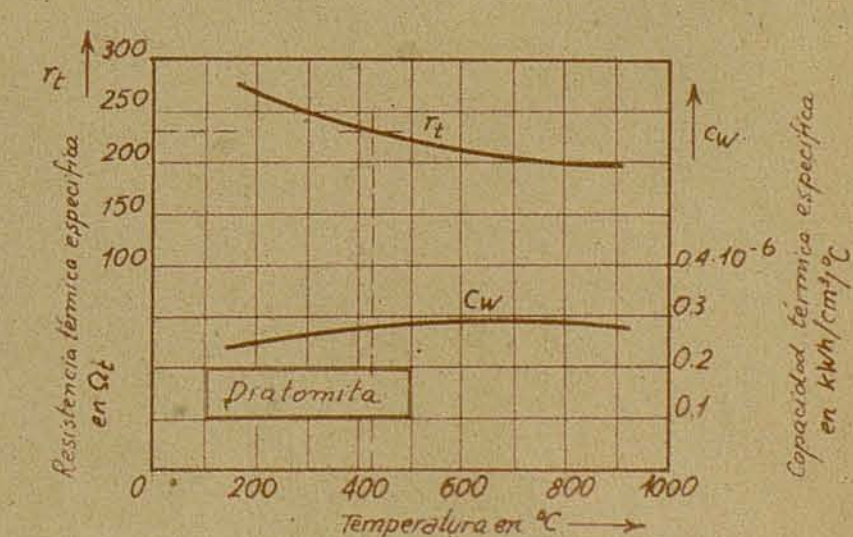


Fig. 205. Característica para la diatomita (Referente al ejemplo de Kawasaki)

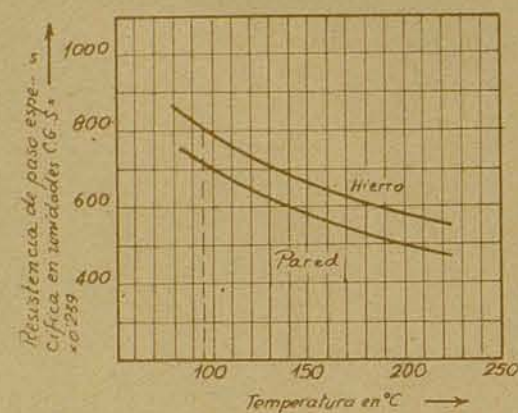


Fig. 206. Resistencia de paso de calor en superficies, según Kawasakiya

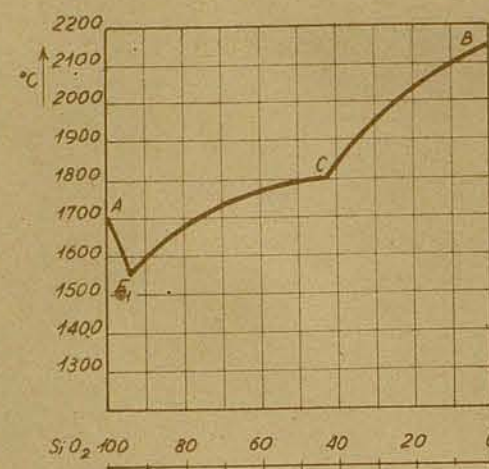


Fig. 209. Línea de fusión del sistema  $Al_2O_3-SiO_2$

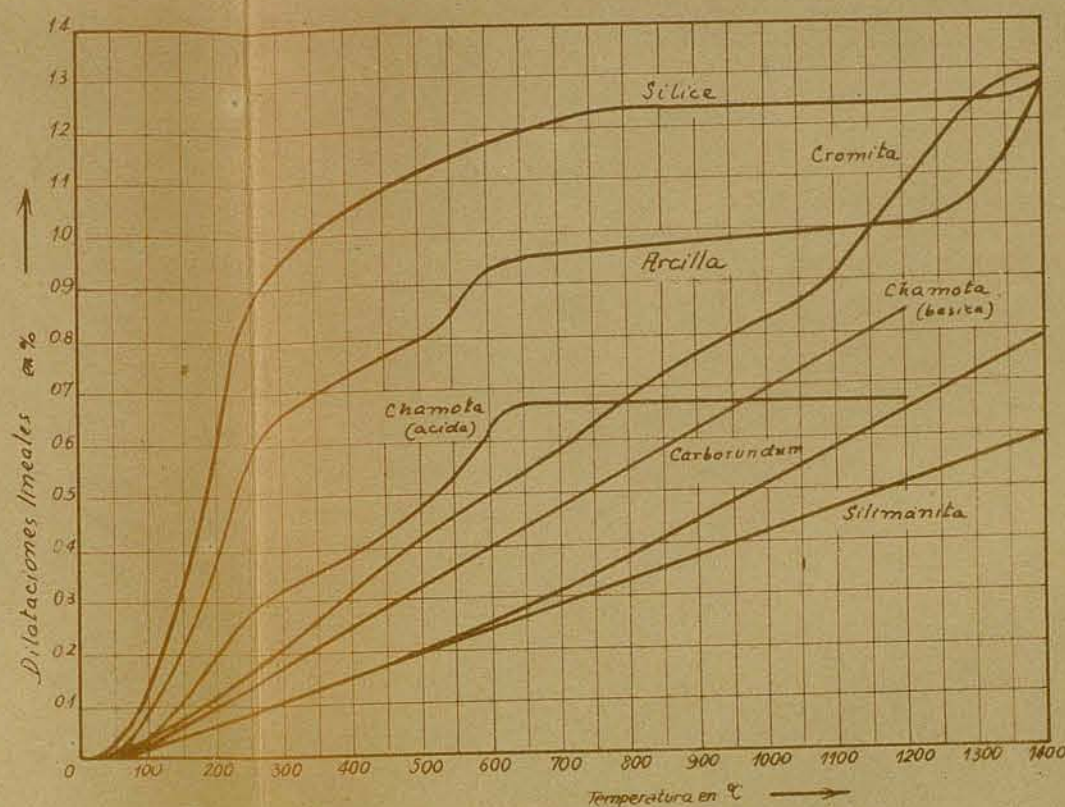


Fig. 210. Dilatación térmica de los refractarios

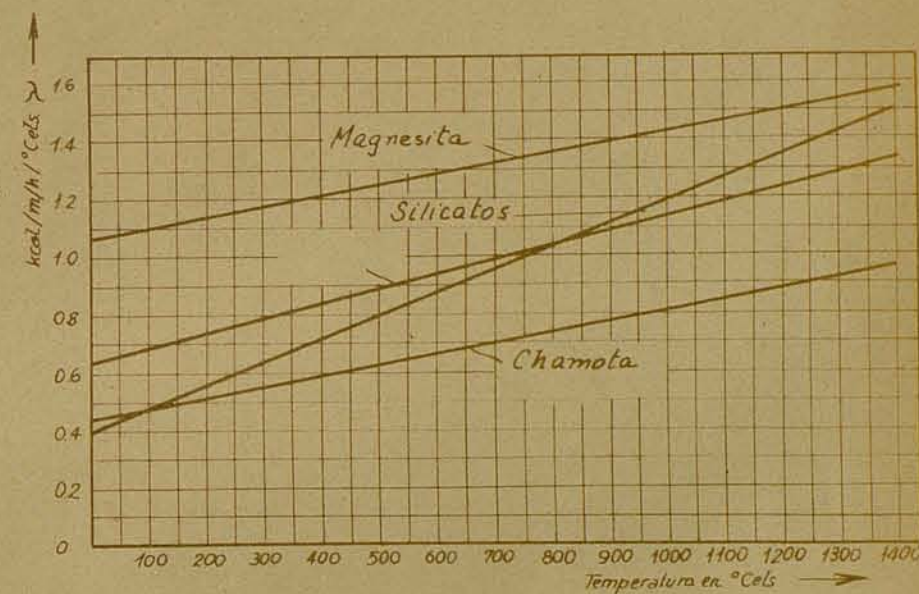


Fig. 212

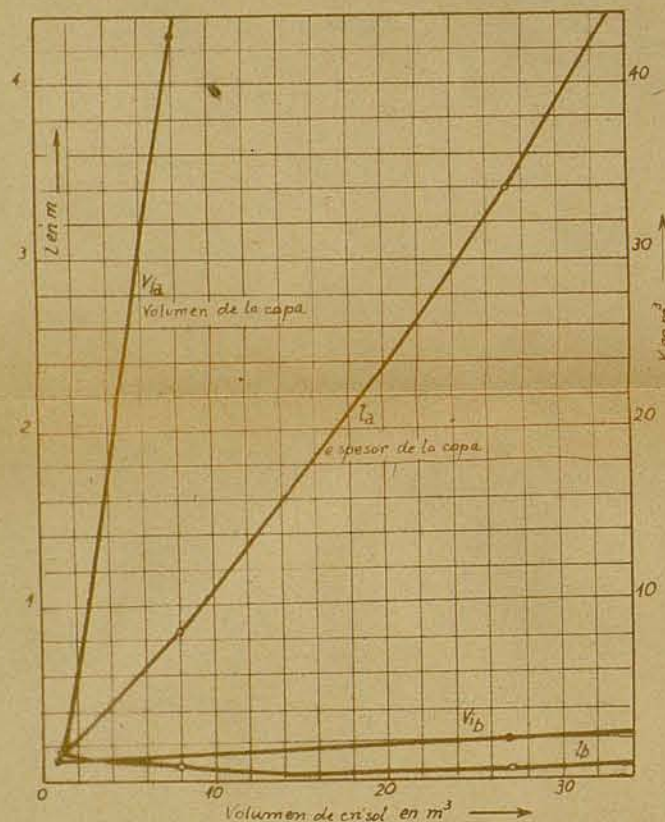


Fig. 207. Volumen  $V_i$  y espesor  $l$  de la capa aislante al variar el volumen de crisol cúbico  
a) Perdidas constantes absolutas de calor  
b) " " " " por  $m^3$  de volumen de crisol

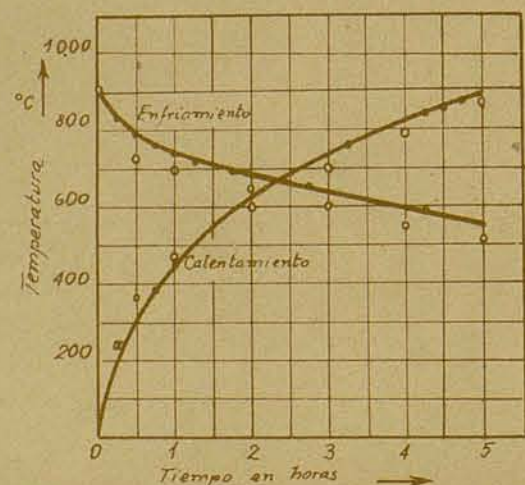


Fig. 208. Calentamiento y enfriamiento de un horno según valores técnicos y experimentales

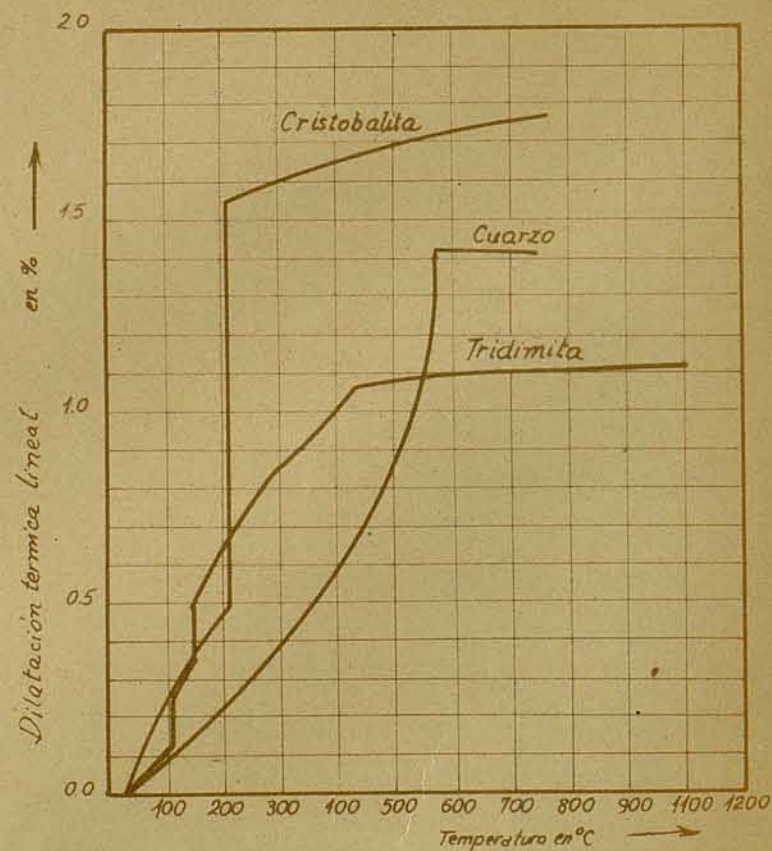


Fig. 211

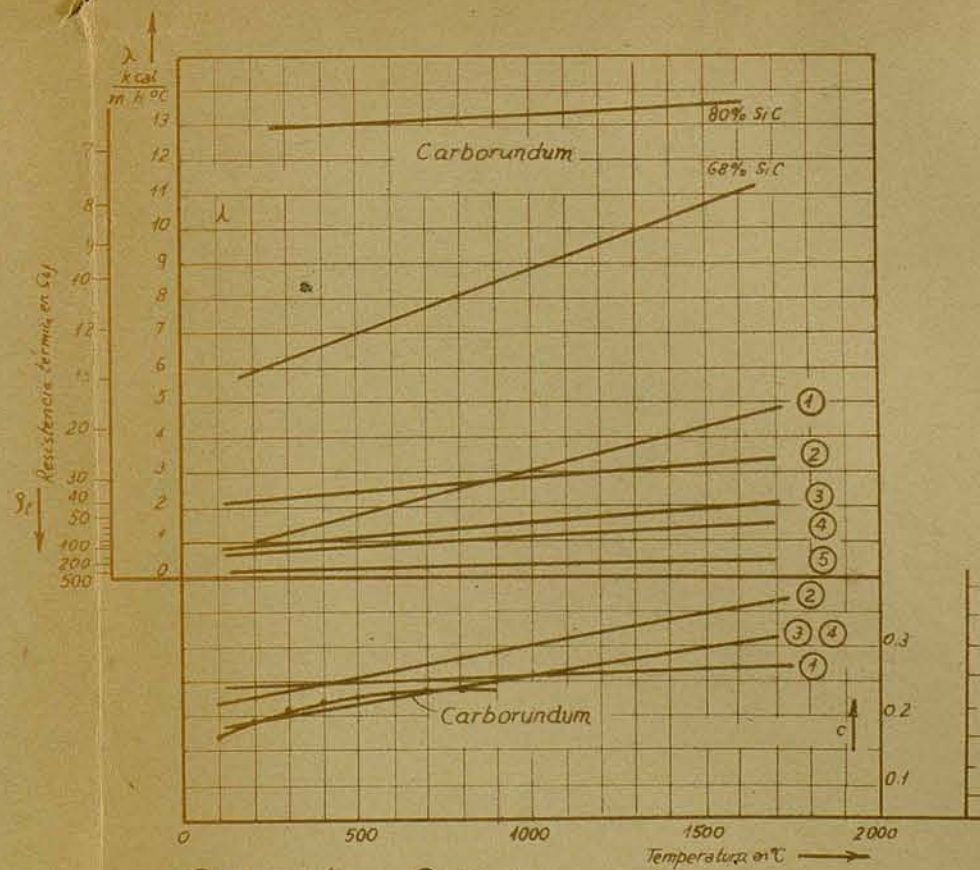


Fig. 213. Cifras características de refractarios.

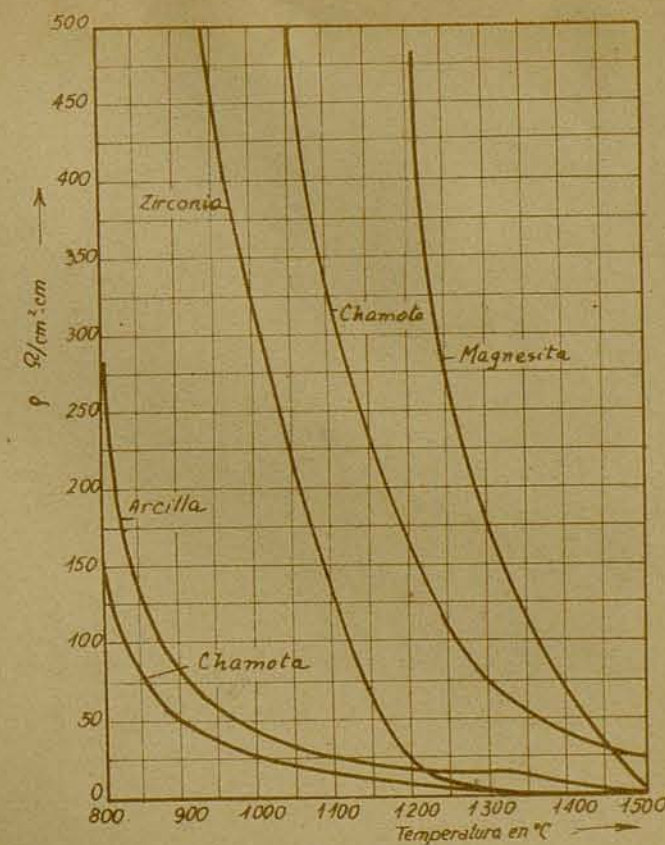


Fig. 215

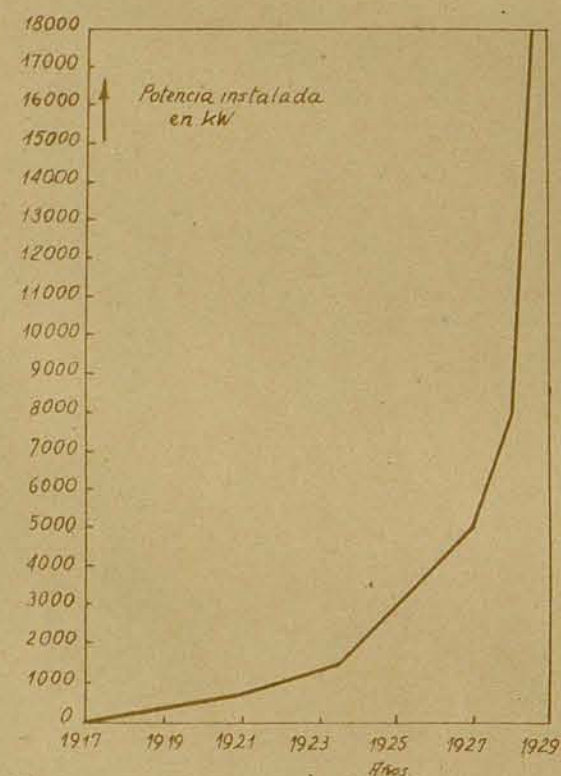


Fig. 216.

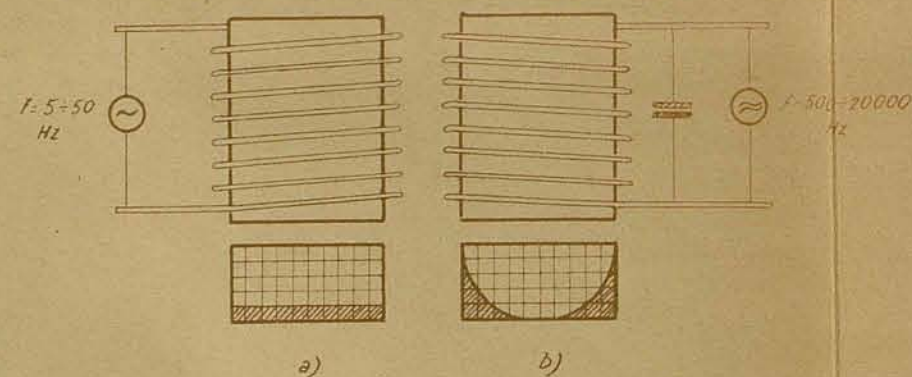


Fig. 220.

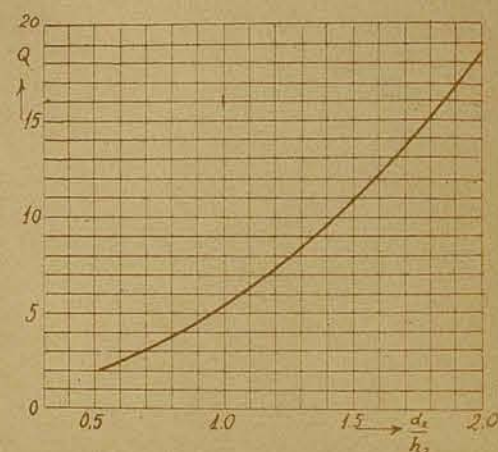


Fig. 222.

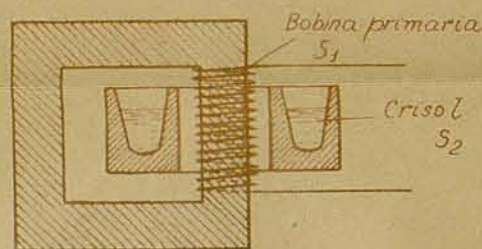


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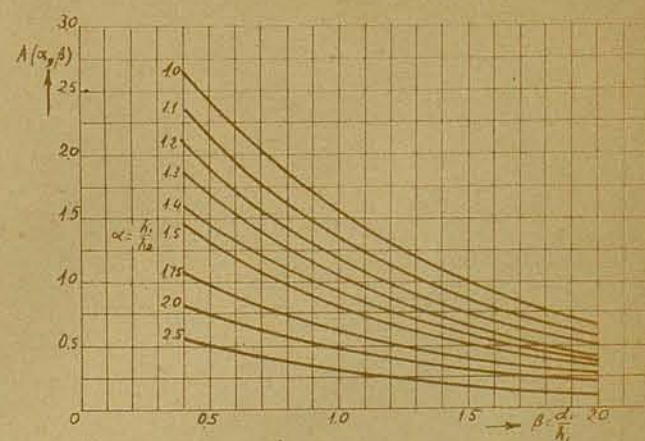


Fig. 223.

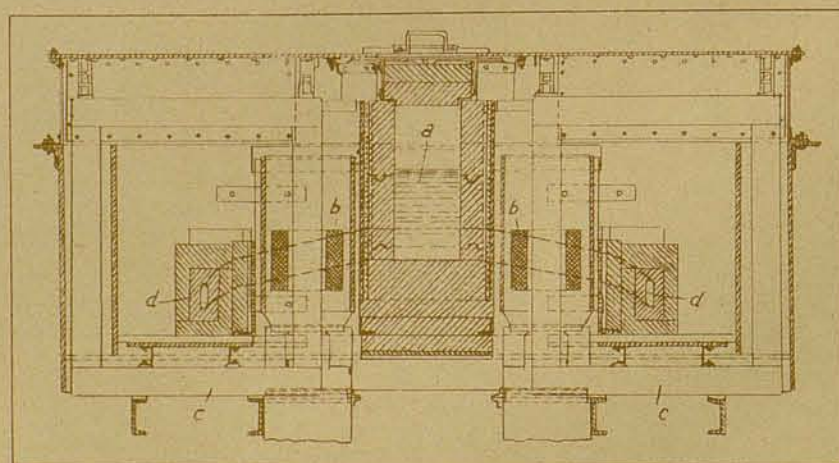


Fig. 218. Horno de inducción de baja frecuencia para refusión de aleaciones  
a = crisol central, b = bobina primaria, c = núcleo de hierro, d = arrollo secundario

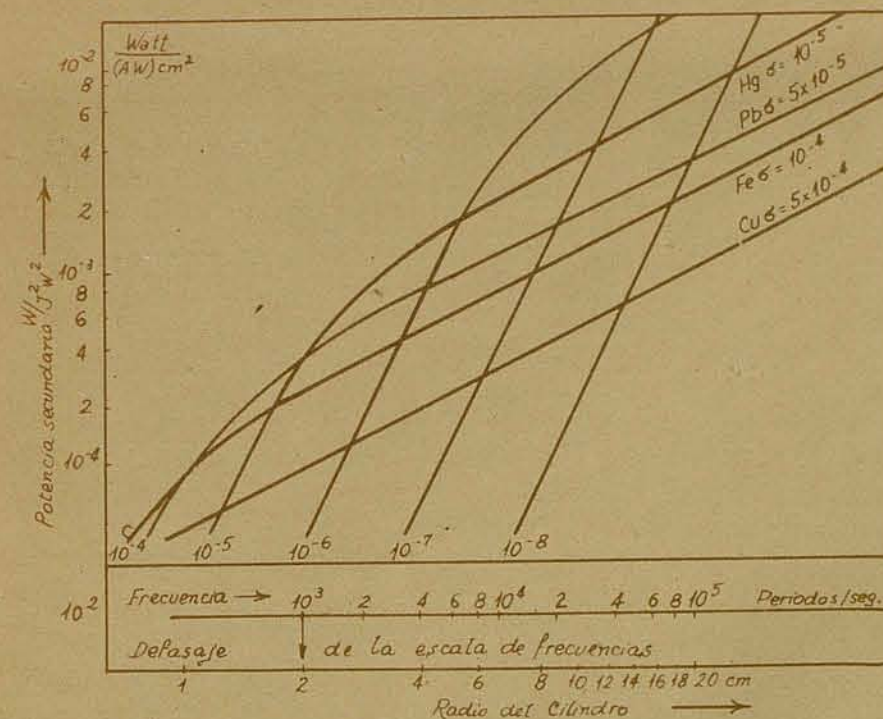


Fig. 224.



Fig. 225. función  $F = f(d/h)$ . (según Esmarch).

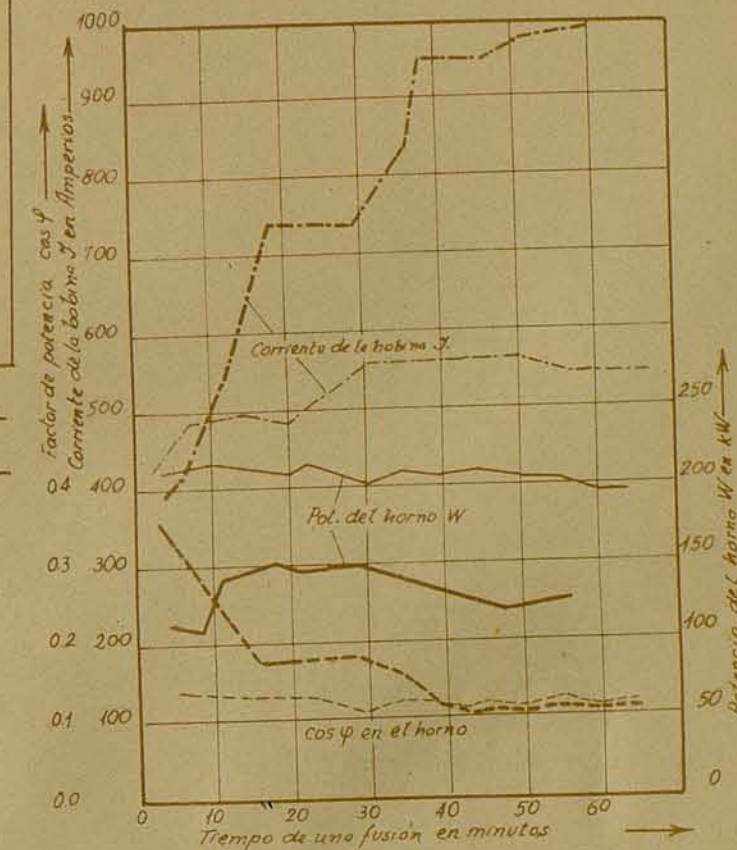


Fig. 227.

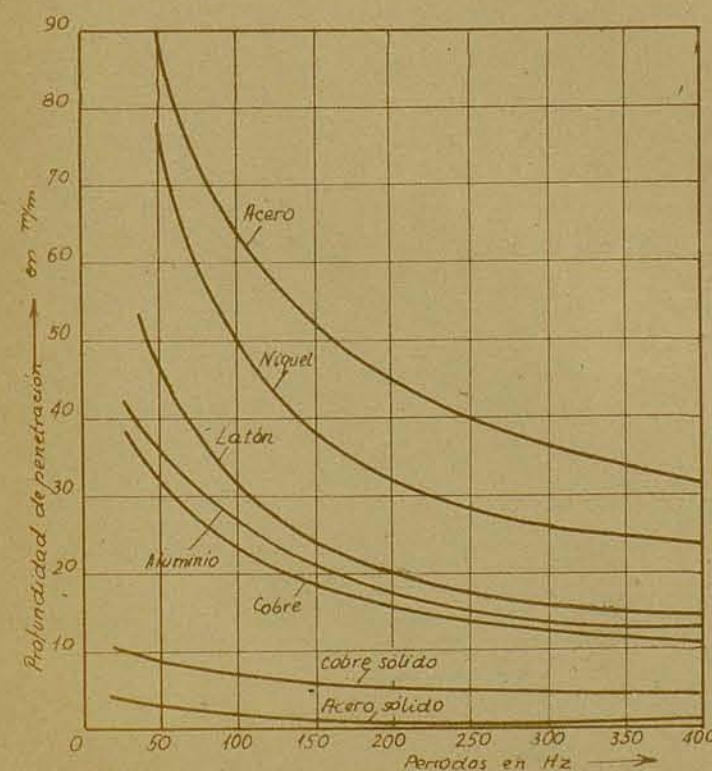


Fig. 226.

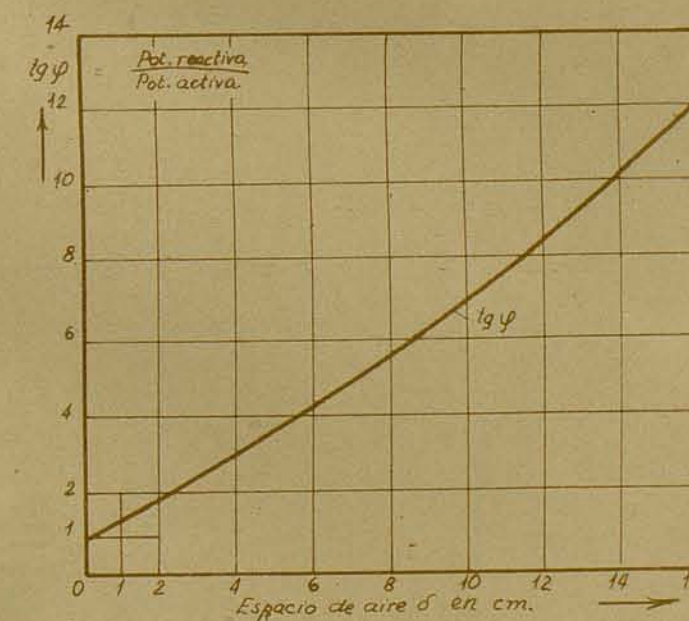


Fig. 228.

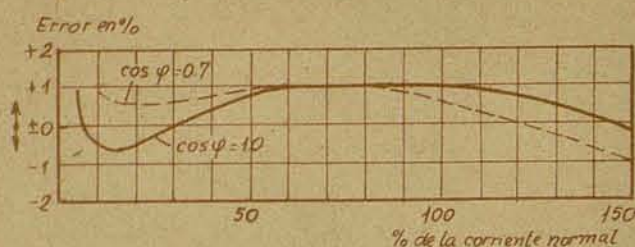


Fig 229.

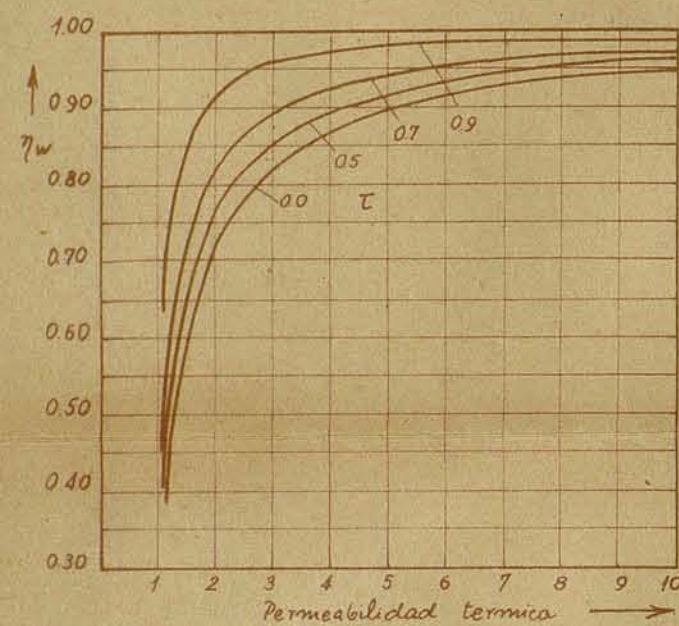


Fig. 232.

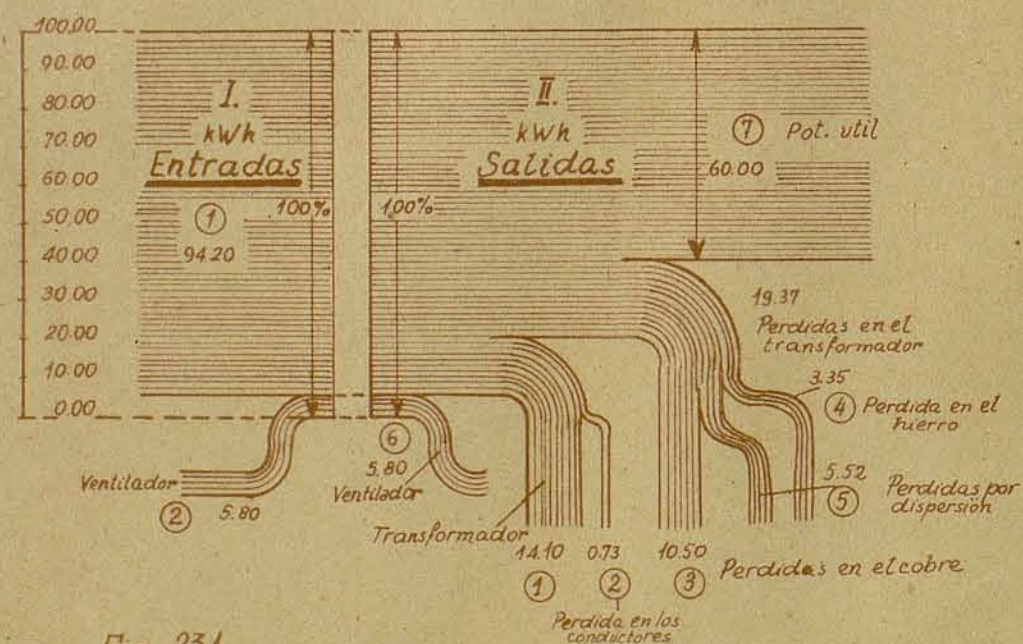


Fig. 231.

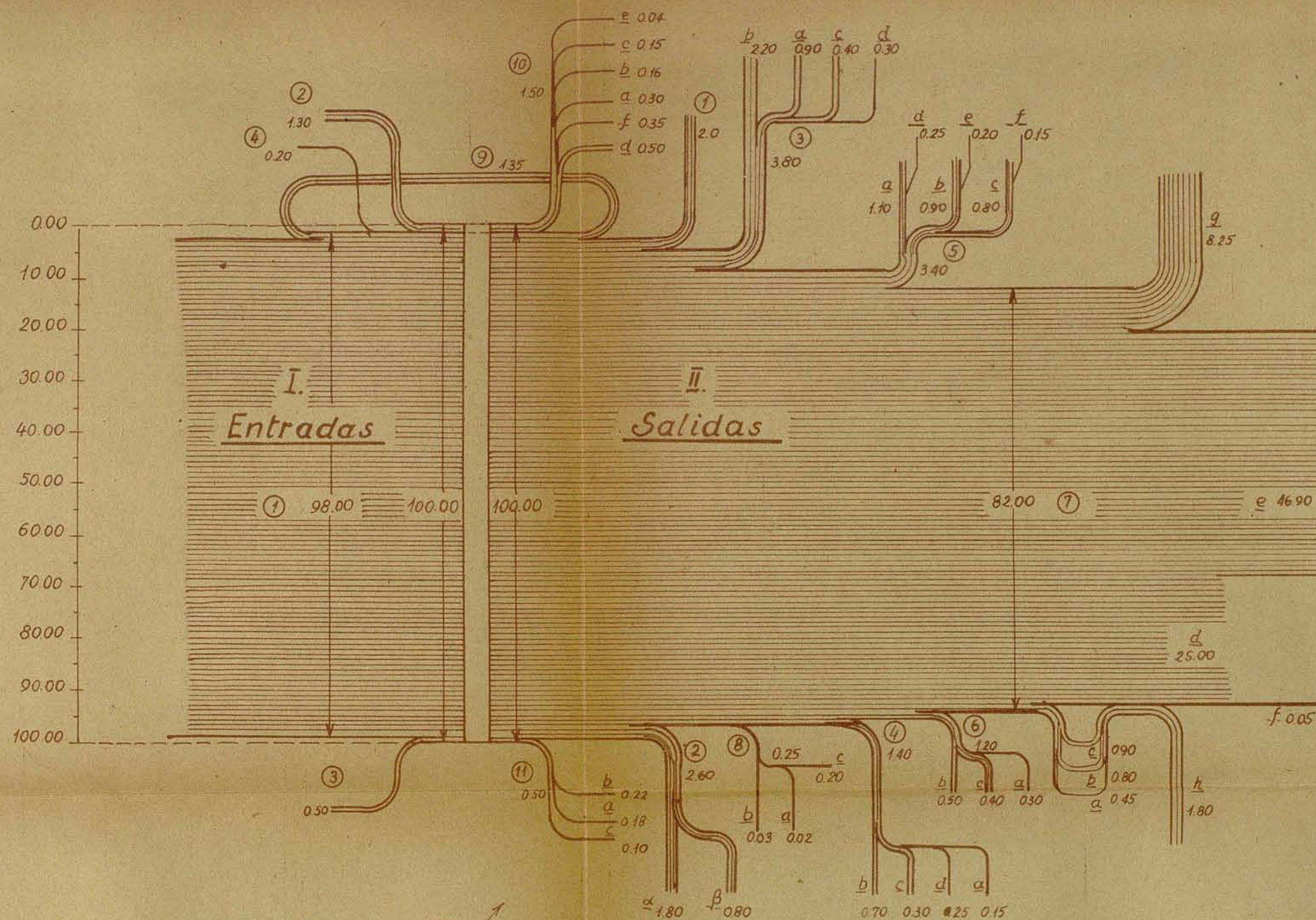


Fig. 230

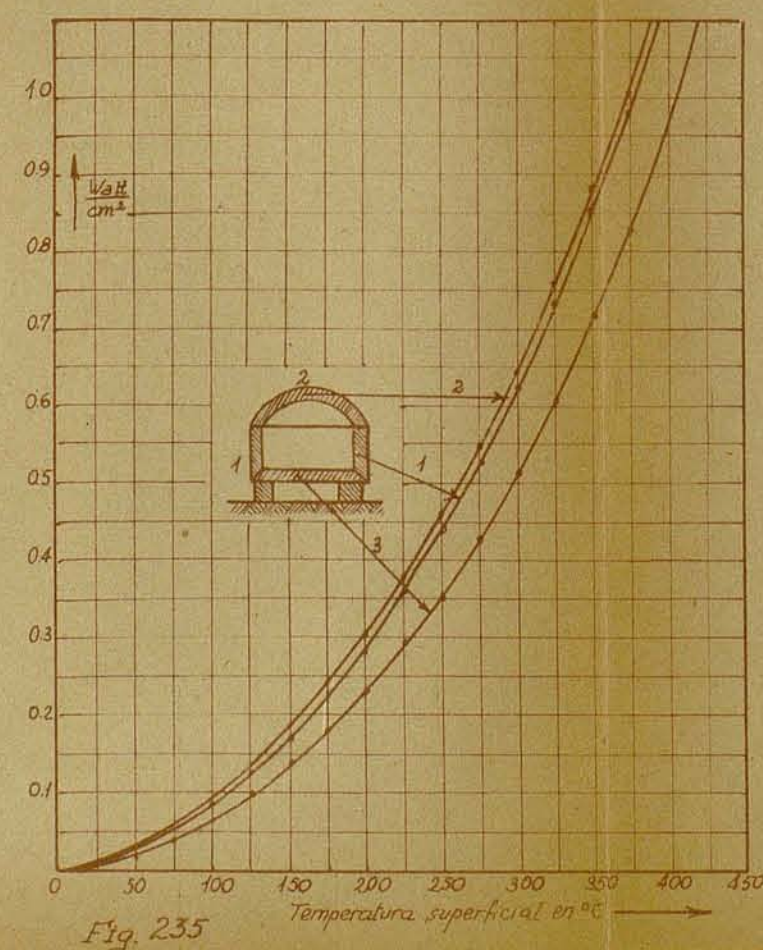


Fig. 235



Fig. 236

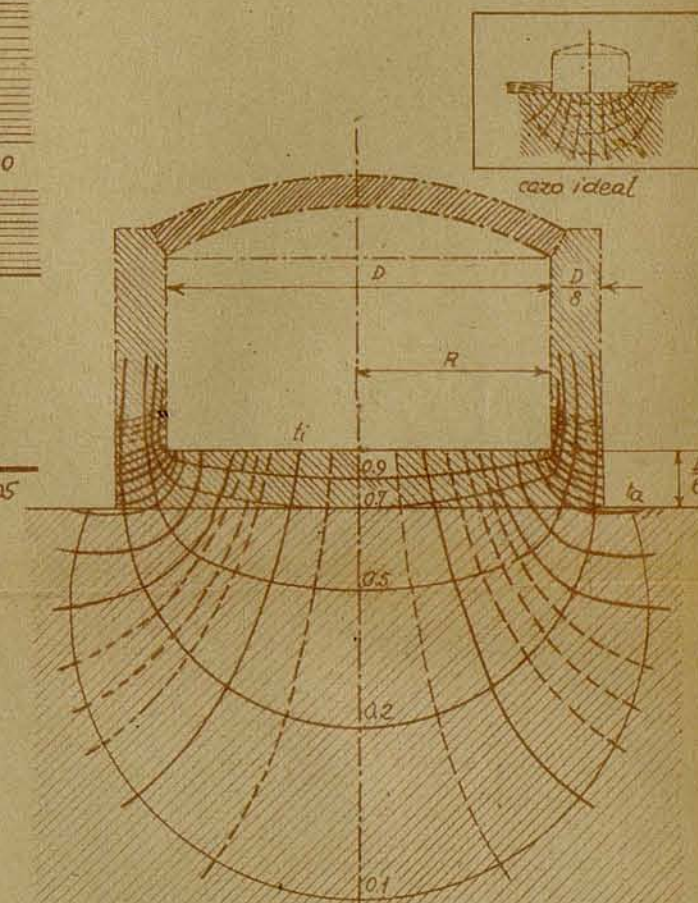


Fig. 234.

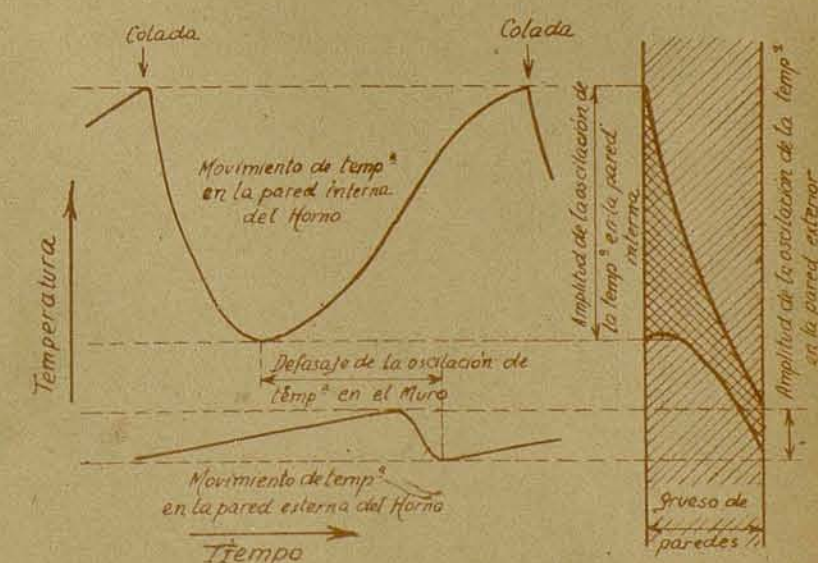


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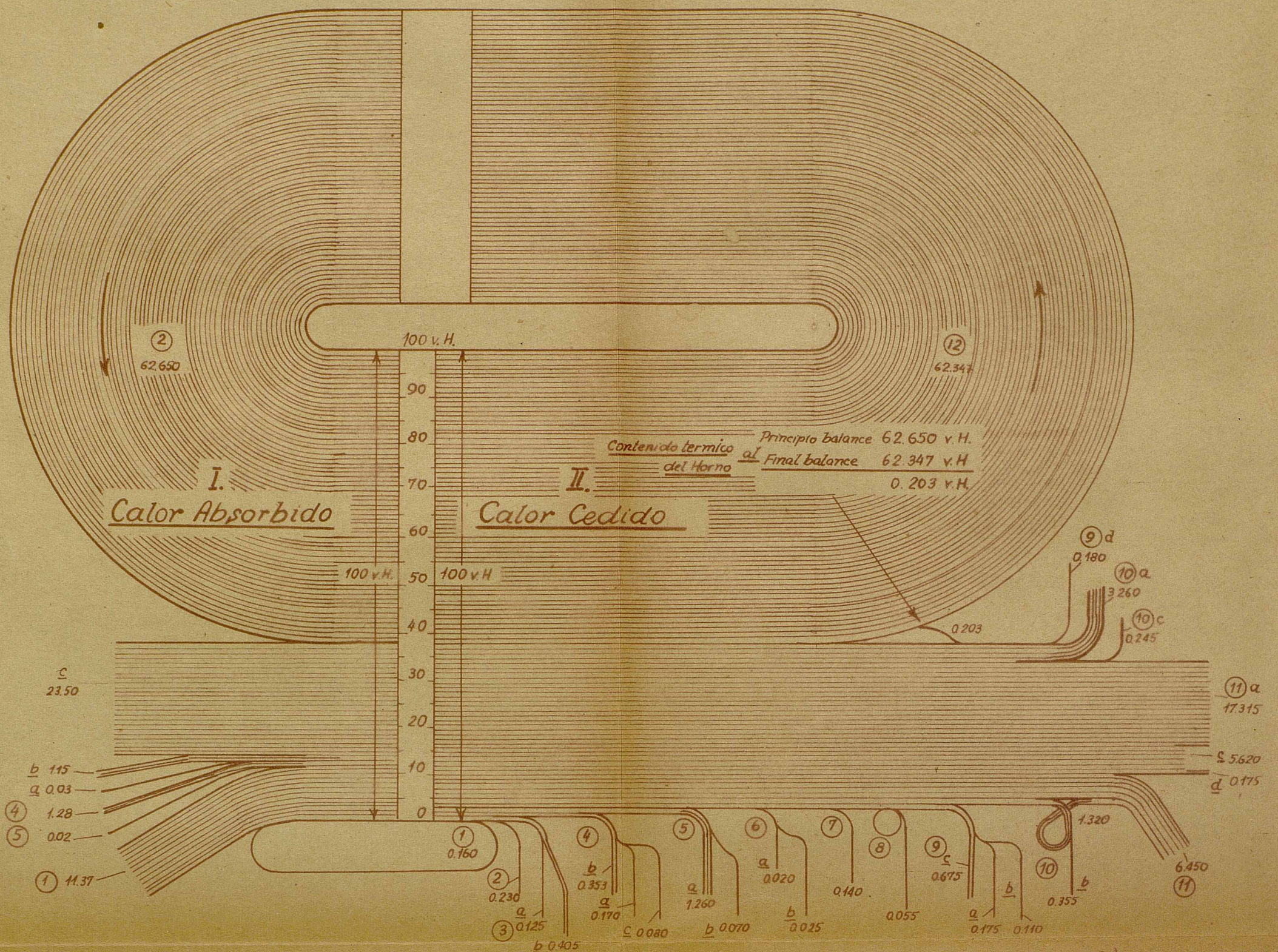


Fig. 242. Ejemplo del balance termico de un gran horno de fusion (con tiempo de comparacion demasiado pequeño)

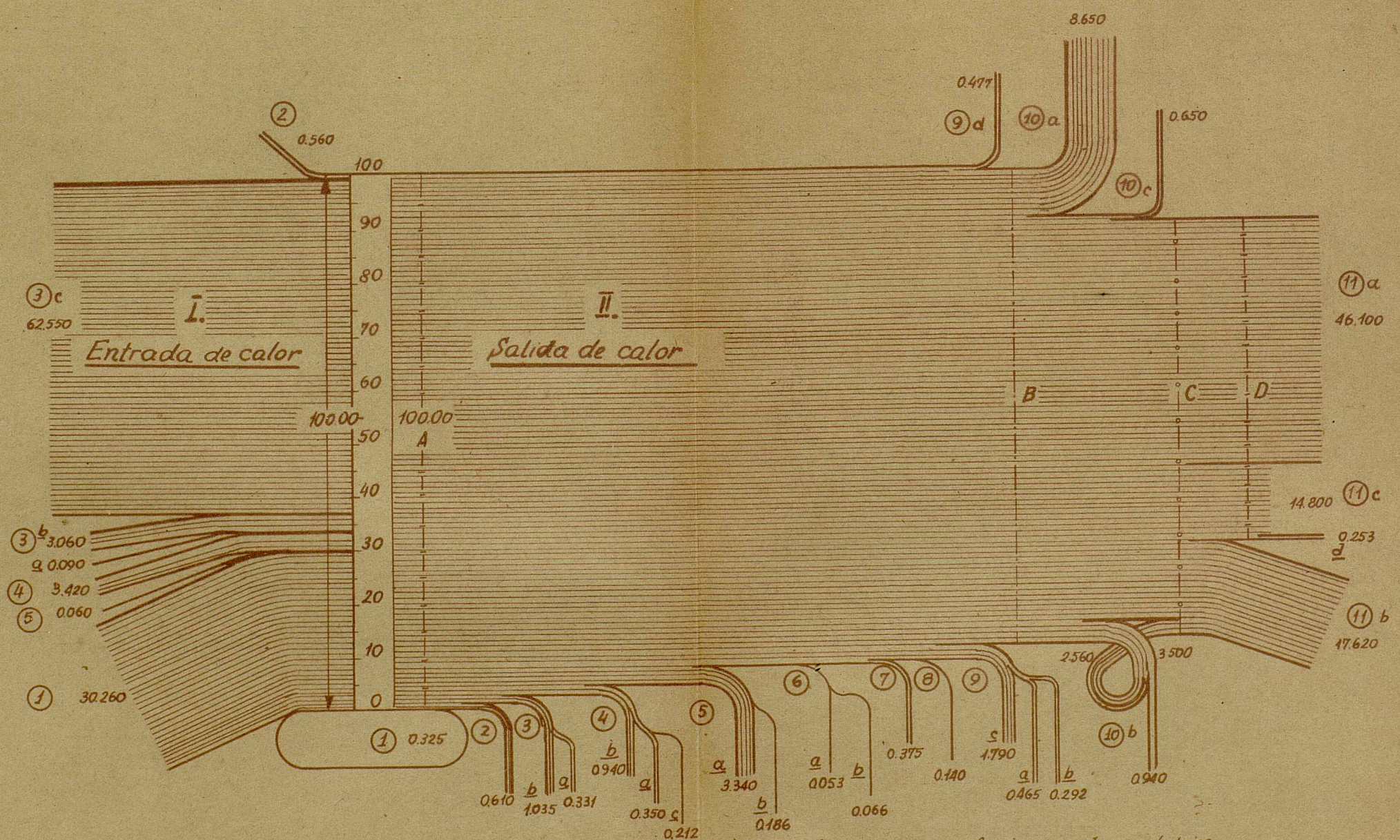


Fig. 243. Calculo de ganancia y perdida de energia calorifica en el proceso de fusion de un horno electrico

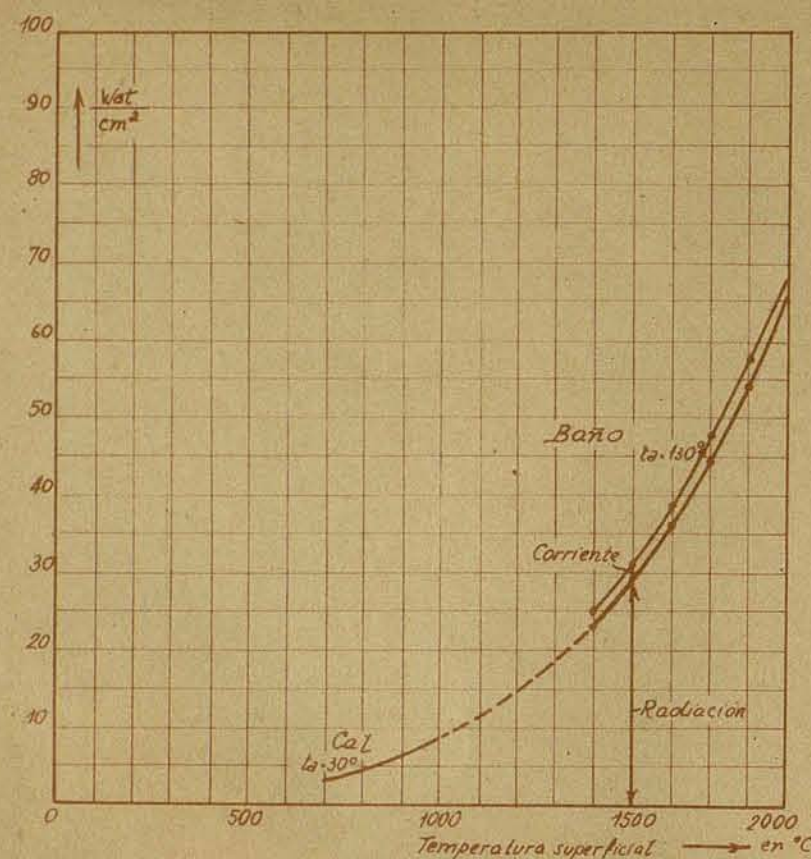


Fig. 237.

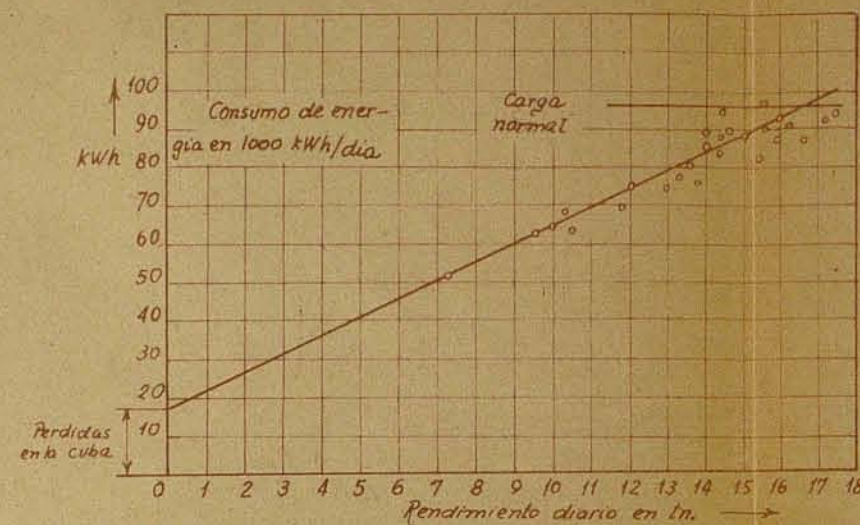


Fig. 239.

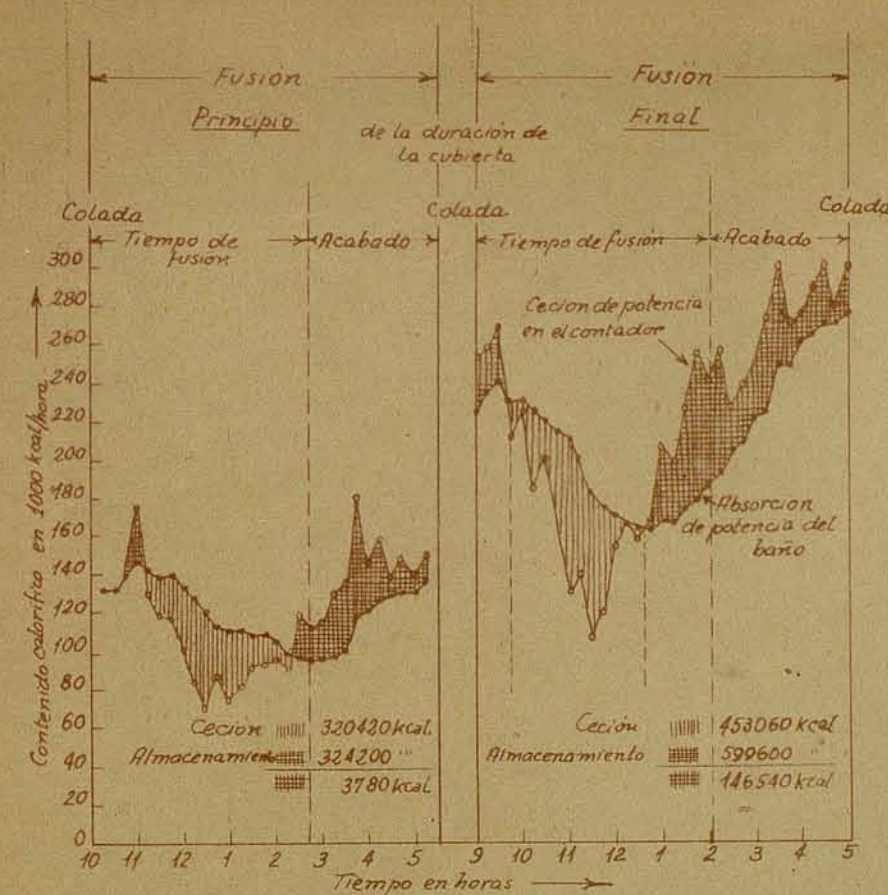


Fig. 241.

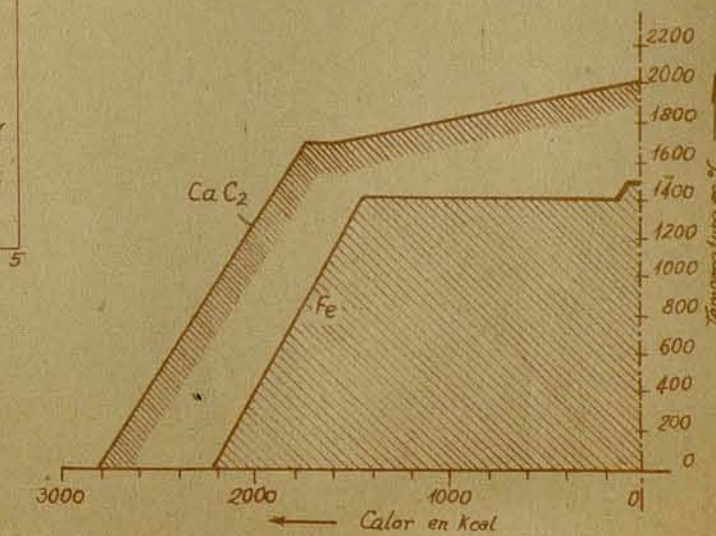


Fig. 245.

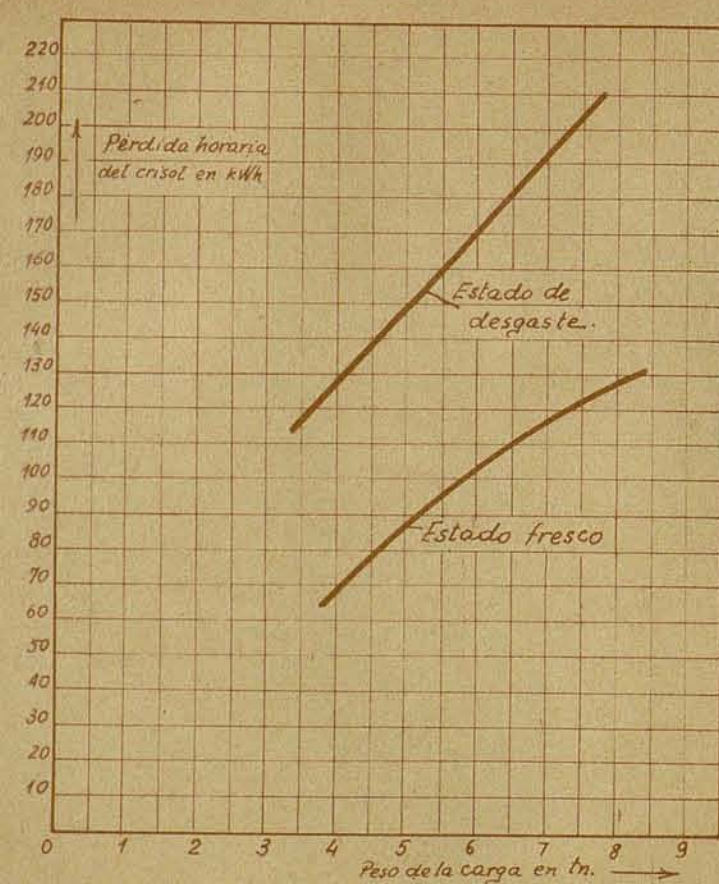


Fig. 238.

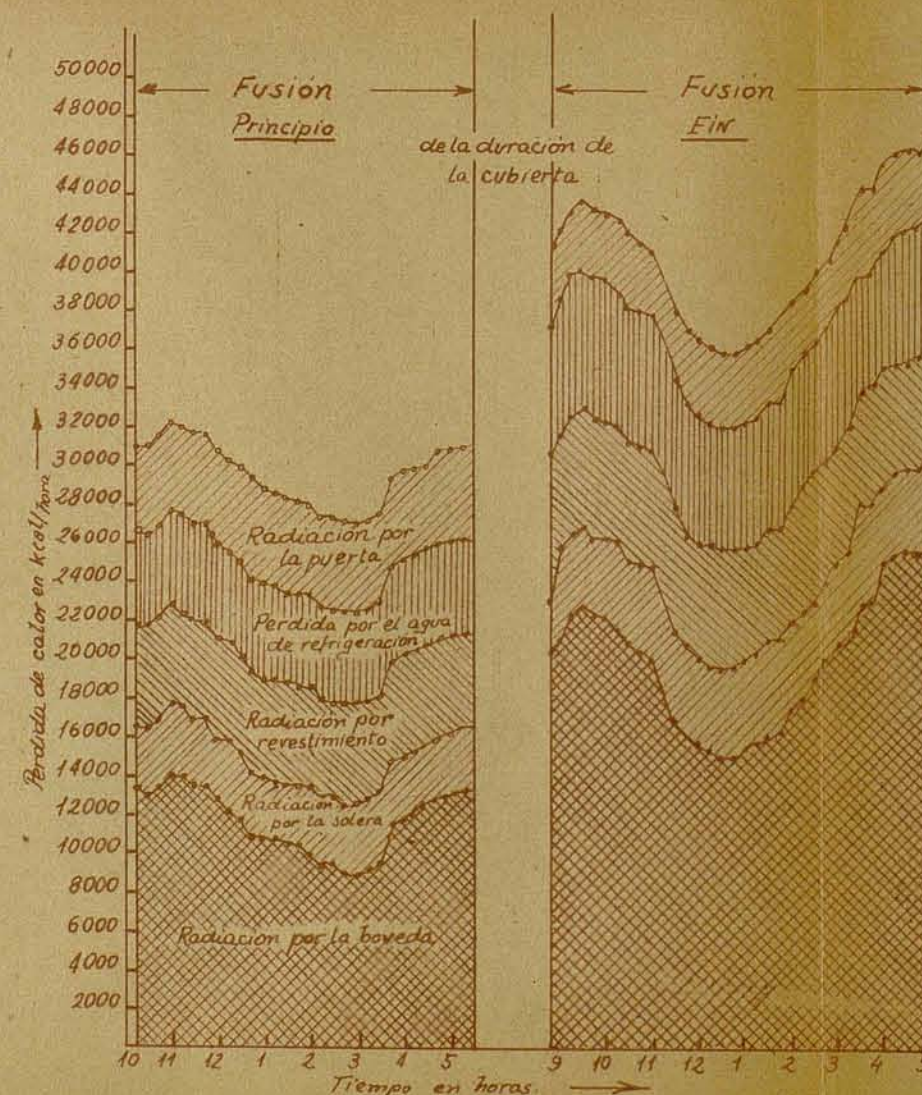


Fig. 240.

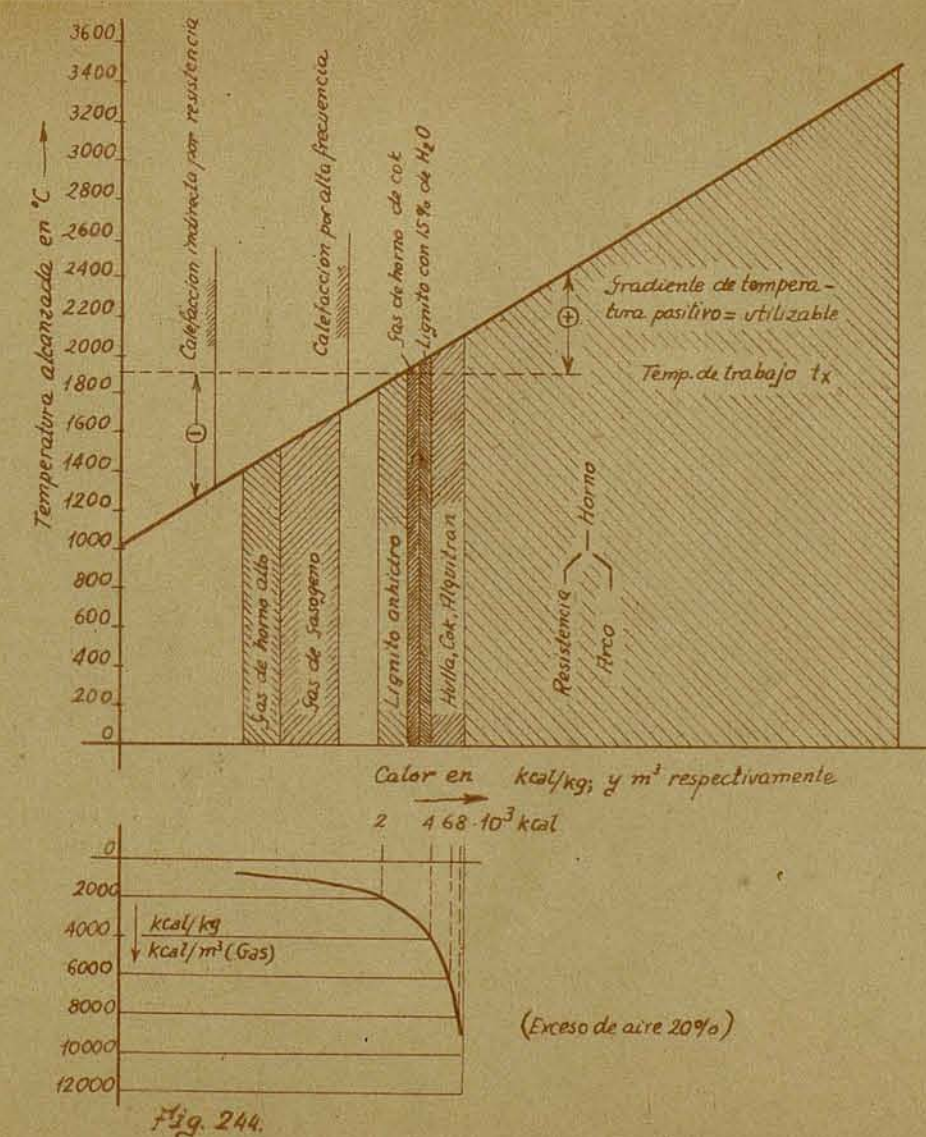


Fig. 244.

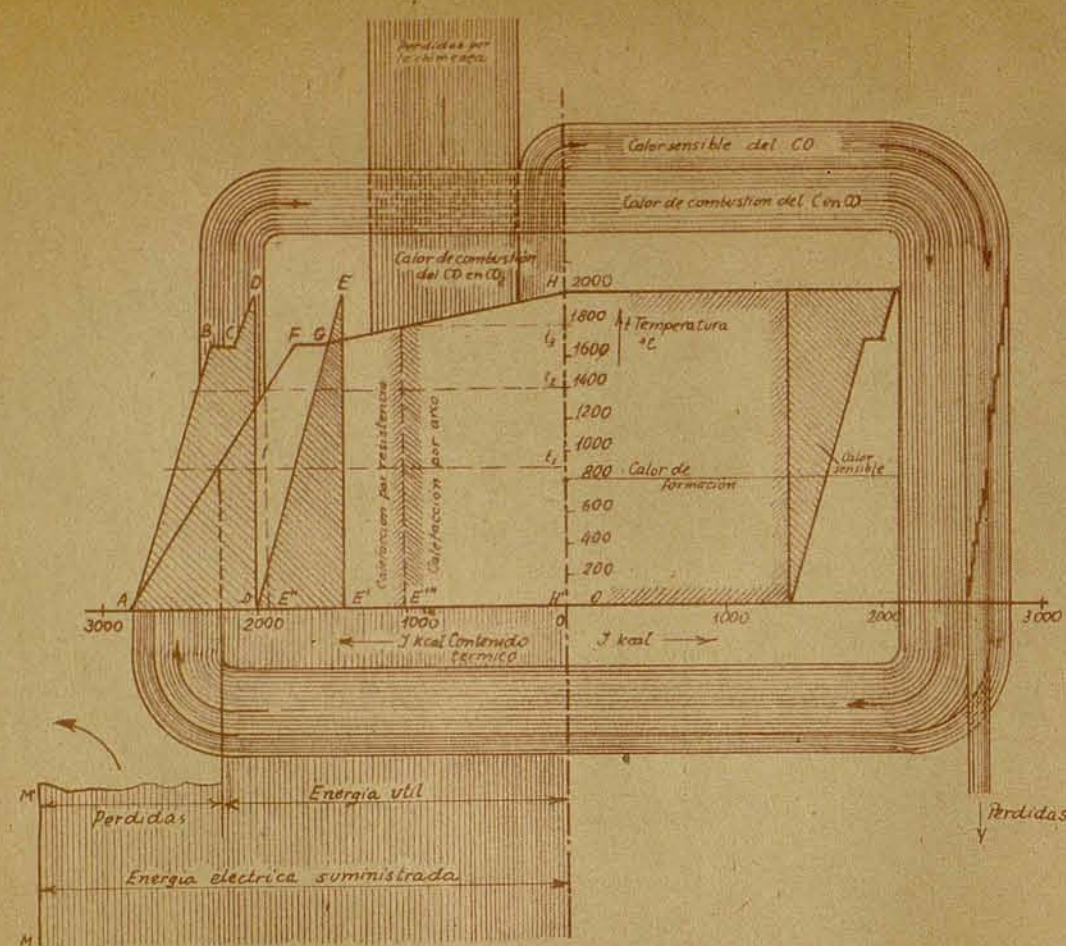


Fig. 246.

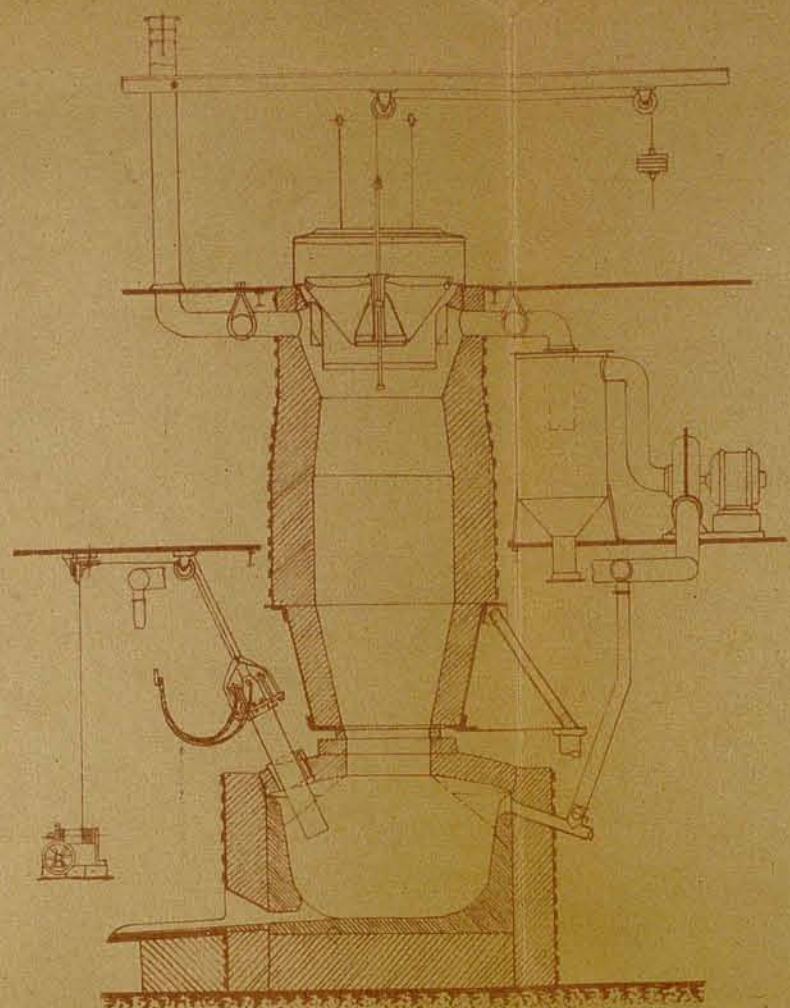
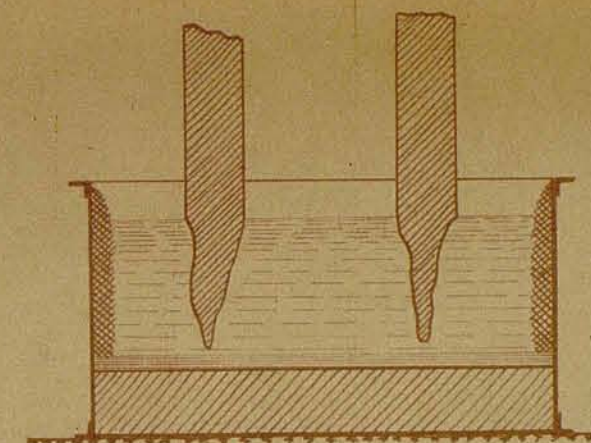
Fig. 247. Horno alto eléctrico  
(corte longitudinal)

Fig. 251. Exesiva penetración en el baño

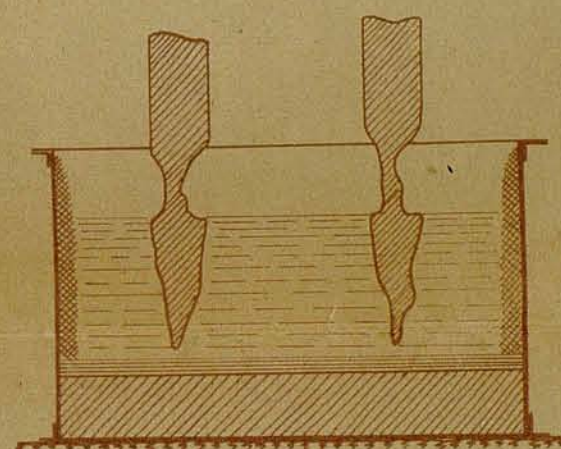
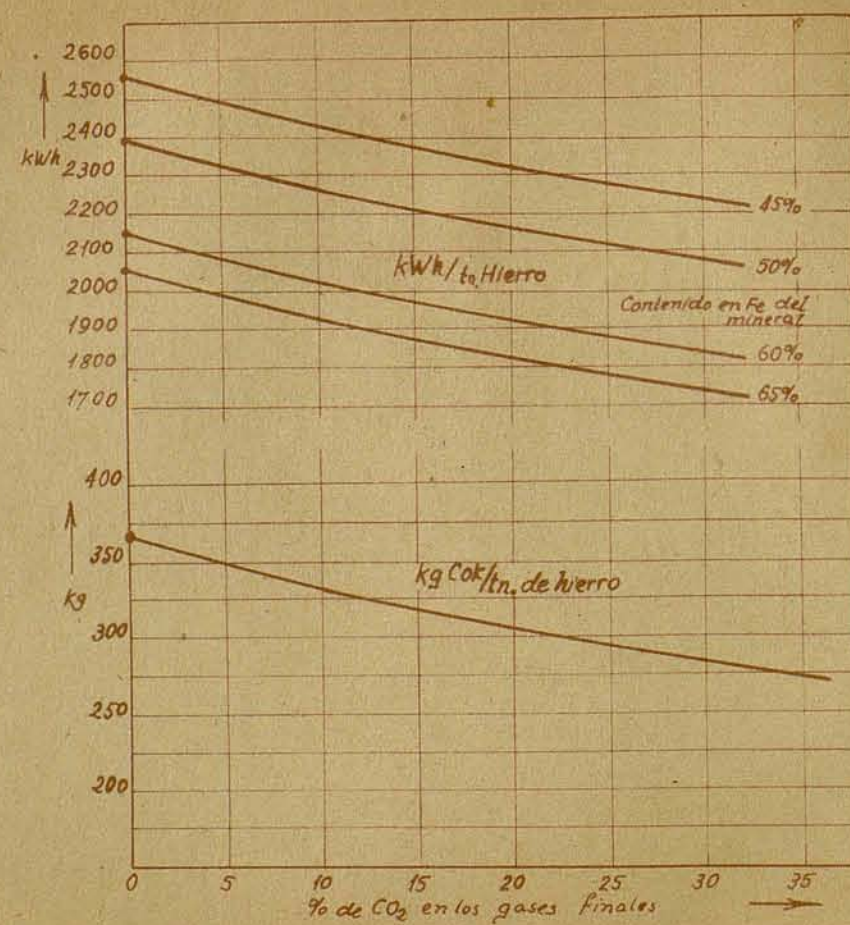
Fig. 252. Desgaste con cuba demasiado alta y exesiva  
inmersión.

Fig. 248.

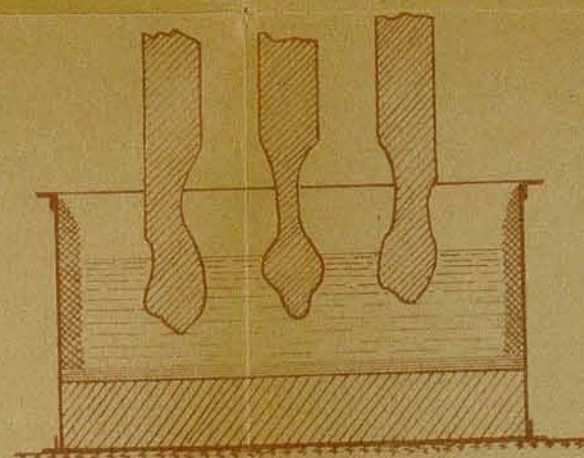
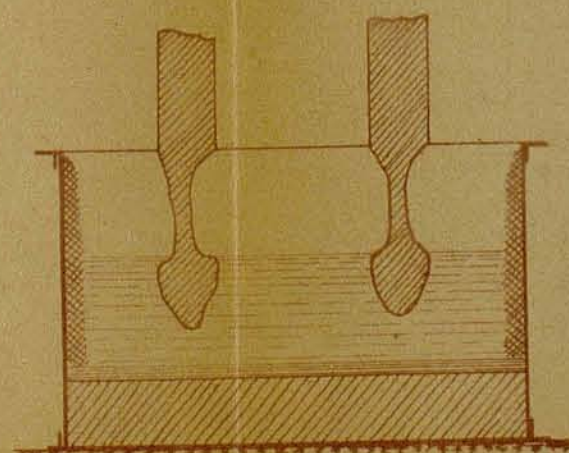
Fig. 249. Quemado de electrodos con distancia dema-  
siado pequeña.

Fig. 250. Cuba demasiado alta

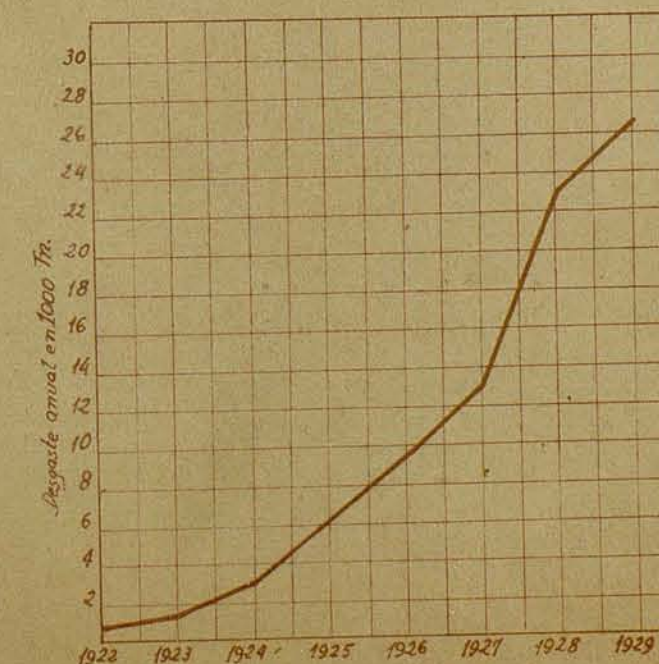


Fig. 253.